

REPORT ON

SELECTION OF REMEDY
AES PUERTO RICO – AGREMAX™ STAGING AREA
GUAYAMA, PUERTO RICO

by Haley & Aldrich, Inc. Cleveland, Ohio

for AES Puerto Rico LP Guayama, Puerto Rico

File No. 133136-004 June 1, 2020



SELECTION OF REMEDY REPORT CERTIFICATION STATEMENT

I, Steven F. Putrich, am a professional engineer and am licensed in the state of Indiana. I have reviewed the Selection of Remedy report for the AES Puerto Rico AGREMAX™ Staging Area located in Guayama, Puerto Rico dated June 1, 2020. By affixing my professional seal and signature, I hereby acknowledge that this report has been prepared in conformance with the requirements of the U.S. EPA CCR Rule¹.

For the purposes of satisfying the requirements of the U.S. EPA CCR Rule, Winston R. Esteves of WRE [WRE, P.O. Box 195597, San Juan, PR 00919-5597, estevesw@yahoo.com], a professional engineer licensed in the Commonwealth of Puerto Rico, has reviewed and sealed and signed the same subject report dated June 1, 2020 for the purpose of certifying conformance with the U.S. EPA CCR Rule, and that same certification is included in the published version of the subject report.

Steven F. Putrich, PE (Indiana)



P.E. Seal License Number: PE11200566

June 1, 2020

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¹ U.S. Environmental Protection Agency's (USEPA) rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities (U.S. EPA CCR Rule).* 80 Fed. Reg. 21302 (April 17, 2015) (promulgating 40 CFR §257 and §261); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257).



Winston R. Esteves

Environmental Consultant

SELECTION OF REMEDY REPORT CERTIFICATION STATEMENT

I, Winston R. Esteves, am a professional engineer and licensed in the commonwealth of Puerto Rico. I have reviewed this Selection of Remedy report for the AES Puerto Rico AGREMAX™ Staging Area located in Guayama, Puerto Rico. I hereby certify that this report has been prepared in general conformance with the requirements of the U. S. Environmental Protection Agency's (USEPA) Rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities*. 80 Fed. Reg. 21302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257.61) (the CCR Rule).

Winston R. Esteves, PE

June 1, 2020

Date

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SELECTION OF REMEDY REPORT - 40 CFR § 257.97 AES Puerto Rico AGREMAX™ Temporary Staging Area

INTRODUCTION

AES Puerto Rico (AES-PR) retained Haley & Aldrich, Inc. (Haley & Aldrich) to prepare this Selection of Remedy Report for the AGREMAXTM temporary staging area (Staging Area) located at the AES-PR generation facility in Guayama, Puerto Rico. The selection of remedy for the Staging Area is completed according to the requirements of the U.S. Environmental Protection Agency's (USEPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities (CCR Rule).

In accordance with 40 CFR § 257.97(b), a remedy must:

- Be protective of human health and the environment;
- Achieve the GWPS;
- Control the source of releases so as to reduce or eliminate, to the maximum extent feasible, further release of Appendix IV constituents; and
- Comply with certain standards for management of waste (40 CFR § 257.98d)).

In September 2019 (amended in November 2019), AES-PR completed the Corrective Measures Assessment (CMA) Report for the AGREMAXTM Staging Area included as **Appendix A.** The CMA considered a series of corrective measure alternatives, all of which were demonstrated to meet these threshold criteria listed above. The CMA Report also included the results of numerous technical evaluations conducted by consultants which include groundwater modeling, human health and ecological risk assessments, and nature and extent of CCR constituents in groundwater assessments. The CMA compared the corrective measure alternatives to one another with respect to three of the four balancing criteria identified in the CCR Rule: long- and short-term effectiveness, source control, and implementability.

As required by the CCR Rule, AES-PR published the CMA Report to its public CCR Website and held a Public Meeting to discuss the results of the CMA with interested and affected parties. AES-PR received public input and comments during the public meeting on December 12, 2019 and accepted comments through a portal on its CCR public website from December 12, 2019 through January 28, 2020. AES-PR received verbal comments from the public during the public meeting and written comments through its CCR public website portal. In addition, AES-PR received written comments from the Puerto Rico Department of Natural and Environmental Resources (DNER) by electronic mail along with written comments received from USEPA Region 2 by electronic mail, dated March 5, 2020.

ASSESSMENT OF THE FOURTH BALANCING CRITERIA

The comments received related to the CMA are addressed herein to inform the assessment of the fourth balancing criteria listed under 40 CFR § 257.97(c)(4) of the CCR Rule which states:

"...the degree to which community concerns are addressed by a potential remedy(s)."

To assess the degree to which community concerns were addressed and thereby assess the fourth balancing criteria, Haley & Aldrich considered comments received related to the CMA and formulated responses to specific issues or concerns raised in those comments. Written responses to comments received related to the CMA are included in **Appendix B** and are responsive to the concerns raised regarding potential remedies thereby satisfying the fourth balancing criteria set forth in 40 CFR § 257.97(c)(4).

Consistent with the approach followed in the CMA report, a graphic of the overall favorability of each remedial alternative with the addition of the fourth balancing criteria is provided below. In this graphic, green represents most favorable, yellow represents less favorable, and red represents the least favorable rating relative to the degree to which community concerns were addressed by each of the potential remedies in the CMA.

Comments or concerns were expressed on the specific remedies associated with all five alternatives in the CMA. In conclusion, green represents a favorable rating relative to the degree to which community concerns were addressed by AES-PR's responses to the noted Alternatives.

	Remedial Alternative Description				
BALLANCING CRITERIA	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)	Alternative 2 Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Alternative 5 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation
CATEGORY 1					
Long- and Short Term Effectiveness, Protectiveness, and Certainty of Success					
CATEGORY 2 Effectiveness in controlling the source to reduce further releases					
CATEGORY 3 Ease of implementation					
CATEGORY 4 Degree to which Community Concerns are Addressed by a Potential Remedy					

The results of the CMA addressing the first three balancing criteria in addition to the information received during the public process informed the final remedy selection. A summary of AES-PR's remedial plan is provided below which will, when fully implemented and completed, achieve the corrective measures objectives in accordance with the CCR Rule requirements.

CORRECTIVE MEASURES REMEDIAL PLAN – SELECTION OF REMEDY

Based on results of the CMA, public input, and the results of additional technical analysis completed in response to public input, AES-PR intends to select the following corrective action for the AGREMAXTM Staging Area:



MA Report Alternative 1: Prevent AGREMAXTM contact with the ground by installation of a synthetic liner and employ Monitored Natural Attenuation (MNA).

The installation of a low-permeability geomembrane liner system along with MNA constitutes an appropriate remedial corrective measure for groundwater impacts. The proposed liner system including the drainage collection system at the base of the relined AGREMAXTM Staging Area will effectively eliminate the infiltration of water into the groundwater aquifer below the Staging Area and MNA will reduce the limited and localized CCR-related impacts in groundwater immediately downgradient of the AGREMAXTM Staging Area. As summarized in the CMA report, constituent concentrations are predicted to decrease over time following the implementation of the selected remedy. This will allow groundwater conditions with the aid of MNA to stabilize and eventually achieve the GWPS.

Within 90 days of selecting a remedy, in accordance with 40 CFR § 257.98(a), AES-PR will:

- 1. Establish and implement a corrective action groundwater monitoring program;
- 2. Implement the corrective action remedy selected; and
- 3. Take any interim measures necessary.

At this time, the corrective measures cited herein are deemed sufficient to meet the objectives of the CCR Rule. No additional corrective measures (including interim measures) beyond those cited herein are envisioned at this time. However, It is recognized that remedial actions are iterative in nature and AES-PR (as part of the long-term performance monitoring program) will periodically evaluate updated groundwater conditions and determine whether additional measures are warranted to achieve the objectives of the CCR Rule related to groundwater.

PLAN AND ACTION STEPS FOR THE IMPLEMENTATION OF THE SELECTED REMEDY

AES plans to take the following steps to implement the selected remedy:

- 1. Establish and implement a corrective action groundwater monitoring program that:
 - a. Meets the requirements of an assessment monitoring program under 40 CFR § 257.95;
 - b. Documents the effectiveness of the corrective action remedy; and
 - c. Demonstrates compliance with the groundwater protection standard.
- 2. Continue the reduction of the volume of AGREMAX[™] from the Staging Area to allow for installation of the liner;
- 3. Install a low-permeability geomembrane liner (a minimum 1 x 10 -7 centimeters per second) under the footprint of the AGREMAXTM staging area to control the source of CCR-related constituents and minimize infiltration of the AGREMAXTM in the Staging Area.



- 4. Utilize MNA of groundwater concentrations¹ to address limited and localized CCR-related impacts. Ongoing monitoring and modeling evaluations will be utilized to document the change in concentrations of CCR constituents in groundwater as previously presented in the CMA.
- 5. Prepare Annual Groundwater Monitoring and Corrective Action Reports for the site that incorporate the corrective action groundwater monitoring program to document the effectiveness of the corrective action remedy.

IMPLEMENTATION OF REMEDY SCHEDULE

Under its currently estimated schedule, AES-PR plans to have the synthetic liner installed under the AGREMAXTM Staging Area by August 1, 2021 based on relevant assumptions, including regulatory agency approvals and permits, contractor availability, AGREMAXTM shipment schedule, and other logistical considerations. AES-PR has implemented the remedy including completion of the following actions to date:

- AES-PR has engaged a contractor to perform the liner installation; and
- Engineering design has been completed for liner installation.

In addition, AES-PR is in the process of geotechnical evaluations of materials for use in the project and preparing application materials for Agency approvals (Environmental Assessment and permits).

Set forth below are estimated key milestones in the future remedial activities associated with the selected remedy. This schedule is based on best available information and assumptions and is subject to change as additional information becomes available. The schedule may be advanced or delayed based on factors including timing of regulatory agency approvals and permits, potential issues related to COVID-19 global pandemic, contractor availability, AGREMAXTM shipment schedules, and other logistical considerations. In any event, AES-PR will complete remedial activities within a reasonable period of time based on these, and other, relevant factors.

- Complete and submit application for Environmental Assessment June 2020
- Complete and submit application for applicable environmental permits Following approval of Environmental Assessment (date to be determined)
- Receive all applicable permits and approvals December 31, 2020
- Initiate installation of liner February 1, 2021
- Complete installation of liner August 1, 2021
- Establish and implement Corrective Action Groundwater Monitoring Program August 1, 2021

HALEY ALDRICH

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¹ MNA occurs due to naturally occurring processes within the aquifer to reduce concentrations of CCR constituents in groundwater. MNA encompasses a variety of physical and chemical processes (biodegradation, sorption, dilution, chemical reactions, and evaporation), which, under the right conditions, can immobilize metals in aquifer sediments. In addition to lining the AGREMAX[™] Staging Area as a remedial corrective measure, EPA recognizes MNA as a corrective action component for addressing inorganics (metals) in groundwater (EPA Directive 9283.1-36 (2015)).

	Revision Log					
Date	Page No.	Section	Description	June 2020 Text	Revised Text	



APPENDIX A

Corrective Measures Assessment



REPORT ON

CORRECTIVE MEASURES ASSESSMENT AES PUERTO RICO – AGREMAX™ STAGING AREA GUAYAMA, PUERTO RICO

by Haley & Aldrich, Inc. Cleveland, Ohio

for AES Puerto Rico LP Guayama, Puerto Rico

File No. 133136-004 September 2019 AMENDED 8 November 2019



Winston R. Esteves

Environmental Consultant

CMA REPORT CERTIFICATION STATEMENT

I, Winston R. Esteves, am a professional engineer and licensed in the commonwealth of Puerto Rico. I have reviewed this Corrective Measures Assessment (CMA) report for the AES Puerto Rico AGREMAX™ Staging Area located in Guayama, Puerto Rico. I hereby certify that this report has been prepared in general conformance with the requirements of the U. S. Environmental Protection Agency's (USEPA) rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities.* 80 Fed. Reg. 21302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257.61) (CCR Rule).

Winston R. Esteves, PE

September 13, 2019

Date

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License Number

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CMA REPORT CERTIFICATION STATEMENT

I, Steven F. Putrich am a professional engineer and licensed in the state of Indiana. I have reviewed the Corrective Measures Assessment (CMA) report for the AES Puerto Rico AGREMAX™ Staging Area located in Guayama, Puerto Rico dated September 13, 2019. By affixing my professional seal and signature I hereby acknowledge that this report has been prepared in conformance with the requirements of the USEPA CCR Rule¹.

For the purposes of satisfying the requirements of the USEPA CCR Rule, Winston R. Esteves of WRE [WRE, PO Box 195597, San Juan, PR 00919-5597. esteves_w@yahoo.com], a professional engineer licensed in the Commonwealth of Puerto Rico has reviewed and sealed and signed the same subject report dated September 13, 2019 for the purpose of certifying conformance with the USEPA CCR Rule, and that same certification is included in the published version of the subject report.

Steven F. Putrich, PE (Indiana)

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September 2019

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¹ U.S. Environmental Protection Agency's (USEPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities (USEPA CCR Rule). 80 Fed. Reg. 21302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257.61).

Overview

Counsel retained Haley & Aldrich, Inc. (Haley & Aldrich) on behalf of AES Puerto Rico LP (AES-PR) to prepare this Corrective Measures Assessment (CMA) for the AGREMAX™ temporary staging area (Staging Area) located at the AES Puerto Rico generation facility in Guayama, Puerto Rico (the Site). The Staging Area is being evaluated under the requirements applicable to a coal combustion residuals (CCR) landfill in the U. S. Environmental Protection Agency's (USEPA) rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities.* 80 Fed. Reg. 21302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257.61) (CCR Rule). AES-PR monitors groundwater at the Staging Area and has conducted detailed geologic and hydrogeologic investigations following USEPA CCR Rule requirements.

AES-PR implemented groundwater monitoring following the CCR Rule requirements through a phased approach to allow for a graduated response and evaluation of steps to address groundwater quality. Detection monitoring indicated statistically significant increases (SSI) for some Appendix III constituents. Assessment monitoring completed in 2018 evaluated the presence and concentration of Appendix IV constituents in groundwater specified in the CCR Rule. Of the 15 CCR Appendix IV parameters evaluated, only three – molybdenum, lithium, and selenium – were detected at statistically significant levels (SSL) above the Groundwater Protection Standards (GWPS) established for the Staging Area.

In performing this CMA, Haley & Aldrich considered the following: presence and distribution of CCR-derived constituents in groundwater, the configuration of the Staging Area, hydrogeologic setting, and the results of a detailed risk evaluation. The alluvial aquifer beneath the Staging Area is approximately 15 feet in thickness transitioning to marsh deposits near the southern portion of the Site. Groundwater flow beneath the Staging Area is generally from north to south, towards Las Mareas Harbor.

To provide a comprehensive CMA, the evaluation described herein includes activities and groundwater remediation alternatives that were combined to constitute comprehensive groundwater remedies designed to achieve the GWPS, including:

- Alternative 1: Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)
- Alternative 2: Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment
- Alternative 3: Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation
- Alternative 4: Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment
- Alternative 5: Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation

These five alternatives were evaluated based on the threshold criteria provided in the CCR rule (§257.97 (b)) and then compared to three of the four balancing criteria stated in the CCR Rule (§257.97 (c)). These criteria are introduced below and included in their entirety in **Section 1**:

§ 257.97 Selection of remedy

(b) Remedies must [Threshold Criteria]:



- (1) Be protective of human health and the environment;
- (2) Attain the groundwater protection standard as specified pursuant to § 257.95(h);
- (3) Control the source(s) of releases so as to reduce or eliminate, to the maximum extent feasible, further releases of constituents in appendix IV to this part into the environment;
- (4) Remove from the environment as much of the contaminated material that was released from the CCR unit as is feasible, taking into account factors such as avoiding inappropriate disturbance of sensitive ecosystems;
- (5) Comply with standards for management of wastes as specified in § 257.98(d).
- (c) In selecting a remedy that meets the standards of paragraph (b) of this section, the owner or operator of the CCR unit shall consider the following evaluation factors [Balancing Criteria]:
 - (1) The long- and short-term effectiveness and protectiveness of the potential remedy(s), along with the degree of certainty that the remedy will prove successful
 - (2) The effectiveness of the remedy in controlling the source to reduce further releases
 - (3) The ease or difficulty of implementing a potential remedy(s)
 - (4) The degree to which community concerns are addressed by a potential remedy(s).

All of the remedies proposed to achieve the GWPS must meet the five <u>threshold criteria</u>, above, to be considered for inclusion as a remedial alternative. Development of these remedial alternatives and their conformance with the threshold criteria are presented in **Section 4**.

Section 5 evaluates the five remedial alternatives with respect to the <u>balancing criteria</u> listed above. Note that balancing criteria (4), which considers community concerns, will be evaluated following a public information session to be held at least 30 days prior to remedy selection.

The following provides a summary of the remedial alternatives for the Staging Area, as described more fully in this report:

- Remedial Alternatives: One remedial alternative to achieve GWPS involves prevention of AGREMAX™ contact with the ground via installation of a synthetic liner in the Staging Area for future management of AGREMAX™. Vertical infiltration via precipitation would be virtually eliminated following installation of the Staging Area liner system. Appendix IV constituents in groundwater above GWPS would be addressed by natural attenuation. The remaining four remedial alternatives do not include a Staging Area liner system and address constituents present in groundwater above GWPS via active groundwater pumping.
- **Groundwater Risk Evaluation:** The CCR Rule groundwater investigation demonstrates that the impacts of the Staging Area are limited. To evaluate extent, nature & extent temporary groundwater monitoring wells were located at the property boundary located less than 200 feet downgradient from the CCR Rule wells, which are located directly adjacent to the Staging Area. The analytical results demonstrate that there are no concentrations of the SSL constituents above GWPS in these wells. In other words, concentrations of lithium, molybdenum and selenium are not elevated beyond the Site property boundary.

There is no impact on drinking water and there is no evidence of impact to human health or the environment. There are no downgradient users of groundwater as drinking water – thus, there is no impact on drinking water. Las Mareas Harbor was sampled and does not show impacts.



There is no exposure to CCR-derived constituents detected in groundwater at the Site – either via groundwater use or surface water. Even for the very few results that may be above screening values for some of the sampling events, there is no complete drinking water exposure pathway to groundwater. Where there is no exposure, there is no risk.

Therefore, because no adverse risk currently exists, any of the remedies considered herein are all protective of human health and the environment, and implementation of any of the remedial alternatives will not result in a meaningful reduction in risk to groundwater-related exposures or risk.

 Remedy Timeframe and Approach: The timeframes to achieve the GWPS associated with Staging Area lining and natural attenuation, and the active hydraulic containment alternatives are comparable, and the period for installation of the Staging Area liner is brief. For the remaining alternatives groundwater would be addressed by long-term pumping with either direct discharge to an existing surface water impoundment or routing of the water to the on-site water treatment system.

In accordance with §257.98, AES-PR will implement a groundwater monitoring program to document the effectiveness of the selected remedial alternative. Corrective measures are considered complete when monitoring reflects that the SSL constituent concentrations in groundwater downgradient of the Staging Area are not present above the Appendix IV GWPS for three consecutive years.

USEPA is in the process of modifying certain CCR Rule requirements and, depending upon the nature of such changes, assessments made herein could be modified or supplemented to reflect such future regulatory revisions. See *Federal Register (March 15, 2018; 83 FR 11584*).



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List of Acronyms and Abbreviations

Abbreviation	Definition
AES-PR	AES Puerto Rico LP
bgs	Below Ground Surface
CCR	Coal Combustion Residual
CPCPRC	Chevron Phillips Chemical Puerto Rico Core, LLC
CMA	Corrective Measures Assessment
CSM	Conceptual Site Model
DNA	DNA-Environment, LLC
GMP	Groundwater Monitoring Plan
GWPS	Groundwater Protection Standards
Haley & Aldrich	Haley & Aldrich, Inc.
HC	Hydraulic Containment
MCL	Maximum Contaminant Level
MNA	Monitored Natural Attenuation
N&E	Nature and Extent
0&M	Operation & Maintenance
RO	Reverse Osmosis
Site	AES Puerto Rico Generating Facility
SSI	Statically Significant Increase
SSL	Statistically Significant Level
Staging Area	AGREMAX™ Temporary Staging Area
SW-DAF	Surface Water Dilution and Attenuation Factor
ug/L	Microgram per Liter
USEPA	United States Environment Protection Agency



1. Introduction

Counsel retained Haley & Aldrich, Inc. (Haley & Aldrich) on behalf of AES Puerto Rico LP (AES-PR) to prepare this Corrective Measures Assessment (CMA) for the AGREMAX™ temporary staging area (Staging Area) located at the AES-PR generation facility (the Site) in Guayama, Puerto Rico. The Staging Area is being evaluated under the requirements applicable to a coal combustion residuals (CCR) landfill in the U. S. Environmental Protection Agency's (USEPA) rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities*. 80 Fed. Reg. 21302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36435 (July 30, 2018) (amending 40 CFR §257.61) (CCR Rule). AES-PR monitors groundwater at the Staging Area and has conducted detailed geologic and hydrogeologic investigations following USEPA CCR Rule requirements.

This CMA includes a summary of the groundwater monitoring results for the CCR Rule Appendix III and Appendix IV constituents, an evaluation of the Appendix III constituents for statistically significant increases (SSI) compared to background, and a comparison of the Appendix IV constituents detected in assessment monitoring to the Groundwater Protection Standards (GWPS). These evaluations identified statistically significant levels (SSL) above GWPS for lithium, molybdenum and selenium in groundwater at two monitoring well locations downgradient of the Staging Area. This report evaluates potential corrective measures to remediate groundwater for the constituents present in groundwater at SSLs above the GWPS.

1.1 FACILITY DESCRIPTION/BACKGROUND

AES-PR operates a 454-megawatt coal-fired power plant in Guayama, Puerto Rico, located on the southern shore of the island (**Figure 1-1**). The Site is bordered by a former pharmaceutical plant to the north, a former chemical plant to the east, a marsh and Las Mareas Harbor to the south, and a solar energy farm to the west.

AES-PR uses CCR generated at the plant to produce AGREMAX™, a manufactured aggregate, which has been used beneficially for landfill daily cover, roadway construction, and other applications. Prior to beneficial use or off-site disposal, AES-PR's inventory of AGREMAX™ is placed in the on-site Staging Area, an approximately seven-acre area located to the south of the generating station (**Figure 1-2**). AES-PR has used the Staging Area to manage AGREMAX™ product since beginning operations in 2002.

The AES-PR generating plant is considered a zero-discharge facility that utilizes reclaimed water obtained from the Guayama wastewater treatment plant operated by Puerto Rico Aqueduct and Sewer Authority, located approximately 0.5 mile east of the power plant. The reclaimed water is stored in a Lagoon in the northern portion of the Site.

Site stormwater is generally directed to and collected in either the 2-million-gallon stormwater retention pond or the larger coal pile runoff pond which stores water for use in the cooling tower, where much of the water is evaporated. A water treatment system, centrally located on-site adjacent to the plant, treats water from the 2-million-gallon stormwater retention pond intended for use for non-process water needs at the Site. The treatment system includes a two-stage side stream Reverse Osmosis (RO) system. According to AES-PR personnel, the secondary system is active, but the primary RO system is currently not in use.



1.2 GROUNDWATER MONITORING

Groundwater monitoring under the CCR Rule occurs through a phased approach to allow for a graduated response (i.e., baseline, detection, and assessment monitoring as applicable) and evaluation of steps to address groundwater quality. DNA-Environment, LLC (DNA) prepared a Groundwater Monitoring Plan (GMP) as required by the CCR Rule [identified as "AES Puerto Rico Groundwater Monitoring System" available at http://aespuertorico.com/ccr/]. The GMP presents the design of the groundwater monitoring system, groundwater sampling and analysis procedures, and groundwater statistical analysis methods.

In July 2017, five groundwater-monitoring wells were installed by DNA, on behalf of AES-PR which meet the CCR Rule requirements in 40 CFR Part 257.91, Groundwater Monitoring Systems. Monitoring well locations are shown in **Figure 1-3**. Three of these wells (MW-3, MW-4 and MW-5) were installed hydraulically downgradient of the Staging Area, whereas monitoring wells MW-1 and MW-2 were placed at hydraulically upgradient locations from the Staging Area. The monitoring wells range in depth from 20 to 25 feet below ground surface (bgs).

Detection monitoring sampling events occurred in 2017 and 2018. The results of the sampling events were then compared to background, or natural groundwater values, using statistical methods to determine if CCR Rule Appendix III constituents at the down-gradient edge of the Staging Area are present at concentrations above background; this condition is referred to as a Statistically Significant Increase (SSI). The results of this analysis indicated SSIs necessitating the establishment of an Assessment Monitoring Program and respective notification.

During the Assessment Monitoring phase, CCR groundwater monitoring well samples were collected during June and October 2018 and subsequently analyzed for CCR Rule Appendix IV constituents. Evaluation of these data identified statistically significant levels (SSL) above GWPS for lithium, molybdenum and selenium in groundwater at two monitoring well locations downgradient of the Staging Area. Appendix IV analytical results for the baseline and Assessment Monitoring events are summarized in **Table I**.

1.3 CORRECTIVE MEASURES ASSESSMENT PROCESS

The CMA process involves assessment of groundwater remediation technologies. These remedies must meet the following threshold criteria as stated in the CCR Rule:

§257.97 Selection of remedy [Threshold Criteria]

- (b) Remedies must:
 - (1) Be protective of human health and the environment;
 - (2) Attain the groundwater protection standard as specified pursuant to §257.95(h);
 - (3) Control the source(s) of releases so as to reduce or eliminate, to the maximum extent feasible, further releases of constituents in appendix IV to this part into the environment;
 - (4) Remove from the environment as much of the contaminated material that was released from the CCR unit as is feasible, taking into account factors such as avoiding inappropriate disturbance of sensitive ecosystems;
 - (5) Comply with standards for management of wastes as specified in §257.98(d).



Once these technologies are demonstrated to meet these threshold criteria, they are then compared to one another with respect to the following balancing criteria as stated in the CCR Rule:

§257.97 Selection of remedy [Balancing Criteria]

- (c) In selecting a remedy that meets the standards of paragraph (b) of this section, the owner or operator of the CCR unit shall consider the following evaluation factors:
 - (1) The long- and short-term effectiveness and protectiveness of the potential remedy(s), along with the degree of certainty that the remedy will prove successful based on consideration of the following:
 - (i) Magnitude of reduction of existing risks;
 - (ii) Magnitude of residual risks in terms of likelihood of further releases due to CCR remaining following implementation of a remedy;
 - (iii) The type and degree of long-term management required, including monitoring, operation, and maintenance;
 - (iv) Short-term risks that might be posed to the community or the environment during implementation of such a remedy, including potential threats to human health and the environment associated with excavation, transportation, and redisposal of contaminant;
 - (v) Time until full protection is achieved;
 - (vi) Potential for exposure of humans and environmental receptors to remaining wastes, considering the potential threat to human health and the environment associated with excavation, transportation, re-disposal, or containment;
 - (vii) Long-term reliability of the engineering and institutional controls; and (viii) Potential need for replacement of the remedy.
 - (2) The effectiveness of the remedy in controlling the source to reduce further releases based on consideration of the following factors:
 - (i) The extent to which containment practices will reduce further releases; and
 - (ii) The extent to which treatment technologies may be used.
 - (3) The ease or difficulty of implementing a potential remedy(s) based on consideration of the following types of factors:
 - (i) Degree of difficulty associated with constructing the technology;
 - (ii) Expected operational reliability of the technologies;
 - (iii) Need to coordinate with and obtain necessary approvals and permits from other agencies;
 - (iv) Availability of necessary equipment and specialists; and
 - (v) Available capacity and location of needed treatment, storage, and disposal services
 - (4) The degree to which community concerns are addressed by a potential remedy(s).

The fourth balancing criterion involves input from the community regarding the proposed remedial alternatives. This criterion will be addressed by presenting the alternatives at a public meeting and soliciting comments. That meeting will be held at least 30 days prior to remedy selection by AES.

1.4 RISK REDUCTION AND REMEDY

As presented above, the CCR Rule (§257.97(b)(1) – Selection of Remedy) requires that remedies must be protective of human health and the environment. Further, §257.97(c) of the CCR Rule requires that in selecting a remedy, the owner or operator of the CCR unit must consider specific evaluation factors,



including the risk reduction achieved by each of the proposed corrective measures. Each of the balancing criteria listed here from §257.97 and discussed in **Section 5** are those that consider risk to human health or the environment including:

- (c)(1)(i) Magnitude of reduction of existing risks;
- (c)(1)(ii) Magnitude of residual risks in terms of likelihood of further releases due to CCR remaining following implementation of a remedy;
- (c)(1)(iv) Short-term risks that might be posed to the community or the environment during implementation of such a remedy, including potential threats to human health and the environment associated with excavation, transportation, and re-disposal of contaminant;
- (c)(1)(vi) Potential for exposure of humans and environmental receptors to remaining wastes, considering the potential threat to human health and the environment associated with excavation, transportation, re-disposal, or containment;

The following are additional factors related to risk that are factored into the schedule for implementing and completing remedial activities once a remedy is selected (§257.97(d)):

- (d)(4) Potential risks to human health and the environment from exposure to contamination prior to completion of the remedy¹;
- (d)(5)(i) Current and future uses of the aquifer;
- d)(5)(ii) Proximity and withdrawal rate of users; and
- (d)(5)(iv) The potential damage to wildlife, crops, vegetation, and physical structures caused by exposure to CCR constituents.

Section 3 presents a summary of the groundwater risk evaluation that provides the basis for evaluating these risk-based balancing criteria in **Section 5**.

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¹ Factors (d)(4) and (d)(5) are not part of the CMA evaluation process as described in §257.97(d)(4), §257.97(d)(5)(i)(ii)(iv); rather they are factors the owner or operator must consider as part of the schedule for remedy implementation.

2. Groundwater Conceptual Site Model

The Staging Area geology and hydrogeology were initially described in the *Groundwater Monitoring System & Sampling and Analysis Program* prepared by DNA in August 2017 to support the development of a hydrogeologic Conceptual Site Model (CSM) [available at http://aespuertorico.com/wp-content/uploads/2017/10/AESPuerto-Rico Groundwater Monitoring System.pdf]. The CSM has been further enhanced with ongoing CCR groundwater monitoring and supplemental subsurface investigation activities performed by DNA. Findings from these extensive geologic and hydrogeologic investigations have produced a robust CSM that supports the CMA activities discussed in this report.

2.1 SITE SETTING

The Site is located near the marine shoreline on the southern side of the island of Puerto Rico. Based on reports prepared by DNA, the Site geology consists of alluvial deposits which transition to marine marsh and beach deposits in the far southern portion of the Site. The Site is bordered by a former pharmaceutical plant to the north, a former chemical plant to the east, a marsh and Las Mareas Harbor to the south, and a solar energy farm to the west.

2.2 GEOLOGY AND HYDROGEOLOGY

Based on reports prepared by DNA, the Site geology consists of alluvial deposits which transition to marine marsh and beach deposits in the far southern portion of the Site. The Site is underlain by fill material to a depth of approximately 10 feet bgs and an upper water bearing unit consisting of sandy clay and clayey sand to a depth of approximately 25 feet bgs. The upper water bearing unit is bounded/underlain vertically by a stiff clay layer. Slug tests performed in the upper water bearing unit indicate that the hydraulic conductivity ranges from 0.035 to 0.67 feet/day (1.2x10⁻⁵ to 2.4x10⁻⁴ centimeters/second).

Groundwater flow beneath the Staging Area is generally from north to south (see **Figure 1-2**). The groundwater hydraulic gradient beneath the Staging Area is approximately 0.005 to 0.011 (ft/ft). Groundwater elevations measured in the three downgradient monitoring wells (MW-3, MW-4, and MW-5) as well as nine temporary monitoring wells (TW-101 through TW-109) (nature and extent (N&E) wells) –installed to address the nature and extent of Appendix IV constituents at SSLs above the GWPS in groundwater) suggest that the groundwater elevations are equalized immediately adjacent to the southern property boundary. The ditch located south of the N&E wells and south property boundary represents a more permeable flow path, resulting in more consistent head values as observed in the N&E wells installed along the property boundary. The N&E wells along the property boundary do not show constituents above GWPS and therefore the ditch would not be impacted by the Staging Area.

Due to the close proximity of the Site to the ocean shoreline, fresh groundwater would be expected to transition to saline (brackish) groundwater near the estuarine or marine margin. While the groundwater collected from monitoring wells MW-3 through MW-5 is freshwater, chemical parameters in the groundwater (boron, chloride) suggest some localized mixing of saline water.



2.3 ADJACENT PROPERTY ENVIRONMENTAL CONDITIONS

The former Chevron Phillips Chemical Puerto Rico Core, LLC (CPCPRC) facility on the eastern border of the Site is in Corrective Action overseen by USEPA. Based on a review of available documents, a groundwater plume of benzene and sulfolane is present beneath the former CPCPRC facility and the plume extends onto the AES-PR site, specifically in the vicinity of the Staging Area. Data from reports on file² indicate that the footprint of benzene and sulfolane from the former CPCPRC facility onto the AES-PR property is generally limited to monitoring wells along or near the eastern property boundary of the Site.

As described in the "Statement of Basis Final Remedy Decision" the remedial alternative selected to address groundwater at the former CPCPRC facility is In-situ Chemical Oxidation using Catalyzed Hydrogen Peroxide that will be injected into the shallow and deep aquifers beneath the Chevron facility. A groundwater monitoring program will be implemented to evaluate the overall remedial program efficiency in reducing the concentrations of the contaminant of concerns in the deep and shallow aquifers.

At this time, the impacts and detailed assessment of nature and extent of this organic plume have not been vetted in this CMA. The specifics of the implementation of the chemical oxidation remedy at the former CPCPRC facility and the potential impact of the CPCPRC remediation system on groundwater at the AES-PR facility is not known at this time. The design of the final corrective measure for the AES-PR Staging Area will take into account the CPCPRC remedial activities. Impacts to Site RO system for treatment of groundwater collected as part of any of the remedial options considered would be part of a future corrective measures work element.

2.4 GROUNDWATER PROTECTION STANDARDS

The GWPS are defined in the CCR Rule at §257.95 Assessment monitoring program:

- (h) The owner or operator of the CCR unit must establish a groundwater protection standard for each constituent in appendix IV to this part detected in the groundwater. The groundwater protection standard shall be:
 - (1) For constituents for which a maximum contaminant level (MCL) has been established under §§141.62 and 141.66 of this title, the MCL for that constituent;
 - (2) For constituents for which an MCL has not been established, the background concentration for the constituent established from wells in accordance with §257.91; or
 - (3) For constituents for which the background level is higher than the MCL identified under paragraph (h)(1) of this section, the background concentration.

USEPA published Amendments to the National Minimum Criteria Finalized in 2018 (Phase One, Part One) in the Federal Register on July 30, 2018 (USEPA, 2018b). This included revising the groundwater protection standard for constituents that do not have an established drinking water standard (or MCL) at §257.95 Assessment monitoring program (h) (2):

Cobalt – 6 ug/L (micrograms per liter)

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² Corrective Measures Study Report Chevron Phillips Chemical Puerto Rico Core, LLC Guayama, Puerto Rico (PEI April 2016).

³ Statement of Basis Final Remedy Decision Chevron Phillips Chemical (USEPA, June 2017).

- Lead 15 ug/L
- Lithium 40 ug/L
- Molybdenum 100 ug/l

Because the GWPS is the higher of the drinking water concentration and the background concentration, and background concentrations are specific to each ash management area, the GWPS are considered to be site-specific.

DNA completed a statistical evaluation of groundwater samples using the methods and procedures outlined in the *Groundwater Monitoring System & Sampling and Analysis Program* (DNA August 2017) [available at http://aespuertorico.com/wp-content/uploads/2017/10/AESPuerto-Rico Groundwater Monitoring System.pdf] to develop the background concentrations and then the site-specific GWPS for each Appendix IV constituent.

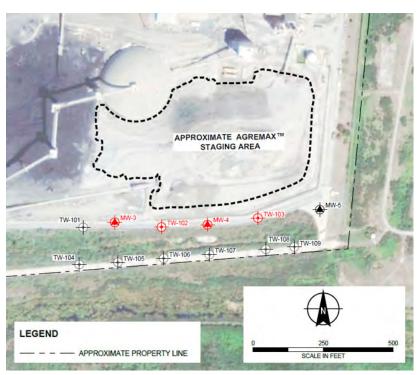
Groundwater results were compared statistically to the site-specific GWPS. SSLs above the GWPS are limited to three constituents at two monitoring wells: lithium (MW-4), molybdenum (MW-3 and MW-4), and selenium (MW-3) as shown on **Figure 2-1**. A sample-by-sample comparison of the groundwater analytical results to GWPS is provided in **Table I**. These three Appendix IV constituents (lithium, molybdenum, and selenium), their respective concentrations compared to the GWPS and associated details of the CSM are used to assemble the viable list of remedial alternatives considered in this CMA.

2.5 NATURE AND EXTENT OF GROUNDWATER IMPACTS

AES-PR initiated a nature and extent (N&E) investigation as required by the CCR Rule in May 2019 by contracting DNA to install two (2) temporary piezometers immediately north and east of the Staging Area and nine (9) temporary monitoring wells (N&E wells) with three (TW-101, TW-102 & TW-103) in line with the three downgradient monitoring wells at the Staging Area boundary and six further downgradient along the southern Site property line. The N&E wells are screened to directly above a stiff, highly plastic Clay, that is the confining layer for the uppermost aquifer, screened in the same zone as the Staging Area monitoring wells. Wells include 10 feet of screen length with total depths ranging from approximately 14 to 25 feet bgs. Depth to water measurements collected at the piezometers and monitoring wells as part of the N&E investigation confirmed the general southerly groundwater flow direction across the Site. The N&E investigation report entitled "Groundwater Characterization Report" is included as **Appendix A**. Locations of temporary piezometers, temporary and permanent monitoring well locations are shown on **Figure 1-3**.

Analytical results from the N&E wells (**Table I**) indicate that lithium, molybdenum and selenium concentrations are limited in their extent. While analytical results from monitoring wells directly adjacent to the Staging Area indicated concentrations of lithium, molybdenum, and selenium above GWPS in two of the three N&E wells, concentrations of lithium, molybdenum, and selenium in N&E wells located less than 200 feet down gradient and along the southern property boundary, are well below the GWPS and in most cases are even below the laboratory reporting limits. In other words, concentrations of lithium, molybdenum and selenium are not elevated beyond AES-PR's property boundary.





Pictured here and shown on Figure 2-1 wells with concentrations above GWPS are marked in red and those below GWPS are marked in black and white. Analytical results from the N&E wells were used to determine and assess corrective measures alternatives.



3. Risk Assessment and Exposure Evaluation

A "Groundwater Risk Evaluation" report has been prepared by Haley & Aldrich, as a companion to this CMA document, and is presented in **Appendix B**. A summary of this report is also available on the AES-PR CCR Rule website [http://aespuertorico.com/ccr/] — titled Summary Haley & Aldrich Groundwater Risk Evaluation. The purpose of the risk evaluation report is to provide the information needed to interpret and meaningfully understand the groundwater monitoring data collected and published for the Staging Area under the CCR Rule. In addition, AES-PR proactively took an additional step of evaluating potential groundwater-to-surface water transport and exposure pathways in the risk evaluation.

The risk evaluation report was completed by developing a CSM to identify the potential for human or ecological exposure to constituents that may have been released to the environment. The Staging Area is located at the ground surface and does not extend into the subsurface or the water table. Constituents present in the AGREMAX™ can be dissolved into infiltrating water (from precipitation and wetting for dust control) and those constituents may move through the subsurface and could then be present in shallow groundwater. Constituents could move with groundwater as it flows, usually in a downgradient/downhill direction. The general direction of groundwater flow at the Site is south/southwest toward Las Mareas Harbor.

Groundwater moves slowly through the rock and soils beneath the ground. Like surface water, it also moves from areas of high elevation to areas of low elevation and can move into adjacent surface water. Any potential release of constituents to groundwater from either the adjacent industrial sites or AES-PR will be limited in extent by the direction of groundwater flow and will not impact areas further inland.

There are no on-site users of shallow groundwater adjacent to AES-PR. As discussed in **Section 2.3** above, the CPCPRC is in Corrective Action overseen by USEPA. CPCPRC conducted a private well investigation as part of a sitewide risk characterization (CPCPRC, 2007) of the property immediately to the east of the AES-PR facility. As documented in the 2007 *CPCPRC Risk Characterization Report*, there are some census-designated communities and smaller villages near the CPCPRC and AES-PR facilities (Guayama, Quebrada, Corazon, Jobos and Puerto Jobos, and Barrancas), however none of these communities is considered downgradient (i.e., south of AES-PR and CPCPRC) and, therefore, would not be impacted by groundwater from either facility. Las Mareas is the only community downgradient of CPCPRC and potentially AES-PR, and according to the 2007 *CPCPRC Risk Characterization Report*, houses in Las Mareas obtain water from a public potable water pipeline and no existing private wells were found in the area. The 2007 CPCPRC Report also did not find any domestic wells constructed near the CPCPRC facility.

Thus, with respect to shallow groundwater, there are no users of the groundwater near the AES-PR facility. Depth to groundwater in this area is approximately 10 feet, thus, contact with groundwater during a short-term construction/excavation event is unlikely.

Analytical data from samples collected from groundwater monitoring wells and Las Mareas Harbor have been included in the risk evaluation. The samples have been analyzed for constituents that are commonly associated with CCR. However, it is recognized by the USEPA that all of these constituents can also be naturally occurring and can be found in rocks, soils, water and sediments; thus, the it is



necessary to understand what the naturally occurring background levels are for these constituents. The CCR Rule requires sampling and analysis of upgradient and/or background groundwater just for this reason. Groundwater samples have also been analyzed for volatile and semi-volatile organic compounds to evaluate groundwater impacts at AES-PR from the adjoining CPCPRC property to the east, as discussed above.

To answer the question, "Are the constituent concentrations high enough to potentially exert a toxic effect?" health risk-based screening levels were used for comparison to the data. Of the groundwater data collected, the majority – 94% – are below GWPS, i.e., below drinking water standards. There is no direct exposure to groundwater by human or ecological receptors.

The groundwater results from the CCR Rule monitoring wells were also compared to ecological screening levels for surface water. All results are below the ecological screening levels with the exception of the results for selenium for MW-3, which is located immediately downgradient of the Storage Area (see **Table 8** in **Appendix B**). Two important observations can be made for the comparison of the analytical results from the N&E investigation (data reported at the end of **Table I**). Only two of the wells (TW-102 and TW-103) have a concentration of selenium above the ecological screening level, and both of these wells are also immediately downgradient of the Staging Area (see **Figure 2-1**). All constituent concentrations in the additional N&E wells located less than 200 ft downgradient of the Staging Area, at the property boundary, are below the ecological screening levels.

There is a narrow marshy area between the Staging Area and the downgradient property boundary. While groundwater may have some flow component into the marshy area, the ecological screening level for selenium is based on fish reproduction, and that type of exposure is not applicable to a marshy area. The N&E well results indicate that constituents in groundwater are not moving off of the Site property at concentrations above GWPS or above the ecological screening levels. The nearest downgradient surface water body is Las Mareas Harbor.

The Las Mareas Harbor sample was compared to risk-based human recreational screening levels, to ecological screening levels, and to seawater results available from the scientific literature. There are no analytical results for the Las Mareas Harbor sample that are above marine ecological screening levels, and with the exception of arsenic no analytical results above human health recreational screening levels; however, the arsenic concentrations are comparable to seawater concentrations worldwide (in fact, arsenic concentrations I seawater worldwide are above the human health recreational screening level). Thus, the Las Mareas Harbor sample results do not show evidence of impact of constituents derived from AES-PR. This is important in that the absence of concentrations above risk-based screening levels means that there is not a significant pathway of exposure.

In addition, a surface water dilution and attenuation factor (SW-DAF) was derived for groundwater that may flow to the Caribbean Sea at Las Mareas Harbor; the conservatively calculated SW-DAF is 1,300 (a unitless value). When the SW-DAF is applied to the lowest conservative risk-based screening level for marine surface water, the results indicate that groundwater concentrations at the Staging Area could be an order or more magnitude higher before an adverse impact on Las Mareas Harbor could occur.

More importantly, the analytical results from the N&E groundwater monitoring wells located at the property boundary – less than 200 feet downgradient from the CCR Rule wells, which are located directly adjacent to the Staging Area – demonstrate that there are no concentrations of the SSL



constituents above GWPS in these wells. In other words, concentrations of lithium, molybdenum and selenium are not elevated beyond AES-PR's property boundary.

This evaluation demonstrates that the impacts of the Staging Area are limited and do not extend beyond the AES-PR property boundary. There is no impact on drinking water and there is no evidence of impact to human health or the environment. There are no downgradient users of groundwater as drinking water – thus, there is no impact on drinking water. Las Mareas Harbor does not show impacts. There is no exposure to CCR-derived constituents detected in groundwater at the AES-PR facility – either via groundwater use or surface water. Even for the very few results that may be above screening values for some of the groundwater sampling events, there is no complete drinking water exposure pathway to groundwater. Where there is no exposure, there is no risk.

Therefore, because no adverse risk currently exists, any of the remedies considered in this CMA are all protective of human health and the environment, and implementation of any of the remedial alternatives will not result in a meaningful reduction in risk to groundwater-related exposures or risk.



4. Corrective Measures Alternatives

4.1 CORRECTIVE MEASURES ASSESSMENT GOALS

As noted in §257.96(a), within 90 days of detecting Appendix IV SSLs, "the owner or operator must initiate an assessment of corrective measures to prevent further releases, to remediate any releases and to restore affected area to original conditions". The corrective measures evaluation that is discussed below and in subsequent sections provides an analysis of the effectiveness of five potential corrective measures in meeting the requirements and objectives of remedies as described under §257.97 (also shown on **Table II**). Additional remedial alternatives were considered but were determined to not be viable for remediating groundwater at the Staging Area. By meeting these requirements, this assessment also meets the requirements promulgated in §257.96 for the balancing criteria (provided in more detail in **Section 1.3**) which includes an evaluation of:

- The performance, reliability, ease of implementation, and potential impacts of appropriate
 potential remedies, including safety impacts, cross-media impacts, and control of exposure to
 residual contamination;
- The time required to complete the remedy; and
- The institutional requirements, such as state or local permit requirements or other environmental or public health requirements that may substantially affect implementation of the remedy.

The criteria listed above are included in the balancing criteria considered during the corrective measures evaluation, described in **Section 5**.

4.2 GROUNDWATER FATE AND TRANSPORT MODELING

Groundwater at the Site was modeled utilizing Groundwater Vista Version 7 for flow and solute transport. The model was constructed, calibrated, and subsequent simulations run to evaluate remedy alternatives for Appendix IV constituents above the GWPS. Site-specific parameters (i.e., groundwater elevations and hydraulic conductivity) were utilized for model preparation. MODFLOW 2005, a finite difference three-dimensional solver, was utilized for groundwater flow estimation. Modeled groundwater elevations were compared to observed values from the on-site well network to achieve a calibration of less than 10% scaled root mean squared of measured water levels. Once groundwater flow was calibrated in the model, solute transport was completed using MT3DMS, a three-dimensional solute transport modeling program. Parameters affecting transport such as advection, diffusion, dispersion, and adsorption are utilized within the MT3DMS package to estimate solute transport within the model domain.

The calibrated flow models were used to simulate the different remediation alternatives and the effects they have on groundwater quality through time. These simulations are incorporated into the discussion on remediation alternatives provided below.

4.3 CORRECTIVE MEASURES ALTERNATIVES

Corrective measures are considered complete when constituent concentrations in groundwater impacted by the Staging Area are no longer above the Appendix IV GWPS for three consecutive years of



groundwater monitoring. In accordance with §257.97, the groundwater corrective measures being considered must meet, at a minimum, the following threshold criteria (provided in more detail in **Section 1.3**):

- 1. Be protective of human health and the environment;
- 2. Attain the GWPS as specified pursuant to §257.95(h);
- 3. Control the source(s) of releases so as to reduce or eliminate, to the maximum extent feasible, further releases of constituents in Appendix IV to this part into the environment;
- 4. Remove from the environment as much of the contaminated material that was released from the CCR unit as is feasible, taking into account factors such as avoiding inappropriate disturbance of sensitive ecosystems; and
- 5. Comply with standards (regulations) for management of waste as specified in §257.98(d).

Each of the remedial alternatives assembled in this CMA meet the requirements of the threshold criteria listed above.

Each of the five remedial alternatives assume continued operation of the Staging Area.

4.3.1 Alternative 1: Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)

This alternative involves the prevention of AGREMAX™ contact with the ground via installation of a synthetic liner in the Staging Area. Passive treatment of groundwater would occur via natural geochemical processes which will reduce concentrations of CCR-derived constituents in groundwater, referred to as monitored natural attenuation, or MNA. This liner alternative would prevent the future potential release of CCR constituents during continued use of the Staging Area.

As stated, lining the Staging Area would reduce infiltration of surface water to groundwater thereby isolating source material. The volume of AGREMAX™ would be reduced to allow for installation of the liner in two phases. All AGREMAX™ contact with the ground would be eliminated as no AGREMAX™ would remain in contact with ground following installation of the liner. Liner installation can be completed safely, in compliance with applicable federal and state regulations, and be protective of public health and the environment. The liner would be a composite/synthetic system consisting of (from bottom to top) a geosynthetic clay liner overlaid with geomembrane, a geocomposite drainage layer, a protective layer, and lastly a dye layer⁴. Liner installation is expected to be completed in two phases. Phase 1 would involve lining one half of the Staging Area and would necessitate removal of all AGREMAX™ from that half of the area while product would remain on the Phase 2 area. During Phase 2 liner installation, the remaining AGREMAX™ would be moved to the completed/lined Phase 1 area. The liner would be installed within the current footprint of the Staging Area. Following liner installation, AGREMAX™ could be managed anywhere within the lined Staging Area.

MNA is a viable remedial technology recognized by both state and federal regulators that is applicable to inorganic compounds in groundwater. The USEPA defines MNA as "the reliance on natural attenuation processes to achieve site-specific remediation objectives within a time frame that is reasonable compared to that offered by other more active methods." The "natural attenuation processes" that are at work in such a remediation approach include a variety of physical, chemical, or

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⁴ The dye layer is used to alert workers in the area that movement of material or excavation should not occur below the dye layer to maintain the integrity of the liner system.

biological processes that, under favorable conditions, act without human intervention to reduce the mass, toxicity, mobility, volume, or concentration of contaminants in soil or groundwater. These in-situ processes may include biodegradation; dispersion; dilution; sorption; volatilization; radioactive decay; and chemical or biological stabilization, transformation, or destruction of contaminants depending on the constituent (USEPA, 2015). When combined with the prevention of the AGREMAX™ contact with the ground and installation of a synthetic liner to address the source by limiting the infiltration of precipitation into and through the CCR, MNA can reduce concentrations of lithium, molybdenum, and selenium in groundwater at the Staging Area.

4.3.2 Alternative 2 – Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment

This alternative involves long-term downgradient pumping of groundwater to hydraulically control downgradient migration of Appendix IV constituents in groundwater, with treatment of pumping system effluent in the existing plant wastewater treatment system and MNA for groundwater downgradient of the Staging Area. This alternative would rely strictly on groundwater pumping wells to control the downgradient migration of Appendix IV constituents in groundwater. The groundwater pumped to maintain hydraulic control would be piped to the existing plant RO treatment system. Based on review of system specifications provided by AES-PR and the report from AES-PR personnel, the primary RO system is currently not in use and could provide treatment capacity with some limited plumbing and limited system modifications.

Implementation of a hydraulic containment (HC) system would require a detailed design effort with bench scale testing to verify groundwater treatment by the existing treatment facility. Pilot testing, such as pumping tests and additional groundwater modeling, would be needed to verify the hydraulic capture zone.

Following the installation of the groundwater pumping well network and connection to the existing RO treatment system, AES-PR would implement activities that include operation and maintenance (O&M) of the HC system, long-term groundwater sampling to monitor HC system and MNA performance, and water treatment system performance monitoring.

4.3.3 Alternative 3 – Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation

This alternative involves long-term downgradient pumping of groundwater to hydraulically control downgradient migration of Appendix IV constituents in groundwater, with direct discharge of pumping system effluent to the coal pile runoff pond and MNA for groundwater downgradient of the Staging Area. The groundwater pumped to maintain hydraulic control would be conveyed to the coal pile runoff pond or used for AGREMAX™ dust suppression (no additional treatment is planned for this alternative).

Implementation of a HC system would require a detailed design effort with pilot testing, such as pumping tests and additional groundwater modeling, to verify the hydraulic capture zone. Following the installation of the groundwater pumping well network and associated pipework, AES-PR would implement activities that include O&M of the HC system, long-term groundwater sampling to monitor HC system and MNA performance, and long-term groundwater elevation monitoring to confirm HC system performance.



4.3.4 Alternative 4 – Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment

This alternative involves low-permeability barrier wall installation and long-term pumping of groundwater to hydraulically control downgradient migration of Appendix IV constituents in groundwater, with treatment of pumping system effluent in the existing plant treatment system, and MNA for groundwater downgradient of the Staging Area. This alternative would rely on a combination of a partial barrier wall, keyed into the underlying clay unit, and groundwater pumping wells upgradient of the barrier wall to control the downgradient migration of Appendix IV constituents in groundwater. Groundwater pumped to maintain hydraulic control would be piped to the existing RO treatment system.

Implementation of a HC system would require a detailed design effort with bench scale testing to verify groundwater treatment by the existing treatment facility. Pilot testing, such as pumping tests and additional groundwater modeling, would be needed to verify the hydraulic capture zone. A detailed design would also be required for the barrier wall.

Following the installation of the groundwater pumping well network, connection to the existing RO treatment system, and barrier wall installation, AES-PR would implement activities that include O&M of the HC system, long-term groundwater sampling to monitor HC system performance and MNA performance, and water treatment system performance monitoring.

4.3.5 Alternative 5 – Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation

This alternative involves low-permeability barrier wall installation and long-term pumping of groundwater to hydraulically control downgradient migration of Appendix IV constituents in groundwater, and MNA for groundwater downgradient of the Staging Area. This alternative would rely on a combination of a partial barrier wall, keyed into the underlying clay unit, and groundwater pumping wells upgradient of the barrier wall to control the downgradient migration of Appendix IV constituents in groundwater. The groundwater pumped to maintain hydraulic control would be conveyed to the coal pile runoff pond or used for AGREMAX™ dust suppression (similar to Alternative 3, no additional treatment is planned).

Implementation of a HC system would require a detailed design effort with pilot testing, such as pumping tests and additional groundwater modeling, to verify the hydraulic capture zone. A detailed design would also be required for the barrier wall. Following the installation of the groundwater pumping well network and associated pipework, and barrier wall, AES-PR would implement activities that include O&M of the HC system and long-term groundwater elevation monitoring to confirm HC system performance.



5. Comparison of Corrective Measures Alternatives

The purpose of this section is to evaluate, compare, and rank the five corrective measures alternatives using the balancing criteria described in §257.97.

5.1 EVALUATION/BALANCING CRITERIA

In accordance with §257.97, remedial alternatives that satisfy the threshold criteria are then compared to four balancing (evaluation) criteria. The balancing criteria allow a comparative analysis for each corrective measure, thereby informing the final corrective measure selection. The four balancing criteria include the following (provided in more detail in **Section 1.3**):

- 1. The long- and short-term effectiveness and protectiveness of the potential remedy(s), along with the degree of certainty that the remedy will prove successful;
- 2. The effectiveness of the remedy in controlling the source to reduce further releases;
- 3. The ease or difficulty of implementing a potential remedy; and
- 4. The degree to which community concerns are addressed by a potential remedy.

The degree to which community concerns are addressed by the potential remedies will be considered following a public information session to discuss the results of the corrective measures assessment with interested and affected parties and will be held at least 30 days prior to remedy selection in accordance with 257.96(e).

5.2 COMPARISON OF ALTERNATIVES

This section compares the alternatives to each other based on evaluation of the balancing criteria listed above. Each of the balancing criteria consists of several sub criteria listed in the CCR Rule (provided in more detail in **Section 1.3**), which have been considered in this assessment. The goal of this analysis is to evaluate the alternatives based on whether each is technologically feasible, relevant and readily implementable, provides adequate protection to human health and the environment, and minimizes impacts to the community as compared to the other alternatives. A summary of remedial alternatives is provided in **Table III**.

A graphic is provided within each subsection below to provide a visual snapshot of the favorability of each alternative, where green represents "most favorable", yellow represents "less favorable", and red represents "least favorable."

Each of the five remedial alternatives evaluated here assume continued operation of the Staging Area. Moreover, the analytical results from the N&E wells (**Table I**) indicate that lithium, molybdenum, and selenium concentrations are limited in their extent, and in fact do not extend to the nearby southern property boundary.

5.2.1 Balancing Criteria 1 - The Long- and Short-Term Effectiveness and Protectiveness of the Potential Remedy, along with the Degree of Certainty that the Remedy Will Prove Successful

This balancing criterion takes into consideration the following sub criteria relative to the long-term and short-term effectiveness of the remedy, along with the anticipated success of the remedy.



5.2.1.1 Magnitude of reduction of existing risks

As summarized in **Section 3** and further confirmed by the results of the N&E evaluation the Staging Area does not pose a risk to human health and the environment. Therefore, the remedial alternatives considered are not necessary to reduce an assumed risk posed by Appendix IV constituents in groundwater because no such adverse risk exists. However, other types of impacts and risks (i.e., the risk of implementing the remedies sometimes referred to as "risk of remedy") can be posed by implementation of the remedial alternatives considered here.

Each of the five remedial alternatives assume continued operation of the Staging Area. The activities associated with Alternative 1 (prevention of AGREMAX™ ground contact, subsequent lining of the Staging Area for placement of material in the future, combined with MNA) are routine, and consistent with current practices. Therefore, relative to risk of remedy, the alternatives are considered equivalent.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 1 - Subcriteria i) Magnitude of reduction of risks				

5.2.1.2 Magnitude of residual risks in terms of likelihood of further releases due to CCR remaining following implementation of a remedy

Alternative 1 (Lining with MNA) has the lowest long-term residual risk in that prevention of AGREMAX™ ground contact eliminates the source and lining of the Staging Area with a synthetic liner system reduces the likelihood of future releases to groundwater. Therefore, Alternative 1 is considered the most favorable. For Alternatives 2 and 3 (HC with and without ex-situ treatment, respectively), dissolved phase Appendix IV constituents in groundwater are addressed through hydraulic containment and MNA, while Alternatives 4 and 5 (HC with a barrier wall, with and without ex-situ treatment, respectively and MNA) incorporate the use of a subsurface barrier wall to further impede downgradient migration of groundwater and avoid salt water intrusion. Since Alternatives 2 through 5 do not remove the source and do not include the use of a low-permeability liner to isolate the Staging Area in the future, a slightly greater residual risk of further release exists, and these four alternatives are considered less favorable than Alternative 1.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Rarrier Wall and
Category 1 - Subcriteria ii) Magnitude of residual risk in terms of likelihood of further release				



5.2.1.3 The type and degree of long-term management required, including monitoring, operation, and maintenance

Alternative 1 (Lining with MNA) is the most favorable alternative with respect to this criterion because it requires the least amount of long-term management and involves no mechanical systems as part of the remedy. Alternatives 2 through 5, which all include active hydraulic containment, are less favorable since they require mechanical systems (well pumps and/or treatment system) long-term until the GWPS is attained.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 1 - Subcriteria iii) Type and degree of long-term management required				

5.2.1.4 Short-term risks that might be posed to the community or the environment during implementation of such a remedy

Each of the five remedial alternatives assume continued operation of the AGREMAX™ Staging Area. Therefore, relative to short-term risks to the community or environment, each alternative is considered equivalent.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Barrier Wall and
Category 1 - Subcriteria iv) Short term risk to community or environment during implementation				

5.2.1.5 Time until full protection is achieved

There is no complete drinking water exposure pathway to groundwater. Where there is no exposure, there is no risk. Therefore, protection is already achieved. Alternatives 2 through 5 all include hydraulic containment and are anticipated to take a similar period of time until natural attenuation and active pumping reduce Appendix IV constituents to GWPS concentrations. These four alternatives are considered equally favorable due to the similar timeframes. Alternative 1 (Lining with MNA) is considered less favorable since the time period to achieve the GWPS is predicted to be slightly longer than Alternatives 2 through 5.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Rarrier Wall and
Category 1 - Subcriteria v) Time until full protection is achieved				



5.2.1.6 Potential for exposure of humans and environmental receptors to remaining wastes, considering the potential threat to human health and the environment associated with excavation, transportation, re-disposal, or containment

Alternatives 1 (Lining with MNA), 3 (HC with no treatment), and 5 (HC with no treatment, with barrier wall) all have similar, minimal potential for exposure to humans and environmental receptors during monitoring well system installation; and installation of the barrier wall and/or HC system, respectively. No groundwater treatment is used for Alternatives 3 and 5, therefore a concentrated waste stream and spent treatment media are not produced. These three alternatives are considered most favorable relative to potential exposure to humans and environmental receptors.

Alternatives 2 (HC with treatment) and 4 (HC with treatment and barrier wall) are considered less favorable since a concentrated waste stream will be generated and spent treatment/filtration media may need to be transported off-site for disposal, which creates a potential for exposure during the operation period.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Barrier Wall and
Category 1 - Subcriteria vi) Potential for exposure of humans and environmental receptors to remaining wastes				

5.2.1.7 Long-term reliability of the engineering and institutional controls

Alternative 1 (Lining with MNA) includes Staging Area lining and long-term monitoring which are common methods for long-term waste management. Hydraulic containment (Alternatives 2 through 5) is considered proven technology and would have high long-term reliability but relies on mechanical systems to attain GWPS. Alternative 1 (Lining with MNA) is considered the most favorable because no additional ongoing operations and maintenance (O&M) would be needed, other than periodic groundwater sampling and verification of decreasing concentrations since the liner system is a reliable technology.

Alternatives 4 (HC with treatment and barrier wall) and 5 (HC with no treatment, with barrier wall) are considered reliable, but less favorable when compared to Alternative 1 since they both rely on mechanical systems such as pumps, pipework, etc. Alternatives 2 (HC with treatment) and 3 (HC with no treatment) are considered the least favorable since they both rely on mechanical systems to operate, and uncertainty is introduced since a barrier wall is not included to improve pumping efficiency and avoid saltwater intrusion at the pumping wells. Saltwater intrusion at the pumping wells would not only create corrosion issues but would reduce the reliability/operability of the treatment system (Alternative 2) or ability to directly discharge the pumping effluent (Alternative 3) to the coal pile runoff pond.

For all alternatives, institutional controls, such as recording of an environmental covenant restricting the use of groundwater can easily be implemented because the AGREMAX™ Staging Area is located on property owned by AES.



	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 1 - Subcriteria vii) Long-term reliability of engineering and institutional controls				

5.2.1.8 Potential need for replacement of the remedy

Prevention of AGREMAX™ ground contact by installation of a synthetic liner at the Staging Area (Alternative 1) is considered permanent and is expected to be effective. Also lining the Staging Area will isolate AGREMAX™ from groundwater in the future, Alternative 1 is considered the most favorable.

Since Alternatives 2 and 3 (HC with and without treatment, respectively) rely on groundwater pumping to achieve the GWPS, and the pumping wells may be susceptible to saltwater intrusion, these alternatives are considered the least favorable. Alternatives 4 and 5 (HC with and without treatment, respectively, plus a barrier wall) include a secondary remedial technology to contain groundwater and reduce the likelihood of saltwater intrusion, these alternatives are considered more favorable than Alternatives 2 and 3, but less favorable than Alternative 1 (Lining with MNA).

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 1 - Subcriteria viii) Potential need for replacement of the remedy				

5.2.1.9 Long- and short-term effectiveness and protectiveness criterion summary

The following graphic provides a summary of the long- and short-term effectiveness and protectiveness of the potential remedy, along with the degree of certainty that the remedy will prove successful. Alternative 1 (Lining with MNA) is the most favorable. There is a similar timeframe for all alternatives to meet the GWPS, with the timeline for Alternative 1 being slightly longer than Alternatives 2 through 5 which include active pumping. Alternative 1 (Lining with MNA) does not include additional treatment technology aside from MNA and, therefore, long-term management requirements are minimal. Alternative 1 (Lining with MNA) does not rely on mechanical systems aside from low permeability lining. Alternatives 2 (HC with treatment) and 4 (HC with treatment and barrier) provide groundwater treatment but require additional long-term operation and maintenance and will generate a secondary waste stream. Alternatives 2 (HC with treatment) and 3 (HC with no treatment) are considered the least favorable since the long-term reliability is uncertain due to the absence of a barrier wall and have the greatest potential for needing replacement.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
CATEGORY 1 Long- and Short Term Effectiveness, Protectiveness, and Certainty of Success				



5.2.2 Balancing Criteria 2 - The Effectiveness of the Remedy in Controlling the Source to Reduce Further Releases

This balancing criterion takes into consideration the ability of the remedy to control a future release, and the extensiveness of treatment technologies that will be required.

5.2.2.1 The extent to which containment practices will reduce further releases

For remedial Alternative 1, installation of the liner system will minimize infiltration of precipitation and decrease/prevent the flux of Appendix IV constituents to groundwater by creating a physical barrier in the future. The construction period to place the liner is expected to be short-term. Alternatives 4 and 5 (HC with treatment and no treatment, respectively, and barrier wall) are expected to effectively control the down-gradient migration of groundwater through groundwater pumping and the subsurface low-permeability barrier wall. These three alternatives (Alternatives 1, 4, and 5) are considered most favorable for reducing further releases.

Alternatives 2 and 3 (HC with treatment and no treatment, respectively) are considered less favorable since these two alternatives rely on groundwater pumping only. Without a barrier wall, the ability to control the down-gradient migration of groundwater, and to avoid saltwater intrusion, is less certain.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Rarrier Wall and
Category 2 - Subcriteria i) Extent to which containment practices will reduce further releases				

5.2.2.2 The extent to which treatment technologies may be used

No groundwater treatment technologies, other than natural attenuation, will be used for Alternative 1 (Lining with MNA). There would be no ongoing operation and maintenance of a treatment technology, other than periodic groundwater monitoring. Alternative 3 (HC with no treatment) relies only on groundwater pumping with no treatment. Therefore, Alternatives 1 and 3 are considered the most favorable since the remedial approaches are the least complex.

Alternatives 2 (HC with treatment), 4, (HC with treatment and barrier wall), and 5 (HC with no treatment and barrier wall) use additional technologies, which increases complexity and reliance on engineering controls. Therefore, these three Alternatives are considered less favorable when compared to Alternatives 1 and 3.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 2 Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 2 - Sub criteria ii) Extent to which treatment technologies may be used					



5.2.2.3 Effectiveness of the remedy in controlling the source to reduce further releases summary

The graphic below provides a summary of the effectiveness of the remedial alternatives to control the source to reduce further releases. Alternative 1 (Lining with MNA) is considered the most favorable since prevention of ground contact and isolation of the AGREMAX™ is expected to be effective at controlling future releases and does not rely on active containment or treatment technology. Alternatives 2 through 5 are all expected to be effective at controlling the source to reduce a further release, but all four alternatives rely on mechanical systems and are considered less favorable when compared to Alternative 1.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 2 Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
CATEGORY 2 Effectiveness in controlling the source to reduce further releases					

5.2.3 Balancing Criteria 3 - The Ease or Difficulty of Implementing a Potential Remedy

This balancing criterion takes into consideration technical and logistical challenges required to implement a remedy, including practical considerations such as equipment availability and disposal facility capacity.

5.2.3.1 Degree of difficulty associated with constructing the technology

Installation of the hydraulic containment system considered under Alternatives 2 (HC with treatment) and 3 (HC with no treatment) is considered straightforward and readily constructible. Alternative 2 (HC with treatment) will utilize the existing treatment system, therefore, no additional difficulty is anticipated. Due to the ease of construction, Alternatives 2 (HC with treatment) and 3 (HC with no treatment) are considered the most favorable.

Installation of the hydraulic containment system considered under Alternatives 4 (HC with treatment and barrier wall) and 5 (HC with no treatment, with barrier wall) are also considered straightforward, however these two alternatives also include the installation of a low-permeability subsurface barrier wall. Relative to Alternatives 2 and 3, Alternatives 4 and 5 are considered less favorable due to the additional complexity of installing the barrier wall.

While the Alternative 1 is considered readily constructible, it is considered less favorable than Alternatives 2 and 3.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
Category 3 - Subcriteria i) Degree of difficulty associated with constructing the technology				



5.2.3.2 Expected operational reliability of the technologies

Alternative 1 (Lining with MNA) includes Staging Area lining and long-term monitoring which are common methods for long-term waste management. Hydraulic containment (Alternatives 2 through 5) are considered proven technologies and would have high long-term reliability but rely on mechanical systems to attain GWPS. Alternative 1 (Lining with MNA) is considered the most favorable because no additional ongoing O&M would be needed, other than periodic groundwater sampling and verification of decreasing concentrations.

Alternatives 4 (HC with treatment and barrier wall) and 5 (HC with no treatment and barrier wall) are considered reliable, but less favorable when compared to Alternative 1 since they both rely on mechanical systems such as pumps, pipework, etc. Alternatives 2 (HC with treatment) and 3 (HC with no treatment) are considered the least favorable since they both rely on mechanical systems to operate, and uncertainty is introduced since a barrier wall is not included to improve pumping efficiency and avoid salt water intrusion at the pumping wells. Saltwater intrusion at the pumping wells would not only create corrosion issues but would reduce the reliability/operability of the treatment system (Alternative 2) or ability to directly discharge the pumping effluent (Alternative 3).

For all alternatives, institutional controls, such as recording of an environmental covenant restricting the use of groundwater, can easily be implemented because the AGREMAX™ Staging Area is located on property owned by AES.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Barrier Wall and
Category 3 - Subcriteria ii) Expected operational reliability of the technologies				

5.2.3.3 Need to coordinate with and obtain necessary approvals and permits from other agencies

Alternatives 4 (HC with treatment and barrier wall) and 5 (HC with no treatment, with barrier wall) are considered the most favorable since inclusion of the barrier wall is expected to reduce the groundwater pumping rate to maintain hydraulic control. While permitting will be required, including permitting for barrier wall construction, the groundwater withdrawal will be minimized to the extent practicable. Relative to Alternatives 4 and 5, Alternatives 2 (HC with treatment) and 3 (HC with no treatment) are considered less favorable due to the higher pumping rate that will be needed to maintain hydraulic control.

Alternative 1 (Lining with MNA) may require permits for liner system construction. Therefore, relative to Alternatives 4 and 5, Alternative 1 is also considered less favorable.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Rarrier Wall and
Category 3 - Subcriteria iii) Need to coordinate with and obtain necessary approvals and permits from other agencies				



5.2.3.4 Availability of necessary equipment and specialists

For all alternatives, construction equipment is readily available, and specialists are not anticipated. Therefore, the alternatives are considered equally favorable.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Rarrier Wall and
Category 3 - Subcriteria iv) Availability of necessary equipment and specialists				

5.2.3.5 Available capacity and location of needed treatment, storage, and disposal services

Alternatives 2 through 5, which include hydraulic containment, are considered the most favorable since the AGREMAX[™] Staging Area continues to operate without modification or interruption. Pumping well effluent will either be discharged to the coal pile runoff pond (Alternatives 3 and 5) or treated on-site using the existing RO system (Alternatives 2 and 4). Alternative 1 (Lining with MNA) is considered less favorable since it will require additional management of AGREMAX[™] during the phase liner system construction.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 2 Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Barrier Wall and
Category 3 - Subcriteria v) Available capacity and location of needed treatment, storage, and disposal services					

5.2.3.6 Ease or difficulty of implementation summary

The color ribbon below provides a summary of the ease or difficulty that will be needed to implement each alternative. Alternatives 4 (HC with treatment and barrier wall) and 5 (HC with no treatment, with barrier wall) are the most favorable, while Alternatives 1 (Lining with MNA), 2 (HC with treatment) and 3 (HC with no treatment) are less favorable for various degrees of difficulty in implementing the remedy.

	Alternative 1 Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ MNA	Alternative 3 Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	Alternative 4 Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	
CATEGORY 3 Ease of implementation				



6. Summary

This Corrective Measures Assessment has evaluated the following alternatives:

- Alternative 1: Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)
- Alternative 2: Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment
- Alternative 3: Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation
- Alternative 4: Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment
- Alternative 5: Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation

In accordance with §257.97, each of these alternatives has been confirmed to meet the following threshold criteria:

- Be protective of human health and the environment;
- Attain the GWPS;
- Control the source(s) of releases so as to reduce or eliminate, to the maximum extent feasible, further releases of constituent of concerns to the environment;
- Remove from the environment as much of the contaminated material that was released from the CCR unit as is feasible, considering factors such as avoiding inappropriate disturbance of sensitive ecosystems; and
- Comply with standards (regulations) for waste management.

In addition, in accordance with §257.96, each of the alternatives has been evaluated in the context of the following balancing criteria:

- The long- and short-term effectiveness and protectiveness of the potential remedy(s), along with the degree of certainty that the remedy will prove successful;
- The effectiveness of the remedy in controlling the source to reduce further releases;
- The ease or difficulty of implementing a potential remedy; and
- The degree to which community concerns are addressed by a potential remedy.

This Corrective Measures Assessment, and the input received during the public comment period, will be used to identify and select a final corrective measure for implementation at the AES-PR Staging Area.



References

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- 5. USEPA. 2017. Statement of Basis Final Remedy Decision, Chevron Phillips Chemical, Puerto Rico Core, LLC Guayama, Puerto Rico. EPA ID Number: PRD991291972.

				Revision Log					
Date	Page No.	Section	Description	September 2019 Text	Revised Text				
11/1/2019	7	2.5	Correction	While analytical results from monitoring wells directly adjacent to the Staging Area indicated concentrations of lithium, molybdenum, and selenium above GWPS in two of the three N&E wells, concentrations of lithium, molybdenum, and selenium in N&E wells located only 100 feet down gradient and along the southern property boundary, are well below the GWPS and in most cases are even below the laboratory reporting limits.	While analytical results from monitoring wells directly adjacent to the Staging Area indicated concentrations of lithium, molybdenum, and selenium above GWPS in two of the three N&E wells, concentrations of lithium, molybdenum, and selenium in N&E wells located less than 200 feet down gradient and along the southern property boundary, are well below the GWPS and in most cases are even below the laboratory reporting limits.				
11/8/2019	Арр	endix A	Updated Appendix A with Amended Version	See description in Amended Appendix A – Groundwater Characterization Report. No additional revisions to CMA required.					

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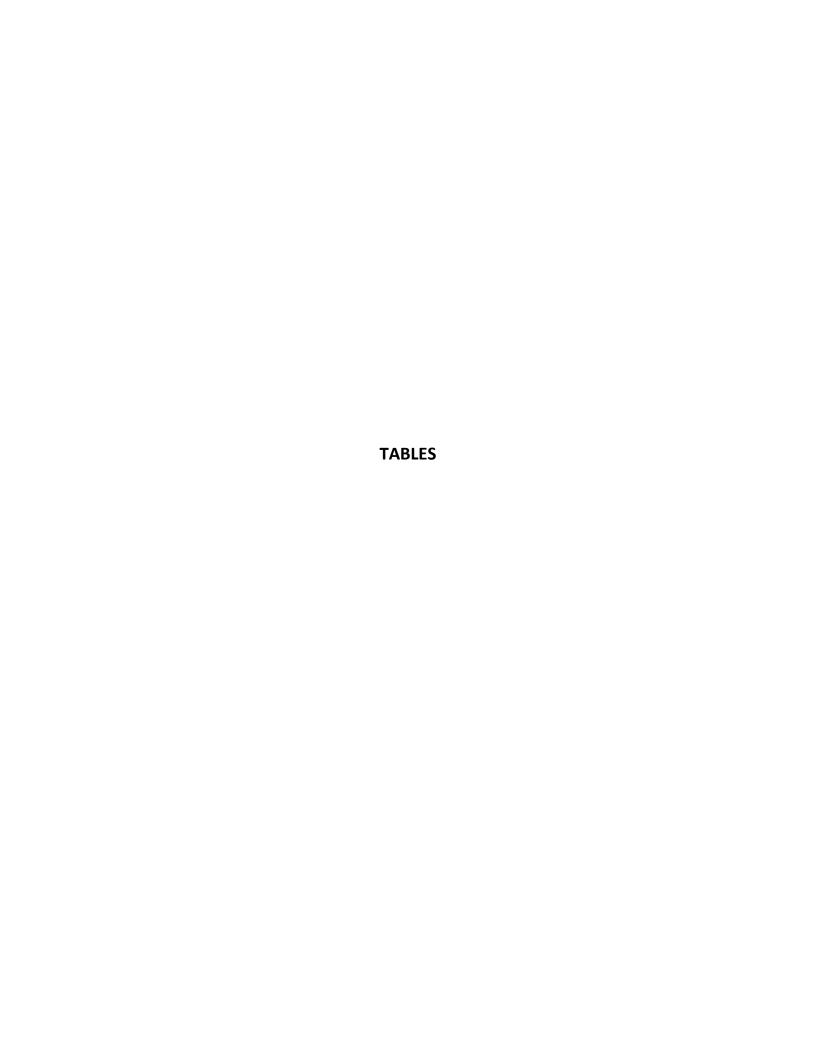


TABLE I
GROUNDWATER ANALYTICAL RESULTS - APPENDIX IV CONSTITUENTS
CORRECTIVE MEASURES ASSESSMENT
AES PUERTO RICO - AGREMAX STAGING AREA
GUAYAMA, PUERTO RICO

		GWPS	0.006	0.010	2	0.004	0.005	0.1	0.006	4	0.015	0.040	0.002	0.100	0.05	0.002	5
WELL ID	Event		_	_	Davis see					Fluorido	_						Da dium 226/229
		Sampling Date	Antimony mg/l	Arsenic mg/l	Barium mg/l	Beryllium mg/l	Cadmium mg/l	Chromium mg/l	Cobalt mg/l	Fluoride mg/l	Lead mg/l	Lithium mg/l	Mercury mg/l	Molybdenum mg/l	Selenium mg/l	Thallium mg/l	Radium 226/228 pCi/L
MW-1	1	8/8/17	0.0010 U	0.00046 U	0.050	0.00034 U	0.00034 U	0.0011 U	0.00058 J	0.47	0.00035 U	0.0032 U	0.000070 U	0.0022 J	0.0073	0.000085 U	0.0899 U
MW-2	1	8/8/17	0.0010 U	0.00046 U	0.10	0.00034 U	0.00034 U	0.0011 U	0.00038 J	0.47	0.00035 U	0.0032 U	0.000070 U	0.0022 J 0.00085 U	0.0073 0.00035 J	0.000085 U	0.129 U
MW-3	1	8/8/17	0.0010 U	0.0038	0.33	0.00034 U	0.00034 U	0.0011 U	0.0018 J	2.0	0.00035 U	0.0032 0	0.000070 U	0.096	0.0052	0.000085 U	0.272 U
MW-4	1	8/8/17	0.0010 U	0.0036	0.057	0.00034 U	0.00034 U	0.0011 U	0.0018 J	0.63	0.00035 U	1.0	0.000070 U	0.090	0.032	0.000085 U	0.527
MW-4	1	8/8/17	0.0010 U		0.057	0.00034 U	0.00036 J			0.61	0.00035 U	1.0		0.44	0.011	0.000085 U	
MW-5	1	8/9/17	0.0014 J	0.0031	0.037	0.00034 U	0.00034 U	0.0011 U 0.0011 U	0.0017 J 0.0034	0.61	0.00035 U	0.0032 U	0.000070 U 0.000070 U	0.43 0.0022 J	0.011	0.000085 U	0.381
10100-3	1	0/3/17	0.0010 0	0.0032	0.041	0.00034 0	0.00034 0	0.0011 0	0.0034	0.42	0.00033 0	0.0032 0	0.000070 0	0.00223	0.010	0.000083 0	0.475
MW-1	2	8/15/17	0.0010 U	0.00055 J	0.056	0.00034 U	0.00034 U	0.0011 U	0.00055 J	0.53	0.00035 U	0.0032 U	0.000070 U	0.00085 U	0.0062	0.000085 U	0.349 U
MW-2	2	8/15/17	0.0010 U	0.00047 J	0.11	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.40	0.00035 U	0.0032 U	0.000070 U	0.00085 U	0.00024 U	0.000085 U	0.614
MW-3	2	8/15/17	0.0010 U	0.0034	0.29	0.00034 U	0.00034 U	0.0011 U	0.0019	2.1	0.00035 U	0.0077	0.000070 U	0.16	0.098	0.000085 U	0.417
MW-4	2	8/16/17	0.0010 U	0.0037	0.060	0.00034 U	0.00034 U	0.0011 U	0.0017	0.63	0.00035 U	1.1	0.000070 U	0.40	0.0048	0.000085 U	0.367 U
MW-4	2	8/16/17	0.0010 U	0.0033	0.060	0.00034 U	0.00034 U	0.0011 U	0.0016	0.61	0.00035 U	1.1	0.000070 U	0.38	0.0061	0.000085 U	0.600
MW-5	2	8/16/17	0.0010 U	0.0024	0.043	0.00034 U	0.00034 U	0.0011 U	0.0035	0.45	0.00035 U	0.0047 J	0.000070 U	0.0086 J	0.013	0.000085 U	0.576
MW-1	3	8/22/17	0.0010 U	0.00046 U	0.058	0.00034 U	0.00034 U	0.0011 U	0.00068 J	0.55	0.00035 U	0.0032 U	0.000070 U	0.0023 J	0.0065	0.000085 U	0.533
MW-2	3	8/22/17	0.0010 U	0.00046 U	0.11	0.00031 U	0.00034 U	0.0011 U	0.00040 U	0.40	0.00035 U	0.0032 U	0.000070 U	0.0010 J	0.00061 J	0.000085 U	-0.0403 U
MW-3	3	8/22/17	0.0010 U	0.0021	0.37	0.00034 U	0.00034 U	0.0011 U	0.0023 J	2.2	0.00035 U	0.0075	0.000070 U	0.2	0.13	0.000085 U	0.231 U
MW-4	3	8/23/17	0.0010 U	0.0026	0.057	0.00034 U	0.00034 U	0.0011 U	0.0017 J	0.65	0.00035 U	0.88 0.000070 U		0.44	0.0060	0.000085 U	0.0815 U
MW-4	3	8/23/17	0.0010 U	0.0025	0.058	0.00034 U	0.00034 U	0.0011 U	0.0017 J	0.65	0.00035 U	1.1	0.000070 U	0.38	0.0065	0.000085 U	0.441
MW-5	3	8/22/17	0.0010 U	0.0018	0.039	0.00031 U	0.00031 U	0.0011 U	0.0036	0.46	0.00035 U	0.0044 J	0.000070 U	0.0080 J	0.014	0.000085 U	0.391 U
		0, 22, 27	0.0010	5.5525		0.0000.0	0.0000.0	0.0022	0.0000		0.00000		0.000070	0.00007	0.021	0.000000	0.001 0
MW-1	4	8/29/17	0.0010 U	0.00046 U	0.055	0.00034 U	0.00034 U	0.0011 U	0.00062 J	0.58	0.00035 U	0.0032 U	0.000070 U	0.00085 U	0.0057	0.000085 U	0.620
MW-2	4	8/29/17	0.0010 U	0.00046 U	0.11	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.42	0.00035 U	0.0032 U	0.000070 U	0.00085 U	0.00044 J	0.000085 U	0.181 U
MW-3	4	8/29/17	0.0010 U	0.0024	0.25	0.00034 U	0.00034 U	0.0011 U	0.0022 J	2.30	0.00035 U	0.0075	0.000070 U	0.22	0.14	0.000085 U	0.374
MW-4	4	8/30/17	0.0010 U	0.0027	0.055	0.00034 U	0.00034 U	0.0011 U	0.0017 J	0.68	0.00035 U	0.90	0.000070 U	0.40	0.0058	0.000085 U	0.457
MW-4	4	8/30/17	0.0010 U	0.0024	0.054	0.00034 U	0.00034 U	0.0011 U	0.0016 J	0.66	0.00035 U	0.98	0.000070 U	0.42	0.0054	0.000085 U	0.146 U
MW-5	4	8/29/17	0.0010 U	0.0021	0.036	0.00034 U	0.00034 U	0.0011 U	0.0033	0.48	0.00035 U	0.0039 J	0.000070 U	0.0057 J	0.0099	0.000085 U	0.601
MW-1	5	9/12/17	0.0010 U	0.00046 J	0.057	0.00034 U	0.00034 U	0.0011 U	0.00075 J	0.47	0.00035 U	0.0032 U	0.000070 U	0.0018 J	0.0057	0.000085 U	0.333 U
MW-2	5	9/12/17	0.0010 U	0.00046 U	0.11	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.35	0.00035 U	0.0032 U	0.000070 U	0.00094 J	0.00046 J	0.000085 U	0.196 U
MW-3	5	9/12/17	0.0012 J	0.0029	0.23	0.00034 U	0.00034 U	0.0011 U	0.0025	1.9	0.00035 U	0.0056	0.000070 U	0.28	0.18	0.000085 U	0.462
MW-4	5	9/13/17	0.0010 U	0.0035	0.056	0.00034 U	0.00034 U	0.0011 U	0.0017	0.53	0.00035 U	0.75	0.000070 U	0.41	0.013	0.000085 U	0.361
MW-4	5	9/13/17	0.0010 U	0.0038	0.056	0.00034 U	0.00034 U	0.0011 U	0.0017	0.63	0.00035 U	0.86	0.000070 U	0.42	0.014	0.000085 U	0.656
MW-5	5	9/12/17	0.0010 U	0.0041	0.0038	0.00034 U	0.00034 U	0.0011 U	0.0033	0.29	0.00035 U	0.0032 U	0.000070 U	0.0048 J	0.0053	0.000085 U	0.227 U
	<u> </u>			<u> </u>	I	1		I	<u> </u>		<u> </u>	I	1	1		I	<u> </u>
MW-1	6	10/3/17	0.0010 U	0.00087 J	0.056	0.00034 U	0.00034 U	0.0011 U	0.00087 J	0.61	0.00035 U	0.0032 U	0.000070 U	0.0027 J	0.0055	0.000085 U	0.230 U
MW-2	6	10/3/17	0.0010 U	0.00046 J	0.093	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.43	0.00035 U	0.0032 U	0.000070 U	0.0013 J	0.0012 J	0.000085 U	0.675
MW-3	6	10/3/17	0.0017 J	0.0036	0.19	0.00034 U	0.00063 J	0.031	0.0040	1.8	0.00035 U	0.034	0.000070 U	0.53	0.57	0.000085 U	1.07
MW-4	6	10/4/17	0.0019 J	0.0059	0.059	0.00034 U	0.00034 U	0.0011 U	0.0018 J	0.64	0.00035 U	0.77	0.000070 U	0.44	0.011	0.000085 U	0.699
MW-4	6	10/4/17	0.0010 U	0.0056	0.065	0.00034 U	0.00034 U	0.0011 U	0.0017 J	0.63	0.00035 U	0.82	0.000070 U	0.46	0.0095	0.000085 U	0.528
MW-5	6	10/3/17	0.0010 U	0.0060	0.034	0.00034 U	0.00034 U	0.0011 U	0.0030	0.52	0.00035 U	0.0061	0.000070 U	0.0053 J	0.0034	0.000085 U	0.445

TABLE I
GROUNDWATER ANALYTICAL RESULTS - APPENDIX IV CONSTITUENTS
CORRECTIVE MEASURES ASSESSMENT
AES PUERTO RICO - AGREMAX STAGING AREA
GUAYAMA, PUERTO RICO

		GWPS	0.006	0.010	2	0.004	0.005	0.1	0.006	4	0.015	0.040	0.002	0.100	0.05	0.002	5
WELL ID	Event	Sampling Date	Antimony mg/l	Arsenic mg/l	Barium mg/l	Beryllium mg/l	Cadmium mg/l	Chromium mg/l	Cobalt mg/l	Fluoride mg/l	Lead mg/l	Lithium mg/l	Mercury mg/l	Molybdenum mg/l	Selenium mg/l	Thallium mg/l	Radium 226/228 pCi/L
MW-1	7	10/11/17	0.0010 U	0.00047 J	0.063	0.00034 U	0.00034 U	0.0023 J	0.0011 J	0.58	0.00035 U	0.0032 U	0.000070 U	0.0028 J	0.0044	0.000085 U	0.362 U
MW-2	7	10/11/17	0.0010 U	0.00094 J	0.10	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.41	0.00035 U	0.0032 U	0.000070 U	0.0013 J	0.0011 J	0.000085 U	0.313 U
MW-3	7	10/11/17	0.0017 J	0.0031	0.22	0.00034 U	0.00054 J	0.0011 U	0.0032	1.9	0.00035 U	0.012	0.000070 U	0.40	0.38	0.000085 U	0.429
MW-4	7	10/12/17	0.0022 J	0.0033	0.047	0.00034 U	0.00034 U	0.0035	0.0017 J	0.67	0.00047 J	0.74	0.000070 U	0.44	0.0067	0.000085 U	0.251 U
MW-4	7	10/12/17	0.0026	0.0038	0.052	0.00034 U	0.00034 U	0.0033	0.0017 J	0.65	0.00047 J	0.73	0.000070 U	0.51	0.0073	0.000085 U	0.236 U
MW-5	7	10/11/17	0.0010 U	0.0065	0.034	0.00034 U	0.00034 U	0.0011 U	0.0032	0.49	0.00035 U	0.0043 J	0.000070 U	0.0054 J	0.0038	0.000085 U	0.300 U
MW-1	8	10/17/17	0.0010 U	0.00069 J	0.06	0.00034 U	0.00034 U	0.0011 U	0.00097 J	0.55	0.00035 U	0.0032 U	0.000070 U	0.0020 J	0.0074	0.000085 U	0.319 U
MW-2	8	10/17/17	0.0010 U	0.0014	0.089	0.00034 U	0.00034 U	0.0039	0.00040 U	0.36	0.00035 U	0.0032 U	0.000070 U	0.0023 J	0.0034	0.000085 U	0.439 U
MW-3	8	10/17/17	0.0010 U	0.0032	0.21	0.00034 U	0.00034 U	0.0024 J	0.0028	1.8	0.00035 U	0.010	0.000070 U	0.37	0.33	0.000085 U	0.537
MW-4	8	10/17/17	0.0012 J	0.0055	0.04	0.00034 U	0.00034 U	0.0012 J	0.0018 J	0.65	0.00036 J	0.69	0.000070 U	0.53	0.010	0.000085 U	0.231 U
MW-4	8	10/17/17	0.0010 U	0.0062	0.04	0.00034 U	0.00037 J	0.0012 J	0.0018 J	0.64 0.00035		0.74 0.000070 U		0.54	0.0092	0.000085 U	0.366 U
MW-5	8	10/17/17	0.0049	0.0060	0.030	0.00034 U	0.00034 U	0.0011 U	0.0029	0.47	0.00035 U	0.0067	0.000070 U	0.0076 J	0.0049	0.000085 U	0.282 U
MW-1	9	6/25/18	0.0010 U	0.00046 U	0.039	0.00034 U	0.00034 U	0.0011 U	0.00040 U	0.61	0.00077 J	0.0011 U	0.000070 U	0.00085 U	0.025	0.000085 U	NA
MW-2	9	6/25/18	0.0010 U	0.00046 U	0.15	0.00034 U	0.00034 U	0.0011 U	0.00067 J	0.52	0.00035 U	0.0011 U	0.000070 U	0.00085 U	0.00040 J	0.000085 U	NA
MW-3	9	6/25/18	0.0010 U	0.0018	0.24	0.00034 U	0.00042 J	0.0011 U	0.0031	1.6	0.00035 U	0.0073	0.000070 U	0.22	0.21	0.000085 U	NA
MW-4	9	6/25/18	0.0023 J	0.0024	0.044	0.00034 U	0.00034 J	0.0011 U	0.0016 J	0.76	0.00035 U	0.54	0.000070 U	0.55	0.0064	0.000085 U	NA
MW-4	9	6/25/18	0.0019 J	0.0021	0.046	0.00034 U	0.00034 U	0.0011 U	0.0016 J	0.76	0.00035 U	0.57	0.000070 U	0.58	0.0055	0.000085 U	NA
MW-5	9	6/25/18	0.0010 U	0.0071	0.036	0.00034 U	0.00034 U	0.0011 U	0.0030	0.49	0.00035 U	0.0038	0.000070 U	0.0042 J	0.00024 U	0.000085 U	NA
MW-1	10	10/1/18	0.0010 U	0.00046 U	0.032	NA	0.00034 U	NA	0.00050 J	0.69	NA	0.0011 U	NA	0.00085 U	0.015	NA	0.495
MW-2	10	10/1/18	0.0010 U	0.00046 U	0.13	NA NA	0.00031 U	NA NA	0.00058 J	0.67	NA NA	0.0011 J	NA NA	0.00085 U	0.00024 U	NA NA	0.321 U
MW-3	10	10/1/18	0.0010 U	0.0024	0.19	NA NA	0.00031 U	NA NA	0.0031	1.6	NA NA	0.021	NA NA	0.22	0.23	NA NA	0.511
MW-4	10	10/2/18	0.0010 U	0.0031	0.035	NA	0.00057 J	NA	0.0016 J	1.00	NA	0.38	NA	0.74	0.0043	NA	0.0708 U
MW-4	10	10/2/18	0.0010 U	0.0027	0.036	NA	0.00051 J	NA	0.0016 J	1.00	NA	0.34	NA	0.76	0.0048	NA	0.168 U
MW-5	10	10/2/18	0.0010 U	0.0088	0.032	NA	0.00034 U	NA	0.0030	0.50	NA	0.0038 J	NA	0.0053 J	0.00046 J	NA	-0.0397

TABLE I
GROUNDWATER ANALYTICAL RESULTS - APPENDIX IV CONSTITUENTS
CORRECTIVE MEASURES ASSESSMENT

AES PUERTO RICO - AGREMAX STAGING AREA GUAYAMA, PUERTO RICO

		GWPS	0.006	0.010	2	0.004	0.005	0.1	0.006	4	0.015	0.040	0.002	0.100	0.05	0.002	5
WELL ID	Event	Sampling Date	Antimony mg/l	Arsenic mg/l	Barium mg/l	Beryllium mg/l	Cadmium mg/l	Chromium mg/l	Cobalt mg/l	Fluoride mg/l	Lead mg/l	Lithium mg/l	Mercury mg/l	Molybdenum mg/l	Selenium mg/l	Thallium mg/l	Radium 226/228 pCi/L
TW-101	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.96	NA	0.0048 J	NA	0.0067	0.0049 U	NA	NA
MW-3	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	1.6	NA	0.0035 J	NA	0.17	0.11	NA	NA
TW-102	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.74	NA	1.1	NA	1.4	0.98	NA	NA
MW-4	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.78	NA	0.38	NA	0.51	0.0049 U	NA	NA
MW-4	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.79	NA	0.37	NA	0.51	0.0049 U	NA	NA
TW-103	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.74	NA	0.60	NA	1.4	0.70	NA	NA
MW-5	11	6/3/19	NA	NA	NA	NA	NA	NA	NA	0.42	NA	0.0043 J	NA	0.0035 J	0.0049 U	NA	NA
TW-104	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	0.78	NA	0.0027 J	NA	0.012 U	0.0049 U	NA	NA
TW-105	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	1.2	NA	0.0026 J	NA	0.012 U	0.0049 U	NA	NA
TW-106	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	0.98	NA	0.0048 J	NA	0.013 U	0.0049 U	NA	NA
TW-107	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	0.61	NA	0.016	NA	0.012 U	0.0049 U	NA	NA
TW-108	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	0.71	NA	0.0041 J	NA	0.012 U	0.0049 U	NA	NA
TW-109	11	6/4/19	NA	NA	NA	NA	NA	NA	NA	0.66	NA	0.0041 J	NA	0.012 U	0.0049 U	NA	NA

Notes:

- 1. mg/L milligrams per Liter.
- 2. pCi/L picoCurie per liter.
- 3. U Constituent was not detected, value is the reporting limit.
- 4. J Result is less than the Reporting Limit but greater than or equal to the MDL; concentration is an approximate value.
- 5. Detected values are shown in **bold**.
- 6. NA not available.
- 7. GWPS Groundwater Protection Standards.

TABLE II REMEDIAL ALTERNATIVE ROADMAP CORRECTIVE MEASURES ASSESSMENT AES PUERTO RICO - AGREMAX™ STAGING AREA GUAYAMA, PUERTO RICO

ive	Daniel Alternative	Gr	oundwater Remedy Components	
Alternative Number	Remedial Alternative Description	A. Groundwater Remedy Approach	B. Groundwater Remedy Implementation Method	C. On-Going / Long-Term Actions
1	Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)	Natural Attenuation with Monitoring Mitigate downgradient migration of CCR-derived constituents present in groundwater at concentrations above Groundwater Protection Standards (GWPS) through process of natural attenuation	Passive Treatment Natural geochemical processes will be used to reduce concentrations of CCR-derived constituents in groundwater	Monitored Natural Attenuation Long-term groundwater monitoring will be used to confirm reduction of CCR-derived constituent concentrations
2	Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	Hydraulic Containment Mitigate downgradient migration of CCR-derived constituents present in groundwater at	Pump & Treat Treat extracted water using existing reverse osmosis (RO) system and discharge to the coal plie runoff pond or reuse for dust control; operate for duration of Staging Area activity	
3	Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	concentrations above GWPS using shallow extraction wells installed downgradient/side-gradient of the Staging Area	Pump with Recirculation Pump water to coal pile runoff pond or re-use for dust control without treatment; operate for duration of Staging Area activity	Pump Long-Term Continue to operate hydraulic
4	Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	Hydraulic Containment with Barrier Wall Install 30-ft barrier wall downgradient from	Pump & Treat Treat extracted water using existing RO system and discharge to the coal pile runoff pond or reuse for dust control; operate for duration of Staging Area activity	containment system to maintain reduction of CCR-derived constituents in groundwater
5	Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation	Staging Area, install extraction wells to reduce groundwater flow and mitigate downgradient migration of CCR-derived constituents present in groundwater at concentrations above GWPS	Pump with Recirculation Pump water to coal pile runoff pond or re-use for dust control without treatment; operate for duration of Staging Area activity	



TABLE III

SUMMARY OF CORRECTIVE MEASURES

CORRECTIVE MEASURES ASSESSMENT AES PUERTO RICO - AGREMAX STAGING AREA

GUAYAMA, PUERTO RICO

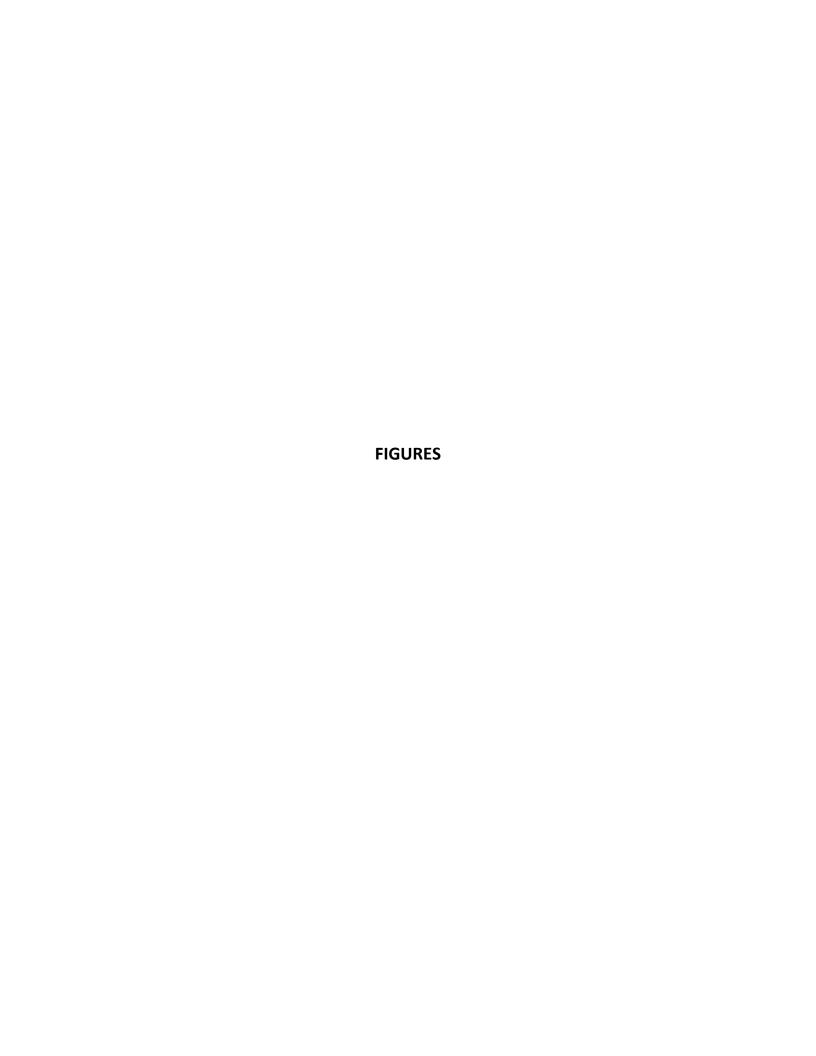
			TH	RESHOLI	D CRITERIA										BALAI	NCING CRITERIA								
											Sub-Ca	tegory 1					Sub-	Cat. 2			Sul	b-Catego	у 3	
				ë, to ⊼ <	ated ole, ate			1	2	3	4	5	6	7	8		1	2		1	2	3	4	5
Alternative Number	Remedial Alternative Description	Be protective of human health and the environment	Attain the groundwater protective standard	Control the source of releases so as to reduce or eliminat the maximum extent feasible, further releases of Appendication constituents into the environment	Remove from the environment as much of the contaminated material that was released from the CCR unit as is feasible, taking into account factors such as avoiding inappropriate disturbance of sensitive ecosystems	Management of waste to comply with all applicable RCRA requirements	CATEGORY 1 Long- and Short-Term Effectiveness, Protectiveness, and Certainty of Success that the Remedy will Prove Successful	Magnitude of reduction of existing risks	Magnitude of residual risks in terms of likelihood of further releases due to CCR remaining following implementation of a remedy	Type and degree of long-term management required, including monitoring, operation and maintenance	Short-term risk to community or environment during implementation of remedy	Time until full protection is achieved	Potential for exposure of humans and environmental receptors to remaining wastes, considering the potential threat to human health and the environment associated with excavation, transportation, re-disposal, or containment	Long-term reliability of engineering and institutional controls	Potential need for replacement of the remedy	CATEGORY 2 Effectiveness in Controlling the Source to Reduce Further Releases	Extent to which containment practices will reduce further releases	Extent to which treatment technologies may be used	CATEGORY 3 The Ease or Difficulty of Implementation	Degree of difficulty associated with constructing the technology	Expected operational reliability of the technologies	Need to coordinate with and obtain necessary approvals and permits from other agencies	Availability of necessary equipment and specialists	Available capacity and location of needed treatment, storage, and disposal services
1	Prevent AGREMAX™ Contact with the Ground by Installation of a Synthetic Liner and Employ Monitored Natural Attenuation (MNA)	√	✓	✓	✓	✓																		
2	Hydraulic Containment of Groundwater via Groundwater Pumping with Treatment	√	✓	√	√	✓																		
3	Hydraulic Containment of Groundwater via Groundwater Pumping with Recirculation	√	✓	√	✓	✓																		
4	Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Treatment	√	✓	√	✓	✓																		
5	Hydraulic Containment of Groundwater via Groundwater Pumping with Barrier Wall and Recirculation	√	✓	✓	✓	✓																		

Most favorable when compared to other alternatives
Less favorable when compared to other alternatives
Least favorable when compared to other alternatives



^{1.} For context, this a relative comparison of remedial options for this site. Site conditions, weather, and site-specific considerations are made in this table. This is not a comparison to all options at all sites.

^{2.} AGREMAX™ is a beneficial use product that has been shown to be protective of human health and the environment in transport, delivery and use.







AERIAL IMAGERY SOURCE: ESRI



600 APPROXIMATE SCALE IN FEET



AGREMAX STAGING AREA AES PUERTO RICO GUAYAMA, PUERTO RICO

SITE LOCATION MAP

SCALE: AS SHOWN SEPTEMBER 2019

FIGURE 1-1

VARI, KATALIN G:\133136 AES P



LEGEND

— - - — APPROXIMATE PROPERTY LINE

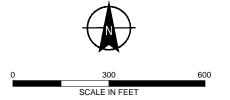
 $\blacksquare \blacksquare \blacksquare \blacksquare \blacksquare \blacksquare \blacksquare$ APPROXIMATE AGREMAXTM STAGING AREA



GROUNDWATER FLOW DIRECTION

NOTES

- BACKGROUND IMAGE WAS TAKEN FROM GOOGLE EARTH PRO, DATED MARCH 06, 2019.
- 2. COORDINATE SYSTEM: NAD83, PUERTO RICO STATE PLANE (METERS). ELEVATION REFERENCE: ORTHOMETRIC, GEOID 12B.
- 3. LIMITS OF EXISTING AGREMAX[™] STAGING AREA AND SOIL BORING LOCATIONS OBTAINED FROM CARASQUILLO ASSOCIATES, LTD. REPORT, DATED OCTOBER 15, 2018.
- 4. ESTUARINE AND MARINE WETLAND BOUNDARIES OBTAINED FROM CCR GROUNDWATER MONITORING PROGRAM PRESENTATION BY DNA-ENVIRONMENT, LLC, DATED DECEMBER 14, 2017.
- 5. ALL BOUNDARY LOCATIONS ARE APPROXIMATE.





CORRECTIVE MEASURES ASSESSMENT AGREMAX STAGING AREA AES PUERTO RICO GUAYAMA, PUERTO RICO

SITE FEATURES MAP

SCALE: AS SHOWN SEPTEMBER 2019



LEGEND

— - - — APPROXIMATE PROPERTY LINE

■■■■■ APPROXIMATE AGREMAX[™] STAGING AREA

CCR MONITORING WELL LOCATION



NATURE AND EXTENT MONITORING WELL LOCATION



P-102 PIEZOMETER LOCATION

NOTES

- 1. BACKGROUND IMAGE WAS TAKEN FROM GOOGLE EARTH PRO, DATED MARCH 06, 2019.
- 2. COORDINATE SYSTEM: NAD83, PUERTO RICO STATE PLANE (METERS). ELEVATION REFERENCE: ORTHOMETRIC, GEOID 12B.
- 3. LIMITS OF EXISTING AGREMAX $^{\text{TM}}$ STAGING AREA AND SOIL BORING LOCATIONS OBTAINED FROM CARASQUILLO ASSOCIATES, LTD. REPORT, DATED OCTOBER 15, 2018.
- 4. ALL BOUNDARY LOCATIONS ARE APPROXIMATE.
- 5. CCR = COAL COMBUSTION RESIDUALS



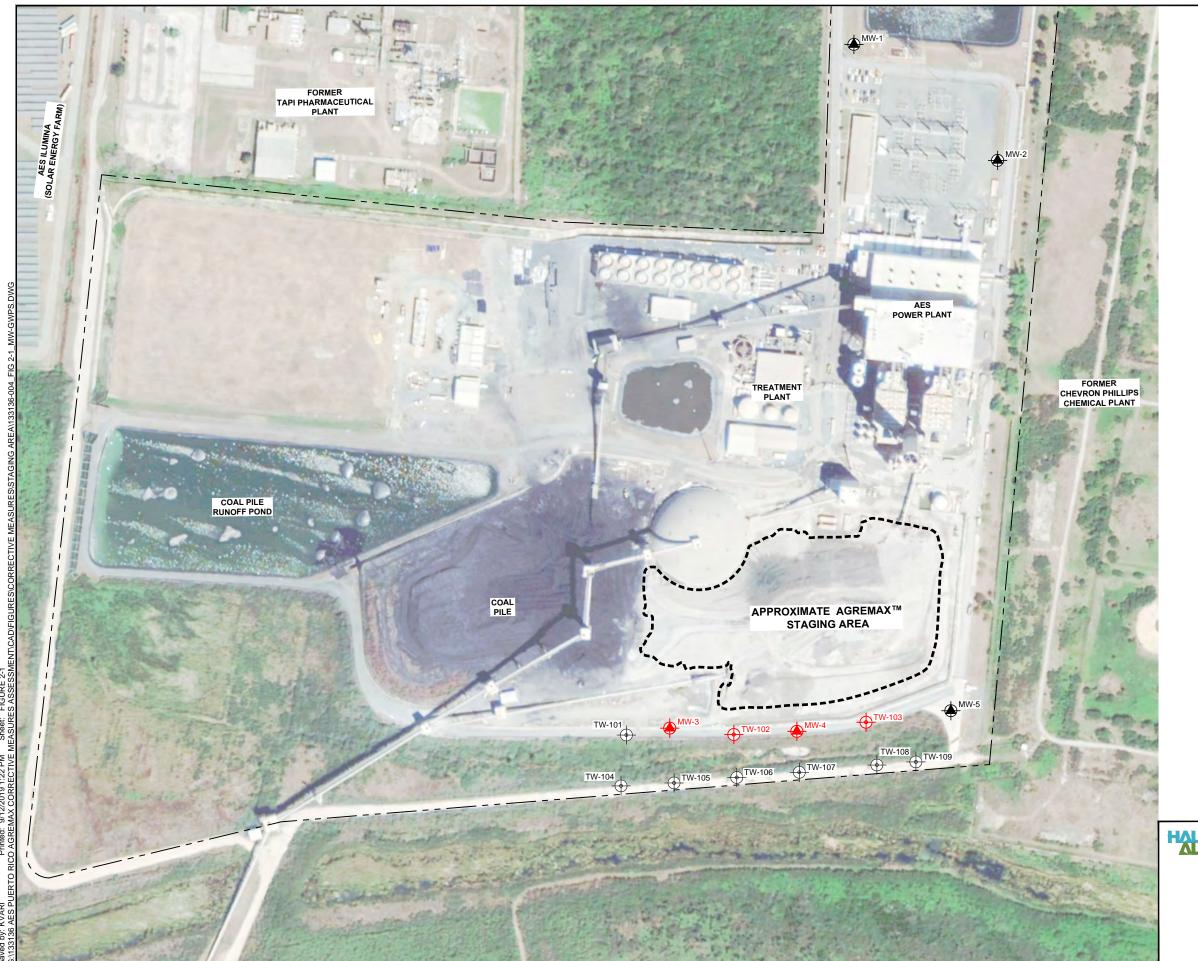


CORRECTIVE MEASURES ASSESSMENT AGREMAX STAGING AREA AES PUERTO RICO GUAYAMA, PUERTO RICO

MONITORING WELL LOCATIONS

SCALE: AS SHOWN SEPTEMBER 2019

FIGURE 1-3



LEGEND

— — — APPROXIMATE PROPERTY LINE

■■■■■ APPROXIMATE AGREMAX[™] STAGING AREA



CCR MONITORING WELL WITH NO CONSTITUENTS



NATURE AND EXTENT MONITORING WELL WITH NO CONSTITUENTS ABOVE GWPS



CCR MONITORING WELL WITH LITHIUM, MOLYBDENUM, OR SELENIUM CONCENTRATION ABOVE GWPS



NATURE AND EXTENT MONITORING WELL WITH LITHIUM, MOLYBDENUM, OR SELENIUM CONCENTRATION ABOVE GWPS

NOTES

- 1. BACKGROUND IMAGE WAS TAKEN FROM GOOGLE EARTH PRO, DATED MARCH 06, 2019.
- 2. COORDINATE SYSTEM: NAD83, PUERTO RICO STATE PLANE (METERS). ELEVATION REFERENCE: ORTHOMETRIC, GEOID 12B.
- 3. LIMITS OF EXISTING AGREMAX[™] STAGING AREA AND SOIL BORING LOCATIONS OBTAINED FROM CARASQUILLO ASSOCIATES, LTD. REPORT, DATED OCTOBER 15, 2018.
- 4. ALL BOUNDARY LOCATIONS ARE APPROXIMATE.
- 5. CCR = COAL COMBUSTION RESIDUALS
- 6. GWPS = GROUNDWATER PROTECTION STANDARDS





CORRECTIVE MEASURES ASSESSMENT AGREMAX STAGING AREA AES PUERTO RICO GUAYAMA, PUERTO RICO

MONITORING WELL LOCATIONS WITH STATISTICALLY SIGNIFICANT LEVELS ABOVE GWPS

SCALE: AS SHOWN SEPTEMBER 2019

APPENDIX A

Groundwater Characterization Report

GROUNDWATER CHARACTERIZATION REPORT USEPA COAL COMBUSTION RESIDUALS RULE AES PUERTO RICO LP, GUAYAMA, PR

SEPTEMBER 2019 AMENDED NOVEMBER 2019

Prepared for:

AES Puerto Rico, LP PO Box 1890 Guayama, Puerto Rico 00785

Prepared by:

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GROUNDWATER CHARACTERIZATION REPORT USEPA COAL COMBUSTION RESIDUALS RULE AES PUERTO RICO LP, GUAYAMA, PR

SEPTEMBER 2019 AMENDED NOVEMBER 2019

Prepared by:

Alberto Meléndez

Principal, DNA-Environment, LLC

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1 INTRODUCTION

1.1 Purpose and Scope

This report describes the procedures, findings and conclusions pertaining to the characterization of the nature and extent of lithium, molybdenum and selenium in the groundwater at AES Puerto Rico, LP (AES-PR) in Guayama, Puerto Rico (Facility). Field activities were conducted from 6 May to 5 June 2019. These included the installation of nine temporary monitoring wells at the southern portion of the Facility, and sampling and analysis of groundwater samples from all newly installed temporary wells and existing Monitoring Wells MW-3 to MW-5. Monitoring Wells MW-3 to MW-5 were installed in 2017 for the monitoring of groundwater in accordance with the U.S. Environmental Protection Agency's (USEPA) Coal Combustion Residuals Rule (CCR Rule).

Groundwater characterization was conducted pursuant to 40 CFR §257.95(g)(1) given that CCR groundwater monitoring events conducted from 2017 to 2018 resulted in statistical significant levels above the groundwater protection standards (GWPS) of lithium, molybdenum and selenium in groundwater samples collected from certain monitoring wells at the Facility.

1.2 Facility Information

AES-PR operates a coal-fired power plant located in the municipality of Guayama in the south coast of Puerto Rico (Figure 1). The Facility utilizes bituminous coal for energy production and generates coal combustion residuals (CCR). The CCR is converted to a manufactured aggregate known as Agremax that is stored in a temporary staging area located near the southern property limit (Figure 2).

Since 2017, AES-PR implemented a groundwater monitoring program in accordance with the CCR Rule. The Facility's monitoring network consists of five monitoring wells located either hydraulically upgradient or downgradient of the Agremax Staging Area. This network includes upgradient wells MW-1 and MW-2, and downgradient wells MW-3, MW-4 and MW-5. The locations of the CCR monitoring wells are shown in **Figure 2**. Groundwater samples collected from these wells have been analyzed for the constituents listed in Appendices III and IV to 40 CFR Part 257. Statistical evaluation completed in January 2019, per the USEPA's CCR Rule, resulted in statistical significant levels above the GWPS of selenium and molybdenum in groundwater samples collected from Monitoring Well MW-3, and of lithium and molybdenum from Monitoring Well MW-4.

2 MONITORING WELL PLACEMENT AND INSTALLATION

Prior to drilling activities, well locations were cleared of subsurface utilities using Ground Penetrating Radar (GPR), Pipe and Cable Line Locator, and Acoustic Detector.

Newly installed monitoring wells were placed hydraulically downgradient from the Agremax Staging Area (Figure 2). These consisted of temporary wells at the downgradient boundary of

the Agremax Staging Area (Wells TW-101 to TW-103), and wells near the southern property boundary of AES-PR (Wells TW-104 to TW-109).

In addition, Temporary Piezometers P-102 and P-106 (Figure 2) were installed to obtain higher definition of groundwater elevation contours at the Facility.

All temporary wells and piezometers were installed in the uppermost aguifer to a depth immediately above the upper aquifer's confining clay layer. During the hydrogeologic investigation conducted at the Facility for CCR groundwater monitoring implementation, the confining clay layer was intercepted at a depth ranging from 20 to 25 feet below ground surface.

2.1 Monitoring Well Installation Procedures

Boreholes for well installation were advanced using a Geoprobe® drill rig. At each well location, continuous soil cores were collected for lithologic description. Temporary Wells TW-102 to TW-109 were installed using 4.25-inch inner diameter hollow stem augers. These wells were constructed of 2-inch diameter, schedule-40, PVC piping and consisted of screen and blank riser sections. Each well consisted of a 10-foot screen section of 0.010-inch factory slotted pipe and blank riser. The blank riser section was installed to span the length from the upper end of the well screen to an approximate height of three feet above existing grade. The wells were completed with a bentonite seal and cement grout.

Attempts to advance a borehole at location TW-101 were met with probe refusal at an approximate depth of nine feet below grade, even after offsetting the original location three times. Analysis of historical site aerial photographs revealed that this area had been underlain with boulders (gabions) during Facility construction. Because subsurface obstructions precluded the advancement of the 4.25 inner diameter hollow stem augers, Temporary Well TW-101 was installed using a 1.5-inch diameter PVC prepacked well screen after advancing a borehole with the 3.25-inch outer diameter Geoprobe® dual tube system. This well consisted of a 10-foot PVC well screen section of 0.010-inch factory slotted pipe containing metal-free prepacked well materials from ECT Manufacturing. The well was completed with a stickup PVC blank riser pipe to an approximate height of three feet above grade. Additional silica sand was added to fill any remaining annular space between the well exterior and borehole walls. The well was completed with a bentonite seal and cement grout. Appendix A includes the prepacked screen monitoring well specifications from the manufacturer.

Newly installed monitoring wells were allowed to set for a minimum of 24 hours after which wells were developed by purging the groundwater with an electrical submersible pump to remove bottom and suspended sediments.

Piezometers P-102 and P-106 were installed with the Geoprobe® 3.25-inch outer diameter dual tube system. The piezometers consisted of 1.5-inch diameter PVC screen and blank riser sections.

A professional land surveyor measured the geographical coordinates and top of casing well elevations of each monitoring well and piezometer. These measurements were subsequently used to determine groundwater elevation contours from depth to groundwater measurements collected at monitoring well and piezometer locations.

2.2 Equipment Decontamination

Hollow stem augers were decontaminated onsite by placing them inside an impervious containment dike and washing each auger with a hot water pressure washer. Augers were thoroughly cleansed and the contact water containerized as Investigation-Derived Waste.

2.3 Handling and Disposal of Investigation-Derived Waste

Soil cuttings, contact water from drilling equipment decontamination, and purged water from well development and sampling were containerized in drums (United Nations Certified), and labeled as investigation-derived waste (IDW) for subsequent handling and disposal in accordance with federal and state regulations.

3 SAMPLING AND ANALYTICAL METHODS

Sampling and analytical methods are described in detail in the Sampling and Analysis Plan prepared for the groundwater characterization event (DNA, March 2019). These procedures are in accordance with 40 CFR §257.93 of the CCR Rule, "Groundwater Sampling and Analysis Requirements".

3.1 Sampling Methods

One groundwater sample from each newly installed monitoring well and from each downgradient CCR monitoring wells (i.e., Wells MW-3 to MW-5) was collected with a peristaltic pump directly into the laboratory-supplied container. Groundwater samples were collected without filtration, so as to measure the total recoverable concentration of the constituent present in the particulate and dissolved fractions of the sample.

Groundwater sampling was conducted using the *Low Stress (Low Flow) Purging and Sampling Procedure* in accordance with USEPA Region 2 (USEPA, 1998). Low flow purging and sampling was conducted using a peristaltic pump and flow-through-cell attached to a handheld multiparameter meter to monitor pH, conductivity, dissolved oxygen, oxidation-reduction (redox) potential, and temperature. Turbidity measurements were collected using a turbidimeter. The pump tubing was set at a depth corresponding to the vertical mid-section of the well screen. Purging proceeded until field parameters achieved stabilization. Instruments for field parameter measurements were calibrated following the instruments' manufacturer instructions. Instrument calibration was conducted daily prior to sampling activities. Additional calibrations or calibration checks were performed based on instrument performance, as needed.

Field quality control samples consisted of one field duplicate sample, and one matrix spike/matrix spike duplicate set per sampling event. In addition, one field blank was prepared and analyzed per each day of sampling. Equipment blanks were not collected as new sampling tubing was used in the peristaltic pump for the collection of each groundwater sample.

Each sample was placed inside a sealable plastic bag before sample container placement in the sample cooler. Samples were kept iced, inside chest coolers until samples were delivered to the analytical laboratory to ensure sample integrity. Sample coolers were packed and shipped to Eurofins TestAmerica laboratory facilities in Pensacola, Florida to be analyzed for the constituents listed in **Table 1**. Sample coolers were shipped via overnight courier following chain-of-custody protocols.

3.2 Analytical Methods

Table 1 summarizes the parameters, analytical methods, holding times and container types for the collected groundwater and quality control samples.

Besides characterizing the nature and extent of lithium, molybdenum and selenium at the Facility, groundwater samples were analyzed for the following parameters to obtain a better understanding of the groundwater chemistry:

 Alkalinity, boron, calcium, chloride, fluoride, iron, magnesium, manganese, potassium, sodium sulfate and total dissolved solids.

4 RESULTS AND DISCUSSION

4.1 Site Geology and Hydrogeology

Site geology is characteristic of an alluvial transitional zone, where alluvial deposits in the uppermost aquifer at the northern portion of the Facility transitions to swamp and beach deposits near the southern boundary of AES-PR.

Based on the soil boring logs (**Appendix B**), the area immediately south of the Agremax Staging Area (i.e., west-to-east transect from Wells TW-101 to MW-5) is underlain by fill material to an average depth of 10 feet below ground surface (bgs). The fill material consists mainly of a mixture of silty sand, sandy silt, and fine to medium sand with rock fragments. The fill stratum is underlain by the uppermost aquifer, which extends from about 10 to 24 feet bgs. This shallow aquifer is comprised of alluvial deposits consisting of layers of sandy silt, silty sand, sandy clay, clayey sand, and fine to medium sand. The lower bound of the uppermost aquifer consists of stiff clay of high plasticity that was intercepted at an average depth of 24 feet bgs. During a hydrogeologic characterization conducted in 2017 by DNA-Environment, LLC (DNA), this clay-confining layer was found to extend to the maximum drilling depth of 30 feet (lithologic data was not collected beyond this depth).

The stratigraphic sequence near the southern property boundary of the facility is similar to the above sequence (Wells TW-101 to MW-5). However, ground elevation near the southern

property boundary drops some 10 feet when compared to ground elevation immediately south of the Agremax Staging Area. Fill material near the southern property boundary (i.e., west-to-east transect from Wells TW-104 to TW-109) extends to about one foot below grade. The uppermost aquifer extends from about 1 to 14 ft below ground surface at most drilled locations (and to 17 ft bgs at location TW-107). The stiff clay layer was intercepted at an average depth of 14 feet (and 17 ft at location TW-107), and was confirmed to extend to the maximum drilling depth of 20 feet (lithologic data was not collected beyond this depth).

A professional land survey was conducted in July 2019 to determine the geographical coordinates and top-of-well-casing and ground elevations at each newly and existing monitoring well. **Table 2** summarizes these data, along with the static water elevations determined from the depth to water measurements collected at each well point during the groundwater characterization sampling event of 3 - 4 June 2019. Based on these data, the general direction of groundwater flow is southward (**Figure 3**).

4.2 Groundwater Sampling Results

The groundwater analytical results are summarized in **Table 3**. The concentrations of lithium, molybdenum and selenium in groundwater samples are referenced to the sampled monitoring well locations in **Figure 4**.

Sampling results revealed the following:

- Concentrations of lithium, molybdenum and selenium in groundwater were generally
 detected immediately downgradient of the Agremax Staging Area along the east-west
 axis, but were not detected above the laboratory reporting limit (limit of quantitation)
 in samples collected from the monitoring wells to the west (Well TW-101) and east
 (Well MW-5).
- The highest groundwater concentrations of lithium, molybdenum and selenium were detected in samples collected from Temporary Wells TW-102 and TW-103, respectively. These monitoring wells are located immediately downgradient of the Agremax Staging Area.
- Molybdenum and selenium were not detected above the laboratory reporting limit in Temporary Wells TW-104 to TW-109, which are located near the Facility's southern property limit. Similarly lithium was not detected in these wells, except for Well TW-107 where the lithium concentration was 0.016 milligram per Liter (mg/L). This concentration is just above lithium's reporting limit of 0.010 mg/L, and below lithium's GWPS of 0.040 mg/L by a factor greater than two.

5 **CONCLUSIONS**

Based on the analytical results from the June 2019 groundwater sampling event, groundwater impacts from lithium, molybdenum and selenium, in the uppermost aquifer, are confined within AES-PR's property boundaries. The concentrations of these metal constituents were below or near their corresponding laboratory reporting limits in all samples from the monitoring wells installed near the Facility's southern property limit. Additionally, all concentrations were well below the GWPS at the southern property limit. That sampled wells are located hydraulically downgradient from the Agremax Staging Area was confirmed from the general southward groundwater flow direction as determined from depth to water measurements at each well point.

6 REFERENCES

DNA (DNA-Environment, LLC) March 2019. Sampling and Analysis Plan, Characterization of Lithium, Molybdenum and Selenium in Groundwater, USEPA Coal Combustion Rule, AES Puerto Rico LP, Guayama, PR

USEPA (United States Environmental Protection Agency). 1998. *Ground Water Sampling Procedure. Low Stress (Low Flow) Purging and Sampling*.

USEPA, 2015. 40 CFR Parts 257 and 261, Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule. 17 April.

Revision Log						
Date	Table	Description				
November 8, 2019	Table 3	Corrected value of Manganese. Revised from 8.2 mg/L to 11 mg/L for Sample ID AES-MW5-060319, collected from Monitoring Well MW-5 on June 3, 2019.				

TABLES

Table 1. Analytical Methods and Testing Requirements for Groundwater and Quality Control Samples

Parameter	Testing Method	Holding Time Before Extraction	Container Type	Preservation				
Characterization of Nature and Extent								
Lithium, Molybdenum and Selenium	EPA 6020 180 days		Plastic 250 mL	HNO ₃ to pH < 2 1 Cool \leq 6 $^{\circ}$ C 2				
Groundwater Geochemistry								
Boron and Calcium	EPA 6020	180 days	Plastic 250 mL ⁴	HNO_3 to pH < 2 Cool \leq 6 °C				
Chloride, Total	SM ³ 4500-Cl-E	28 days	Plastic 1 L 5	Cool ≤ 6 °C				
Fluoride, Total	SM 4500-F-C	28 days	Plastic 1 L	Cool ≤ 6 °C Cool ≤ 6 °C				
Sulfate, Total	SM 4500-SO4-E	28 days	Plastic 1 L					
Total Dissolved Solids	SM 2540C	7 days Plastic 1 L		Cool ≤ 6 °C				
Iron, Magnesium, Manganese, Potassium and Sodium	EPA 6020	180 days	Plastic 250 mL	HNO₃ to pH <2 Cool ≤ 6 °C				
Alkalinity (Total, Bicarbonate and Carbonate)	SM 2320B	14 days	Plastic 1 L	Cool <u><</u> 6 °C				

Notes:

 $^{^{1}}$ HNO₃ to pH < 2 = Nitric acid added to lower sample pH to less than two units. 2 Cool \leq 6 °C = Cool sample to six degrees Celsius or less. 3 SM = Standard Methods for the Examination of Waters and Wastewaters. 4 mL = milliliter

⁵L = Liter

Table 2. 2019 Monitoring Well Professional Land Survey and Groundwater Elevation Data from June 2019 Sampling Event

					Ground	Ground	TOC	TOC	Depth to	Groundwater
Well ID	Northing (Y)	Easting (X)	Latitude	Longitude	Elevation	Elevation	Elevation	Elevation	Water	Elevation
					(meters)*	(feet)	(meters)	(feet)	(feet)	(feet)
MW-1	212731.3196	230013.699	17.9481512	-66.1500155	6.148	20.171	6.948	22.795	12.22	10.58
MW-2	212639.2969	230127.7269	17.9473182	-66.1489405	6.193	20.318	6.998	22.959	12.57	10.39
MW-3	212188.6158	229867.5265	17.9432499	-66.1514032	4.022	13.196	4.842	15.886	13.75	2.14
MW-4	212186.082	229968.4781	17.9432256	-66.1504504	4.507	14.787	5.372	17.625	13.10	4.52
MW-5	212202.488	230090.6473	17.9433722	-66.1492969	4.141	13.586	4.953	16.250	13.65	2.60
TW-D	212492.9126	229980.8134	17.9459977	-66.1503294	5.407	17.740	6.026	19.770	10.12	9.65
TW-101	212183.1763	229833.1169	17.9432013	-66.1517281	3.962	12.999	4.869	15.974	14.13	1.84
TW-102	212183.5493	229918.3735	17.9432035	-66.1509233	4.256	13.963	5.183	17.005	15.20	1.80
TW-103	212193.3289	230023.3263	17.9432904	-66.1499325	4.563	14.970	5.479	17.976	15.18	2.80
TW-104	212142.7859	229828.8634	17.9428364	-66.1517689	4.594	15.072	1.759	5.771	4.11	1.66
TW-105	212145.2408	229870.9677	17.9428580	-66.1513714	0.972	3.189	1.931	6.335	4.65	1.69
TW-106	212149.4473	229920.7523	17.9428953	-66.1509014	1.257	4.124	2.189	7.182	5.54	1.64
TW-107	212153.5554	229970.3777	17.9429317	-66.1504329	1.349	4.426	2.254	7.395	5.69	1.71
TW-108	212159.3198	230031.9076	17.9429830	-66.1498520	1.280	4.199	2.155	7.070	5.45	1.62
TW-109	212162.1096	230060.4476	17.9430078	-66.1495826	1.255	4.117	2.179	7.149	5.45	1.70
P-102	212375.0089	229935.0988	17.9449331	-66.1507627	4.834	15.860	5.542	18.182	9.19	8.99
P-106	212299.0367	230114.7307	17.9442441	-66.1490682	4.609	15.121	4.949	16.237	10.49	5.75

SURVEYED SURVEYED SURVEYED SURVEYED FIELD DATA CALCULATED

Notes:

Coordinate System: NAD 83, Puerto Rico State Plane (meters)

Elevation Reference: Orthometric, Geoid12B

Horizontal and vertical coordinates were surveyed in meters.

Meters to feet conversion factor = 3.28084 feet per meter.

TOC - Top of Well Casing.

Groundwater Elevation was calculated by substracting the Depth to Water (Ft) from the TOC Elevation (Ft).

^{*} Ground surface elevations at Wells MW-1 to MW-5 were determined by subtracting the aboveground thickness of the concrete pad (0.08 m) from the concrete pad's surface elevation.

Table 3. Analytical Results and Monitoring Data for Groundwater Samples Collected in June 2019

AES Puerto Rico, LP in Guayama, Puerto Rico

	Well ID	TW-101	MW-3	TW-102	MW-4	MW-4	TW-103	MW-5
	Well Type and Location	N&E Downgradient ¹	CCR Downgradient ¹	N&E Downgradient	CCR Downgradient	Field Duplicate	N&E Downgradient	CCR Downgradient
	Sample I D	AES-TW101-060319	AES-MW3-060319	AES-TW102-060319	AES-MW4-060319	AES-MW4-Dup-060319	AES-TW103-060319	AES-MW5-060319
	Sampling Date	6/3/2019	6/3/2019	6/3/2019	6/3/2019	6/3/2019	6/3/2019	6/3/2019
Static Water Elevation (ft MSL)		1.84	2.14	1.80	4.52	NA	2.80	2.60
Statis Water Elevation (it mez)			2	1.00			2.00	2.00
Field Parameters	Units							
рН	SU	6.81	7.00	6.93	7.16	NA	7.09	6.56
Conductivity	mS/cm	13.94	13.95	35.52	18.72	NA	30.86	12.67
Redox Potential	mV	-89.9	-76.9	-73.3	-117.8	NA	-94.6	-67.6
Dissolved Oxygen	mg/L	1.02	0.76	1.02	0.51	NA	0.51	0.76
Turbidity	NTU	7.07	2.30	4.18	15.60	NA	2.70	20.99
Temperature	°C	30.30	30.83	31.90	33.14	NA	30.90	29.26
Analytical Results								
Lithium	mg/L	0.0048 J	0.0035 J	1.1	0.38	0.37	0.60	0.0043 J
Molybdenum	mg/L	0.0067	0.17	1.4	0.51	0.51	1.4	0.0035 J
Selenium	mg/L	0.0049 U	0.11	0.98	0.0049 U	0.0049 U	0.70	0.0049 U
Boron	mg/L	0.77	1.1	2.8	1.6	1.6	2.0	0.43
Calcium	mg/L	950	310	590	280	270	590	680
Chloride	mg/L	4700	4100	9000	4400	4500	5200	3800
Fluoride	mg/L	0.96	1.6	0.74	0.78	0.79	0.74	0.42
pH, Field	SU	6.81	7.00	6.93	7.16	NA	7.09	6.56
Sulfate	mg/L	620	1900	11000	4500	4300	10000	2300
Total Dissolved Solids	mg/L	16000	8700	41000	16000	13000	32000	9900
Alkalinity, Total	mg/L	650	550	350	800	810	320	500
Iron	mg/L	45	0.83	0.23 U	13	10	1.3	10
Magnesium	mg/L	840	480	290	68	66	180	380
Manganese	mg/L	7.6	1.2	4.0	2.2	2.1	6.9	11
Potassium	mg/L	10	23	1100	900	860	1000	7.4
Sodium	mg/L	1800	2700	11000	5900	5700	11000	2600

Notes:

mg/L - milligrams per Liter

SU - Standard Units

ft MSL - Feet above Mean Sea Level

mS/cm - millisiemens per centimeter

mV - millivolt

NTU - Nephelometric Turbidity Units

°C - degrees Celsius

NS - Not Sampled.

Static water elevations listed are based on measurements collected in all wells on 4 June 2019.

¹Wells installed immediately south (hydraulically downgradient) of the Agremax Staging Area.

N&E = Well for Nature and Extent Characterization; CCR = Well for Coal Combustion Residuals Groundwater Monitoring. Analytical results of metal elements are "Total Recoverable".

Sampling Date format is mmddyy.

Sample ID format is: "Site Name-MW_ID-Sampling_Date".

Sample AES-MW4-DUP-060319 is the field duplicate sample of AES-MW4-060319.

U - Not detected at indicated Method Detection Limit (MDL).

 ${\sf J}$ - Result is less than the Reporting Limit, but greater than

or equal to the MDL and concentration is an approximate value.

NA - Not Applicable to the field duplicate sample.

Table 3 (Cont.). Analytical Results and Monitoring Data for Groundwater Samples Collected in June 2019 AES Puerto Rico, LP in Guayama, Puerto Rico

	Well ID	TW-104	TW-105	TW-106	TW-107	TW-108	TW-109
	Well Type and	N&E Property	N&E Property	N&E Property	N&E Property	N&E Property	N&E Property
	Location	Boundary ²	Boundary	Boundary	Boundary	Boundary	Boundary
	Sample I D	AES-TW104-060419	AES-TW105-060419	AES-TW106-060419	AES-TW107-060419	AES-TW108-060419	AES-TW109-060419
	Sampling Date	6/4/2019	6/4/2019	6/4/2019	6/4/2019	6/4/2019	6/4/2019
Static Water Elevation (ft MSL)		1.66	1.69	1.64	1.71	1.62	1.70
Field Parameters	Units						
рН	SU	7.00	7.14	6.93	7.18	6.91	6.76
Conductivity	mS/cm	14.28	13.28	21.45	26.35	20.81	12.86
Redox Potential	mV	-92.7	-131.1	-98.4	-85.6	-68.4	-69.9
Dissolved Oxygen	mg/L	0.86	0.85	1.16	0.69	0.81	1.02
Turbidity	NTU	14.63	11.01	7.59	3.50	21.14	16.45
Temperature	°C	28.09	29.02	28.86	29.36	28.60	27.54
Analytical Results							
Lithium	ma/L	0.0027 J	0.0026 J	0.0048 J	0.016	0.0041 J	0.0041 J
Molybdenum	mg/L	0.012 U	0.012 U	0.013 J	0.012 U	0.012 U	0.012 U
Selenium	mg/L	0.0049 U	0.0049 U	0.0049 U	0.0049 U	0.0049 U	0.0049 U
Boron	mg/L	0.78	0.79	1.1	1.1	0.66	0.43
Calcium	mg/L	630	420	810	570	700	970
Chloride	mg/L	4800	3600	6300	7000	6300	4000
Fluoride	mg/L	0.78	1.2	0.98	0.61	0.71	0.66
pH, Field	SU	7.00	7.14	6.93	7.18	6.91	6.76
Sulfate	mg/L	1800	3000	4400	7800	4200	2300
Total Dissolved Solids	mg/L	13000	12000	50000	39000	26000	13000
Alkalinity, Total	mg/L	600	820	830	510	530	500
Iron	mg/L	1.5	1.5	6.7	4.9	5.7	13
Magnesium	mg/L	650	460	810	580	640	570
Manganese	mg/L	12	8.2	16	16	18	14
Potassium	mg/L	21	30	89	170	10	4.7
Sodium	mg/L	2600	2900	5600	8900	5200	2100 V

Notes:

mg/L - milligrams per Liter

SU - Standard Units

ft MSL - Feet above Mean Sea Level

mS/cm - millisiemens per centimeter

mV - millivolt

NTU - Nephelometric Turbidity Units

°C - degrees Celsius

NS - Not Sampled.

Static water elevations listed are based on measurements collected in all wells on 4 June 2019.

²Wells installed near AES-PR's southern property boundary.

N&E = Well for Nature and Extent Characterization.

Analytical results of metal elements are "Total Recoverable".

Sampling Date format is mmddyy.

Sample ID format is: "Site Name-MW_ID-Sampling_Date".

Sample AES-MW4-DUP-060319 is the field duplicate sample of AES-MW4-060319.

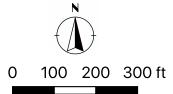
- U Not detected at indicated Method Detection Limit (MDL).
- J Result is less than the Reporting Limit, but greater than or equal to the MDL and concentration is an approximate value.
- V Serial Dilution exceeds the control limits.

FIGURES

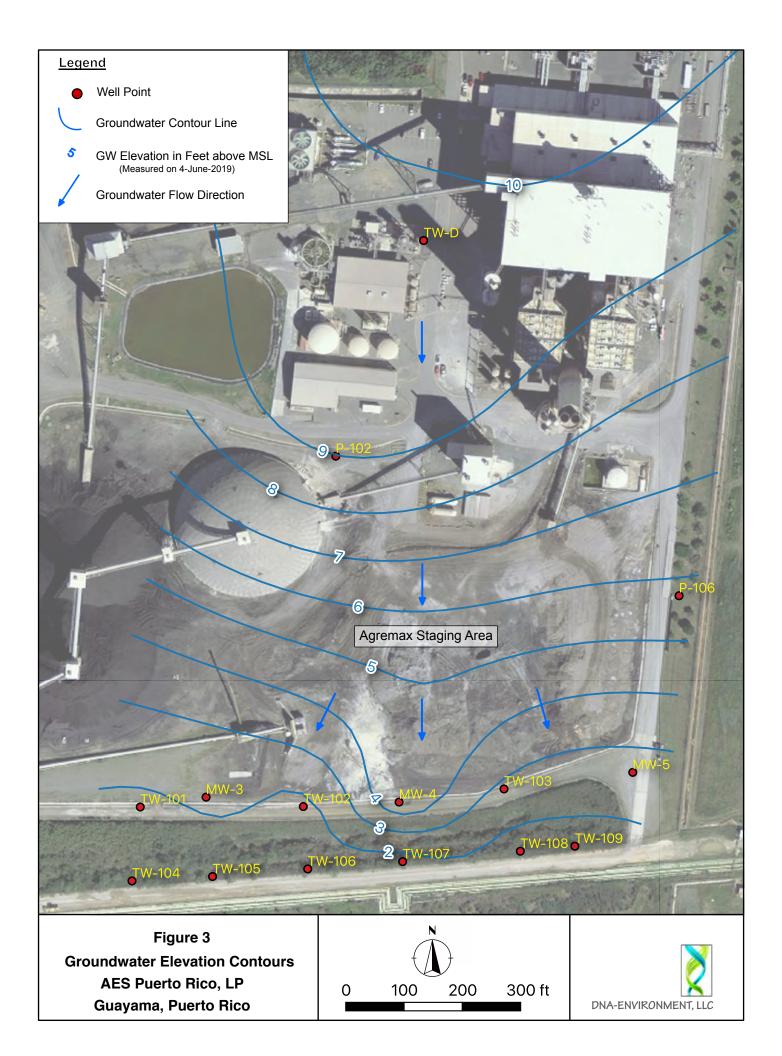


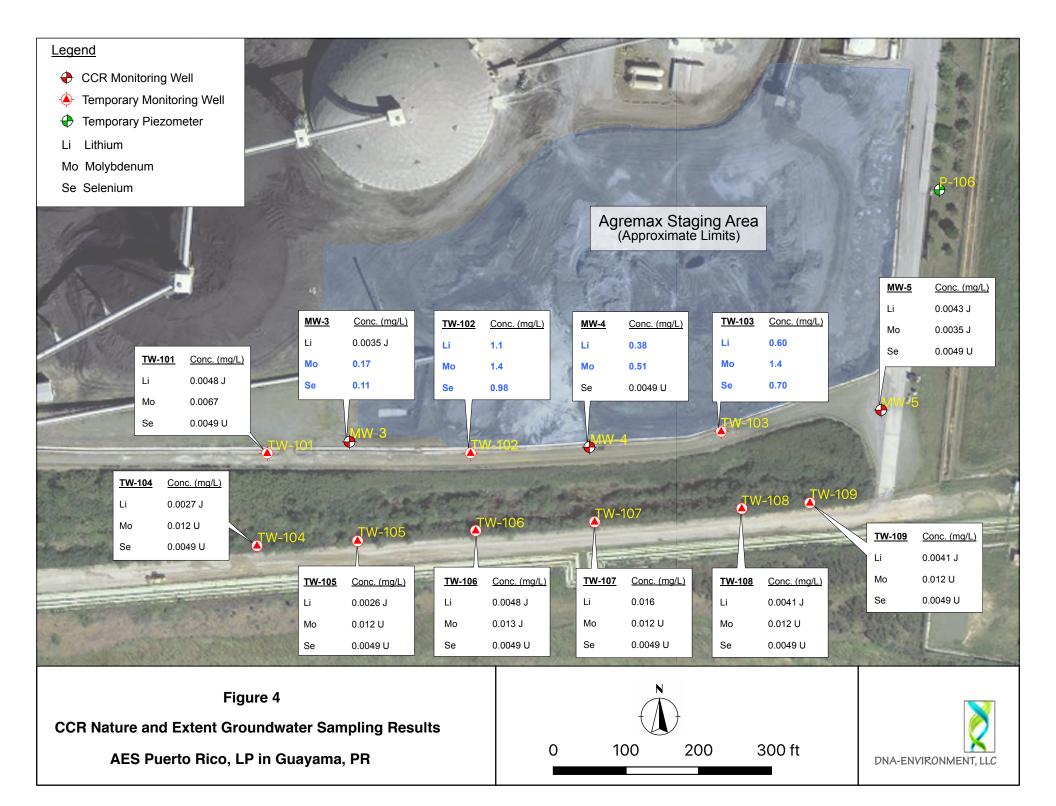


CCR Groundwater Monitoring System and Groundwater Characterization Temporary Wells AES Puerto Rico, LP in Guayama, PR









APPENDIX A

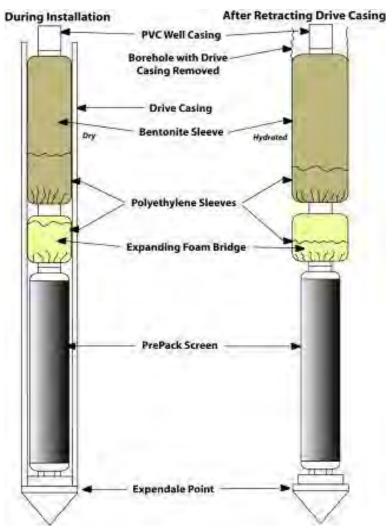
PREPACKED SCREEN MONITORING WELL SPECIFICATIONS

Pre-Pack Screen Monitoring Wells

1.5" Metals Testing Prepack (2.4" OD) x 5' length

<u>Description</u>: Outer layer is food grade nylon mesh, sand packed with 20×40 silica sand over 0.010" slotted Sch40 PVC Screen. No metal components are used.

- Assures accurate placement of filter media across desired interval.
- Quick Seal and Bentonite sleeves protects the sampling environment.
- Installed through cased borehole, provides high integrity well construction and sample quality.
- Meets ASTM standard D6725 for Direct Push Monitoring Well Installation.
- Meets basic EPA and RCRA construction requirements.
- ◆ DOD and EPA Studies reveal no statistically significant difference between water quality samples collected from paired Pre-Packs and conventional drilled wells.



ECT Pre-Pack Specifications

Pre-Pack Screen

Expanding Foam Bridge

Pipe Size	Length (feet)	Original Diameter (inch) ID/OD	Fits Casing (inchs OD)	Pipe Size	Length (feet)	Original Diameter (inch)	Fill Hole Approx. Diameter (inchs)
0.50-inch	2 .5, 5	0 .625 / 1.4	2, 2-1/4	0 .75-inch	2 .5	1.4	>2.5
0 .75-inch	2 .5, 5	0 .81 / 1.4	2, 2-1/4	1-inch	2 .5	2 .4	>3.5
1-inch	2 .5, 5	1.03 / 1.7	3-1/4, 3-1/2	1.25-inch	2 .5	2 .4	>3.5
1-inch	2 .5, 5	1.03 / 2.4	3-1/4, 3-1/2	1.50-inch	2 .5	2 .4	>3.5
1.25-inch	2.5, 5	1.34 / 2.4	3-1/4, 3-1/2	2-inch	2 .5	2 .8	>4
1.50-inch	2 .5, 5	1.59 / 2.4	3-1/4, 3-1/2				
2-inch	2.5, 5	2 .05 / 2.8	3-1/2, 3-3/4				
2-inch	2.5, 5	2.05 / 3.5	4-1/2				
3-inch	2.5, 5	3.04 / 5.5	4-1/4 HSA				
4-inch	2.5, 5	3.99 / 5.5	4-1/4 HSA				

Bentonite Sleeve

Expansion times (example) - 3/4-inch model seals 2-inch hole in approx. 6-12 hours.

Quick Seal Sleeve

Expansion times (example) - 3/4-inch model seals 2-inch hole in approx. 15-30 minutes.

Pipe Size	Length (feet)	Original Diameter (inch)	Fill Hole Approx. Diameter (inchs)	Pipe Size	Length (feet)	Original Diameter (inch) ID/OD	Fill Hole Approx. Diameter (inchs)
0 .75-inch	2 .5	1.4	>2.5	0.75-inch	0 .5	0 .81 / 1.4	>2.5
1-inch	2 .5	2 .4	>3.5	1-inch	0 .5	1.03 / 1.7	>3.5
1.25-inch	2.5	2 .4	>3.5	1.25-inch	0 .5	1.34 / 2.4	>3.5
1.50-inch	2.5	2 .4	>3.5	1.50-inch	0 .5	1.59 / 2.4	>3.5
2 -inch	2.5	2 .8	>4	2 -inch	0.5	2 .05 / 2.8	>4

Direct Push Drive Casing and Expendable Points

2-1/4 inch OD Casing	2-1/4-inch Expendable Point Steel 2-1/4-inch Expendable Pt. Aluminum
3-1/4 inch OD Casing	3-1/4-inch Expendable Point Steel 3-1/4-inch Expendable Pt. Aluminum
3-1/2 inch OD Casing	3-1/2-inch Expendable Point Steel
3-3/4 inch OD Casing	3-3/4-inch Expendable Point Steel
4-1/2 inch OD Casing	4-1/2-inch Expendable Point Steel



11 Black Forest Rd. Hamilton, NJ 08691 Phone:609-631-8939 Fax: 609-631-0993 E-Mail: ectmfg@aol.com

Web Address: ectmfg.com

Call Today 888-240-4328

APPENDIX B

SOIL BORING LOGS AND WELL CONSTRUCTION DIAGRAMS

GROUNDWATER LOG Temporary Well TW-101

IENT: AEDDRESS: RILLERS:	ES Puert Guayar GeoEnv IETHOD: well mat	Geoprobe 3.25-in ID Dual Tu	DIAMETER: 1.5-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-in) bes. Well was installed using metal-free	COORD SYS: NAD 83, PR State Plane (m ELEVATION REF: Orthometric, Geoid 12B GROUND ELEVATION: 3.962 m (12.999 Ft WELL ELEVATION AT TOC: 4.869 m (15.9	t)
DDRESS: RILLERS: RILLING M epacked v ell Screen	Guayar GeoEnv IETHOD: well mat	na, Puerto Rico riroTech, Inc. (Guaynabo, PR) Geoprobe 3.25-in ID Dual Tul	CASING: PVC SCREEN: PVC Factory Slotted (0.010-in) bes. Well was installed using metal-free	GROUND ELEVATION: 3.962 m (12.999 Ft	t)
RILLERS: RILLING M epacked v ell Screen	GeoEnv METHOD: well mat	riroTech, Inc. (Guaynabo, PR) Geoprobe 3.25-in ID Dual Tul	SCREEN: PVC Factory Slotted (0.010-in) bes. Well was installed using metal-free		
RILLING Mepacked vell Screen	METHOD: well mat	Geoprobe 3.25-in ID Dual Tu	bes. Well was installed using metal-free	WELL ELEVATION AT TOC: 4.869 m (15.9	974 Ft)
epacked very library (Ft) http://epacked.very library	well mat				
			(i.e., 1.5" ID Metals Testing PrePacked PVC	LOGGED BY: Alberto Melendez CHECKED BY: Juan D. Negron, PG	
	б			П	
	Graphic Log	Lithol	ogic Description	Well Diagram	£
	ihdi				Depth (Ft)
_	Gra			well stickup pipe ~ 3 ft	Der
 		Silty sand with some angular r	ock fragments, light yellowish brown,		Ŧ
		medium dense, moderate esti	mated K, no odor, fill material.	d ka	ŀ
- ₂				M N	_2
-					
H					H
				M M	L۷
					F"
l					F
				neat cement grout, 1–10 Ft	ا ر
6					F 6
					ļ.
					F
8					<u></u> ⊢8
				$\bowtie \bowtie$	F
l		Sandy silt vallouish brown me	sist madium stiff madium plasticity		ŀ
- 10		moderate estimated K, no odo	oist, medium stiff, medium plasticity		- 1
		moderate estimated it, no odo	i, anaviai acposits.	bentonite seal, 10-12 Ft	Ė
 					-
- 12					- 13
	:: ::: <u> </u> ::			20–30 mesh silica sand, 12–14 Ft	Ė
-					-
- 14		Sandy clay dark brown moist	medium stiff, high plasticity, low		- 1
LĖI	/ /	estimated K, no odor, alluvial o			Ė
II ⊦ I	///	, ,	·		-
- 16	/ /:				- 1
lt l	//				t
II F	///				F
– 18	/-/-	Clayey sand, dark brown, mois	st, loose, medium plasticity, moderate	20-40 mesh prepacked silica sand,	- 18
lt I	/ /	estimated K, no odor, alluvial o		14–24 Ft	Ė
∎F I			ne feldspars minerals, light brown, moist,		F
20		loose, high estimated K, no oc	lor, alluvial beach deposits.		- 20
					t
F				0.010-in slotted screen	F
- 22				Scientification 14-2410	- 2
			<u> </u>		Ė
-	7		dium dense, medium plasticity, moderate \		F
- 24					<u> </u>
		alluvial deposits.			+
- 26					- 20
- 20		Borehole Termination Depth: 2	25 Ft.		[-2
-			epted at 9 Ft below ground surface.		H
- I					٢,
	i				- 2
– 28 –					L
- 24 - 26 26		alluvial deposits. Borehole Termination Depth: 2	h plasticity, low estimated K, no odor,		

PROJECT NAME: CLIENT: AES Pue ADDRESS: Guaya DRILLERS: GeoEr	ma, Puerto Rico	DRILLING DATE: May 6, 2019 WELL DEPTH: 25 Ft DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-in) Stem Augers	COORD SYS ELEVATION GROUND EL WELL ELEVA	TES: Y=212183.5493, X=2299 :: NAD 83, PR State Plane (m REF: Orthometric, Geoid12B EVATION: 4.256 m (13.963 Ft TION AT TOC: 5.183 m (17.03) BY: Juan D. Negron, PG) ;)
%Recovery Depth (Ft) Graphic Log	Lith	nologic Description		Well Diagram ell stickup pipe ~ 3 ft	Depth (Ft)
- 2 - 2 - 4 - 6 - 8 - 10 - 12 - 14	Sandy silt with angular gravel moderate estimated K, no od	yellowish brown, medium stiff, or, fill material. st, medium stiff, high plasticity, low luvial deposits.		–neat cement grout, 1–11 Ft –bentonite seal, 11–13 Ft	- 2 - 2 - 4 - 6 - 8 - 10 - 12 - 14
- 16 - 18 - 18 - 20 - 22 - 24 - 24 - 26 - 28	May 30, 2019 collected core sa location and confirmed that lit Sandy clay, dark brown, moi estimated K, organic odor, al Clayey sand, dark brown, mois estimated K, no odor, alluvial clay, yellowish brown, stiff, hodor, alluvial deposits. Borehole Termination Depth at	t, loose, medium plasticity, moderate eposits. igh plasticity, low estimated K, no		_20-30 mesh silica sand, _13-25 Ft _0.010-in slotted screen _screen interval 15-25 Ft	- 16 - 18 - 18 - 20 - 22 - 24 - 26 - 26

GROUNDWATER LOG Temporary Well TW-103

PROJ CLIE ADD DRIL	ECT N NT: A RESS: LERS:	AME: C ES Puert Guayan GeoEnv	R: DNA-190167 CR Groundwater Monitoring to Rico, LP na, Puerto Rico riroTech, Inc. (Guaynabo, PR) : Geoprobe 4.25-in ID Hollow	DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010)	COORDINATES: Y=212193.3289, X=230023.3 COORD SYS: NAD 83, PR State Plane (m) ELEVATION REF: Orthometric, Geoid12B GROUND ELEVATION: 4.563 m (14.970 Ft) WELL ELEVATION AT TOC: 5.479 m (17.976 Ft) LOGGED BY: Hardy Rodriguez CHECKED BY: Juan D. Negron, PG	
%Recovery	7 - 1 - Depth (Ft)	Graphic Log	Silty sand with some angular re	ogic Description ock fragments, light yellowish brown, plasticity, moderate estimated K,	Well Diagram – well stickup pipe ~ 3 ft	Depth (Ft)
ŀ	- 4 - 4 6 6				neat cement grout, 1–10.5 Ft	- 4 - 6
	- - - - - - - - - - -		gray, medium dense hardne no odor, fill material.	e angular rock fragments, light olive ess, non plasticity, high estimated K est, stiff hardness, high plasticity, low	bentonite seal, 10.5–12.5 Ft	· 10
	- - 14 - - - - 16 -		estimated K, vague odor, so	me organic material, alluvial deposits. ose, medium plasticity,moderate		- 14 - 16
	- - 18 - - - - 20	//		minerals, loose hardness, non no odor, alluvial beach deposits.	20–30 mesh silica sand, 12.5–24.5 Ft 0.010–in slotted screen screen interval, 14.5–24.5 Ft	- 18 - 20
	- - 22 - - - - - 24		plasticity, low estimated K, no	nardness, high plasticity, low		- 22 - 24
	- - 26 - - - - 28 -	<i>\/////</i>	Borehole Termination Depth: 2		e	- 26 28

PROJ CLIE ADD DRIL	ECT N NT: A RESS: LERS:	AME: C ES Puert Guayar GeoEnv		DRILLING DATE: May 8, 2019 TOTAL DEPTH: 14 Ft DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-in)	
DKIL	LING N	METHOD	: Geoprobe 4.25-in ID Hollow	Stem Augers	LOGGED BY: Hardy Rodriguez CHECKED BY: Juan D. Negron, PG
%Recovery	Depth (Ft)	Graphic Log		ogic Description	Well Diagram — well stickup pipe ~ 3 ft
ŀ	3 4 5 6 6		hardness, moist, some subrou \no odor, alluvial deposits.	I, brown to light brown, medium dense nded rock fragments, very low plasticity, nedium plasticity, moist, moderate deposits.	neat cement grout, 1–2 Ft bentonite seal, 2–3 Ft
ı	6		Clay, yellowish brown, stiff lestimated K, no odor, alluvia Fine to medium sand with som non plasticity, high estimated Medium to coarse sand with so	edium dense hardness, medium ed K, no odor, alluvial deposits. nardness, high plasticity, low I deposits. ne feldspars minerals, brown, moist, d K, no odor, alluvial beach deposits. ome feldspars minerals, brown, loose, d K, no odor, alluvial beach deposits.	20–30 mesh silica sand, 3–14 Ft 9 0.010–in slotted screen screen interval, 4–14 Ft 11
ı	13 14 15 16 16 17 18		estimated K, no odor, alluvia	ive gray, moist, stiff hardness,	13 14 15 16 16
	- 18 - 19 - 20 - 21 - 22 - 22		Borehole Termination Depth: 2 Water level while drilling interc	0 Ft. epted at 1.5 Ft. below ground surface.	18
	24				24

GROUNDWATER LOG Temporary Well TW-105

PROJ CLIE ADD DRIL	ECT N NT: A RESS: LERS:	IAME: C ES Puert Guayan GeoEnv	R: DNA-190167 CR Groundwater Monitoring to Rico, LP na, Puerto Rico riroTech, Inc. (Guaynabo, PR) : Geoprobe 4.25-in ID Hollow	DRILLING DATE: May 7, 2019 TOTAL DEPTH: 14 Ft DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-	C(EL GI	OORDINATES: Y=212145.2408, X=229870 OORD SYS: NAD 83, PR State Plane (m) LEVATION REF: Orthometric, Geoid12B ROUND ELEVATION: 0.972 m (3.189 Ft) FELL ELEVATION AT TOC: 1.931 m (6.335 FT) LOGGED BY: Hardy Rodriguez CHECKED BY: Juan D. Negron, PG	
%Recovery	Depth (Ft)	Graphic Log	Lithol Six inches of fill followed by cl	ogic Description		Well Diagram — well stickup pipe ~ 3 ft	Depth (Ft)
	- 1 - 2 - 3 - 4 - 5 - 6		hardness, medium plasticity, odor, alluvial deposits.	moist at 2 Ft., low estimated K, no medium stiff hardness, medium to high		neat cement grout, 1–2 Ft bentonite seal, 2–3 Ft	- 1 - 2 - 3 3 4 5 5 6
	- 7 - 7 - 8 - 9		plasticity, low estimated K, n			—20–30 mesh silica sand, 3–14 Ft	- 7 - 7 - 8 - 8 9
	- 10 - 11 - 11 - 12		moderate estimated K, no odd	loose hardness, medium plasticity, or, alluvial deposits. ne feldspars minerals, moist, brown, n plasticity, high estimated K, no odor,		0.010-in slotted screen screen interval, 4-14 Ft	- 10 - 11 - 11 - 12
	- 13 - 13 - 14 - 14		no odor, alluvial deposits.	ft, high plasticity, low estimated K, f hardness, high plasticity, low l deposits.			- 13 - 13 - 14
	- 15 - - -		Borehole Termination Depth: 1 Water level while drilling inter	5 Ft. rcepted at 2.5 Ft. below ground surface.			- 15 - - -

GROUNDWATER LOG Temporary Well TW-106

PROJ CLIE ADD DRIL	JECT N NT: A PRESS: LERS:	AME: C ES Puert Guayan GeoEnv	R: DNA-190167 CR Groundwater Monitoring to Rico, LP na, Puerto Rico viroTech, Inc. (Guaynabo, PR) : Geoprobe 4.25-in ID Hollow	DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-in	COORDINATES: Y =212149.44 COORD SYS: NAD 83, PR ST ELEVATION REF: Orthometric, GROUND ELEVATION: 1.257 r WELL ELEVATION AT TOC: 2.: LOGGED BY: Hardy Rodrigu CHECKED BY: Juan D. Neg	ATE PLANE (m) Geoid12B n (4.124 Ft) 189 m (7.182 Ft)
%Recovery	Depth (Ft)	Graphic Log	Lithol	ogic Description	Well Diagram — well stickup pipe ~ 3 ft	h (Ft)
	- 1 - 2 - 3 - 4 - 5 - 6 - 7		loose, non plasticity, high es		neat cement grout, bentonite seal, 2-3	_ _ 2
	- 8 - 9 - 10 - 11		moderate estimated K, no ode		20–30 mesh silica si ————————————————————————————————————	- 9 - 10 - 10 - 4 Ft - 11
	- 12 - 13 - 13 - 14 - 15		medium dense, non plasticity, beach deposits. Clay, yellowish brown, stiff l estimated K, no odor, alluvia Borehole Termination Depth: 1	<u> </u>		- 12 - 13 - 14 - 14

PROJECT NAME: C CLIENT: AES Pueri ADDRESS: Guayar DRILLERS: GeoEnv	na, Puerto Rico	DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-in	COORDINATES: Y=212153.5554, X=229970 COORD SYS: NAD 83, PR State Plane (m) ELEVATION REF: Orthometric, Geoid12B GROUND ELEVATION: 1.349 m (4.426 Ft) WELL ELEVATION AT TOC: 2.254 m (7.395 I) LOGGED BY: Hardy Rodriguez CHECKED BY: Juan D. Negron, PG	
%Recovery Depth (Ft) Graphic Log	Lithol	ogic Description	Well Diagram — well stickup pipe ~ 3 ft	Depth (Ft)
-1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -	Sandy silt, dark brown, stiff hestimated K, no odor, alluvial Silty sand, yellowish brown, mestimated K, no odor, alluvial Fine to medium sand with feld material, brown, loose hardne K, no odor, alluvial beach dep Clay, yellowish brown, moist plasticity, low estimated K, no Clay, dark brown to dark oli	ardness, high plasticity, low deposits. ardness, high plasticity, low deposits. poist, soft, high plasticity, low deposits. spars minerals and calcareous ess, non plasticity, high estimated osits.	- neat cement grout, 1–3 Ft - bentonite seal, 3–5 Ft - 20–30 mesh silica sand, 5–17 Ft 0.010-in slotted screen screen interval, 7–17 Ft	- 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 17 - 18 - 19
20	Borehole Termination Depth: 2 Water level while drilling interce	0 Ft. epted at 2.5 Ft below ground surface.		20 - -

Fine to medium sand with some angular rock fragments, brown, loose, non plasticity, non odor, high estimated K, fill material. Clayey sand, olive brown, moist, soft, medium plasticity, moderate estimated K, no odor, alluvial deposits. Silty sand, dark yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Fine sand with some feldspars minerals, light brown, moist, medium dense hardness, moderate estimated K, no odor, alluvial deposits. Fine sand with some feldspars minerals, light brown, moist, medium dense hardness, non plasticity, high estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.	PROJECT NA CLIENT: AR ADDRESS: DRILLERS:	AME: C ES Puert Guayan GeoEnv	na, Puerto Rico	DRILLING DATE: May 7, 2019 WELL DEPTH: 14 Ft DIAMETER: 2-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-	COORDINATES: Y=212159.3198, X=230031. COORD SYS: NAD 83, PR State Plane (m) ELEVATION REF: Orthometric, Geoid12B GROUND ELEVATION: 1.280 m (4.199 Ft) WELL ELEVATION AT TOC: 2.155 m (7.070 F LOGGED BY: Hardy Rodriguez CHECKED BY: Juan D. Negron, PG	
non plasticity, non odor, high estimated K, full material. Clayey sand, olive brown, moist, soft, medium plasticity, moderate estimated K, no odor, alluvial deposits. Silty sand, dark yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Bilty sand, dark yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Fine sand with some feldspars minerals, light brown, moist, medium dense hardness, non plasticity, high estimated K, no odor, alluvial beach deposits. Clay, light yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.	%Recovery Depth (Ft)	Graphic Log	Litholo	ogic Description		Depth (Ft)
Fine sand with some feldspars minerals, light brown, moist, medium dense hardness, non plasticity, high estimated K, no odor, alluvial beach deposits. Silty sand, dark yellowish brown, moist, medium dense hardness, medium plasticity, moderate estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits. Clay, light yellowish brown, moist, stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.	1 2 1 3 1 4 1 5 1 6 1 7 1 8 8 1 9 1 9 1 9 1 1 9 1 9 1 1 9 1		non plasticity, non odor, high Clayey sand, olive brown, mois estimated K, no odor, alluvial Silty sand, dark yellowish brow	n estimated K, fill material. it, soft, medium plasticity,moderate deposits. n, moist, medium dense hardness,	heat cement grout, 1–2 Ft bentonite seal, 2–3 Ft	
Borehole Termination Depth: 15 Ft.	- 11 - 12 - 13	† 	dense hardness, non plasticity beach deposits. Silty sand, dark yellowish brow medium plasticity, moderate Clay, light yellowish brown, r plasticity, low estimated K, no Clay, light yellowish brown, r plasticity, low estimated K, no clay the control of t	y, high estimated K, no odor, alluvial n, moist, medium dense hardness, estimated K, no odor, alluvial deposits noist, medium stiff hardness, high odor, alluvial deposits. noist, stiff hardness, high odor, alluvial deposits.	0.010-in slotted screen screen interval, 4-14 Ft	- 10 - 11 - 12 - 13 - 14 - 15

GROUNDWATER LOG Temporary Well TW-109

PROJECT NA CLIENT: AES ADDRESS: C DRILLERS: C	ME: C S Puert Guayan GeoEnv	R: DNA-190167 DRILLING DATE: May 8, 2019 CR Groundwater Monitoring WELL DEPTH: 14 Ft TO Rico, LP DIAMETER: 2-in The plant of the proof	LOGGED BY: Hardy Rodriguez
%Recovery Depth (Ft)	Graphic Log	Lithologic Description	Well Diagram - well stickup pipe ~ 3 ft
-1 -2 -3 -4 -4 -7		Fill material with some organic matter. Silty sand, dark brown, moist, dense hardness, low plasticity, moderate estimated K, no odor, alluvial deposits. Sandy silt, brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.	neat cement grout, 1–2 Ft bentonite seal, 2–3 Ft - 4 - 6 - 7
- 10 - 12 - 14 - 14 - 14 - 14 - 14 - 14 - 14 - 16 -		Silty sand, brown, moist, medium dense hardness, low plasticity, moderate estimated K, no odor, alluvial deposits. Fine to medium sand with some feldspars minerals and calcareous material, light brown, moist, medium dense hardness, non plasticity, high estimated K, no odor, alluvial beach deposits. Clay, light yellowish brown, moist, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits. Clay, yellowish brown, moist, stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.	20–30 mesh silica sand, 3–14 Ft 9 0.010–in slotted screen screen interval, 4–14 Ft 11 12 14
15	/////	Borehole Termination Depth: 15 Ft. Water level while drilling intercepted at 3 Ft below ground surface.	15

GROUNDWATER LOG Temporary Piezometer P-102

PROJ CLIE ADD	ECT N NT: A RESS:	IAME: (ES Puer Guayai	R: DNA-190167 DRILLING DATE: May 10, 2019 CCR Groundwater Monitoring WELL DEPTH: 24 Ft to Rico, LP DIAMETER: 1.5-in ma, Puerto Rico CASING: PVC viroTech, Inc. (Guaynabo, PR) SCREEN: PVC Factory Slotted (0.010-in)	COC ELEV GRO	ORD SY ATION UND E	ATES: Y=212375.0089, X=229 (S: NAD 83, PR State Plane (m N REF: Orthometric, Geoid128 ELEVATION: 4.834 m (15.860 F (ATION AT TOC: 5.542 m (18.	t)
DRIL	LING	METHO	D: Geoprobe 3.25-in ID Dual Tubes			D BY: Hardy Rodriguez ED BY: Juan D. Negron, PG	
%Recovery	Depth (Ft)	Graphic Log	Lithologic Description			Well Diagram well stickup pipe	Depth (Ft)
	- 2 - 2 - 4 - 6 - 6 - 8	7/	Fine to medium sand with some angular rock fragments, reddish brown, medium dense hardness, no plasticity, high estimated K, no odor, fill material. Clayey sand with some angular to sub-angular rock fragments, dark yellowish brown, moist, medium dense hardness, medium plasticity,			neat cement grout, 1–10 Ft	- 2 - 4 - 6 - 8
	- 10 - 12 - 12		moderate estimated K, no odor, fill material. Sandy clay, very dark brown, medium stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.			-bentonite seal, 10-12 Ft	- - 10 - - - - 12 -
ı	- 14 - - - 16		Fine to medium sand with some sub-angular rock fragments, dark yellowis brown, moist, loose hardness, non plasticity, high estimated K, no odor alluvial deposits.				14 16
	- 18 - 20		Clayey silt, moist, very dark gray,soft, high plasticity, low estimated K, vague odor, alluvial deposits.			20–30 mesh silica sand, 12–24 Ft	- 18 - 18 20
	- - - - 22		Fine sand with some feldspars, olive brown, moist, loose hardness, no plasticity, high estimated K, no odor, alluvial beach deposits. Clayey sand, very dark gray,moist,medium dense, medium plasticity, moderate estimated K, vague swamp odor, swamp deposits.			0.010-in slotted screen screen interval 14-24 Ft	- - - - 22
	- - 24 - - - - 26 -		Clay, dark yellowish brown, stiff hardness, high plasticity, low estimated K, no odor, alluvial deposits.				- - 24 - - - 26
	- 28 - - -	<i>V/////</i>	Borehole Termination Depth at: 28 Ft. Water level intercepted at 15 Ft. below ground surface during soil description sampling conducted on 24 May 2017.				- 28 - - -

PROJECT CLIENT ADDRE DRILLE	CT NA T: AE ESS: (ERS: (AME: C S Puert Guayan GeoEnv	R: DNA-190167 CR Groundwater Monitoring to Rico, LP na, Puerto Rico riroTech, Inc. (Guaynabo, PR) : Geoprobe 3.25-in ID Dual T	DRILLING DATE: May 10, 2019 WELL DEPTH: 23 Ft DIAMETER: 1.5-in CASING: PVC SCREEN: PVC Factory Slotted (0.010-	COORE ELEVAT GROUN -in) WELL E	DINATES: Y=212299.0367, X=23011 D SYS: NAD 83, PR State Plane (m) TION REF: Orthometric, Geoid12B ID ELEVATION: 4.609 m(15.121 Ft) LEVATION AT TOC: 4.949 m(16.23 GED BY: Hardy Rodriguez CKED BY: Juan D. Negron, PG	
%Recovery	Depth (Ft)	Graphic Log		nologic Description ne angular rock fragments, yellowish brow		Well Diagram —well stickup pipe	Depth (Ft)
-	- 2 - 4 - 6 - 10 - 12		Clayey sand with angular to su medium dense hardness, med no odor, fill material.	b-angular rock fragments, yellowish browdium plasticity, moderate estimated K,	rial.	neat cement grout, 1–9 Ft bentonite seal, 9–11 Ft	- 2 - 4 - 6 - 8 - 10 - 12 - 14 - 16
-	- 18 - 20 - 22		plasticity, low estimated K, n	n, medium stiff hardness, high plastic	city,	20–30 mesh silica sand, 11–23 Ft 0.010-in slotted screen screen interval 13–23 Ft	- 18 - 18 20 22
	- 24 - 26 - 28		Clay, dark yellowish brown, estimated K, no odor, alluvia	stiff hardness, high plasticity, low I deposits.			- 24 - 24 26 28
-	-30		Borehole Termination Depth at Water level intercepted at 11 F soil description sampling cond	t. below ground surface during			- 30 - - -

APPENDIX B

Groundwater Risk Evaluation



REPORT ON GROUNDWATER RISK EVALUATION AES PUERTO RICO LP GUAYAMA, PUERTO RICO

by Haley & Aldrich, Inc. Chicago, Illinois

for AES Puerto Rico, LP Guayama, Puerto Rico

File No. 133478-002 April 2019

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List of Acronyms

AES-PR AES Puerto Rico LP

AWQC Ambient Water Quality Criteria

BTEX Benzene, Toluene, Ethylbenzene, and Xylene

CCC Continuous Concentration Chronic

CCR Coal Combustion Residual

CPCPRC Chevron Phillips Chemical Puerto Rico Core, LLC

CSM Conceptual Site Model

MCL Maximum Contaminant Level

PRASA Puerto Rico Aqueduct and Sewer Authority

PREPA Puerto Rico Electric Power Authority

RSL Regional Screening Level

SMCL Secondary Maximum Contaminant Level

SW-DAF Surface Water Dilution Attenuation Factor

USEPA United States Environmental Protection Agency

USGS United States Geological Survey

VOC Volatile Organic Compound



1. Introduction

Haley & Aldrich, Inc. (Haley & Aldrich) prepared this groundwater risk assessment for the AES Puerto Rico LP (AES-PR) facility located in the municipality of Guayama, Puerto Rico (site).

AES-PR operates a 454-megawatt coal-fired power plant that produces electricity that is supplied to the Puerto Rico Electric Power Authority (PREPA). Coal combustion residual (CCR) material generated from energy production at the site is processed to produce AGREMAX™, which is placed in a temporary storage area located near the southeastern property boundary. The site is considered a zero-discharge facility that utilizes reclaimed water obtained from the Guayama wastewater treatment plant operated by Puerto Rico Aqueduct and Sewer Authority (PRASA), located approximately 0.5 mile east of the power plant. The reclaimed water is stored in a lagoon in the northern portion of the site. The site is bounded by the inactive former Chevron Phillips Chemical Plant to the east, open land and the inactive former pharmaceutical plant TAPI to the north, open land and the AES Ilumina, LLC solar energy farm to the west, and open land to the south. The location of the site is shown on **Figure 1**.

The temporary AGREMAX™ Storage Area is not a CCR management unit subject to the United States Environmental Protection Agency (USEPA) CCR Rule (USEPA, 2015). However, AES-PR voluntarily monitors groundwater at the temporary AGREMAX™ Storage Area following the USEPA CCR Rule requirements.

2. Objective

In this report, Haley & Aldrich examines groundwater monitoring data collected for the well network associated with the temporary AGREMAX™ Storage Area at the AES-PR facility and collected using the methods and procedures outlined in the USEPA CCR Rule. DNA-Environment, LLC, of Guaynabo, Puerto Rico, conducted the well installation and the groundwater and seawater sampling.

The risk assessment follows current USEPA guidance for risk assessment (USEPA, 1989) and includes consideration of Puerto Rico water quality regulations as appropriate.

3. Approach

The analysis presented in this report was conducted by evaluating the environmental setting of the AES-PR facility, including its location and where CCR management has occurred at the facility. Information on where groundwater is located at the facility, the rate(s) of groundwater flow, the direction(s) of groundwater flow, and where waterbodies may intercept groundwater flow are reviewed and summarized here.

A conceptual model was developed based on this physical setting information, and the model was used to identify what human populations could contact groundwater and/or surface water in the area of the facility. This information was also used to identify where ecological populations could come into contact with surface water. Groundwater data are evaluated on a human health risk basis and an ecological risk basis.



Human health risk assessment is a process used to estimate the chance that contact with constituents in the environment may result in harm to people. Generally, there are four components to the process (USEPA, 1989):

- (1) Hazard Identification/Data Evaluation,
- (2) Toxicity Assessment,
- (3) Exposure Assessment, and
- (4) Risk Characterization.

The USEPA develops "screening levels" of constituent concentrations in groundwater (and other media) that are considered to be protective of specific human exposures. These screening levels are referred to as "Regional Screening Levels," or RSLs, and are published by USEPA and updated twice yearly¹. In developing the screening levels, USEPA uses a specific target risk level (component 4) combined with an assumed exposure scenario (component 3) and toxicity information from USEPA (component 2) to derive an estimate of a concentration of a constituent in an environmental medium, for example groundwater, (component 1) that is protective of a person in that exposure scenario (for example, drinking water). Similarly, ecological screening levels for surface water are developed by Federal and Puerto Rico agencies to be protective of the wide range of potential aquatic ecological resources, or receptors.

Risk-based screening levels are designed to provide a conservative estimate of the concentration to which a receptor (human or ecological) can be exposed without experiencing adverse health effects. Due to the conservative methods used to derive risk-based screening levels, it can be assumed with reasonable certainty that concentrations below screening levels will not result in adverse health effects, and that no further evaluation is necessary. Concentrations above conservative risk-based screening levels do not necessarily indicate that a potential risk exists, but indicate that further evaluation may be warranted. As described further below, through this evaluation which involves the evaluation of groundwater flow, groundwater analytical data, and surface water analytical data, it was confirmed that there is no impact on drinking water and there is no evidence of impact to human health or the environment.

The data in this report were evaluated using human health risk-based and ecological risk-based screening levels drawn from Federal and Puerto Rico sources. The screening levels are used to determine if the concentration levels of constituents could pose a risk to human health or the environment. The evaluation also considers whether constituents that may be present in groundwater and surface water above screening levels could be due to the CCR management operations.

4. Conceptual Site Model

A conceptual site model (CSM) is used to evaluate the potential for human or ecological exposure to constituents that may have been released to the environment. Some of the questions posed during the CSM evaluation include:



¹ USEPA Regional Screening Levels (November 2018). http://www.epa.gov/reg3hwmd/risk/human/rb-concentration_table/Generic_Tables/index.htm

What is the source? How can constituents be released from the source? What environmental media may be affected by constituent release? How and where do constituents travel within a medium? Is there a point where a receptor (human or ecological) could contact the constituents in the medium? Are the constituent concentrations high enough to potentially exert a toxic effect?

AES-PR is located in the municipality of Guayama, Puerto Rico. The site is 1870 feet north of the Caribbean Sea at Las Mareas Harbor (approximately 1/3 mile). See **Figure 1**.

AES-PR is in an industrial area of Guayama. The neighboring inactive Chevron Phillips Chemical Puerto Rico Core, LLC (CPCPRC) facility to the east of the AES-PR site is a source of organic and potentially other constituents in groundwater at AES-PR. Sulfolane and benzene, toluene, ethylbenzene, and xylene (BTEX) plumes in the upper and lower aquifers at CPCPRC² have migrated to the southeastern portion of the AES-PR property. The inactive former pharmaceutical plant TAPI³ to the north, and upgradient (similar to upstream) of AES-PR has also released organics to the groundwater. AES-PR is not the source of plumes or releases from neighboring sites. In addition, a USEPA Superfund site (Fibers Public Supply Wells⁴) is located approximately one mile to the northeast.

For the evaluation of the AGREMAX™ management operations at AES-PR, the temporary AGREMAX™ Storage Area in the southeastern area of the site is the potential source. The storage area is located on the ground surface and does not extend into the subsurface or the water table. Constituents present in the AGREMAX™ can be dissolved into infiltrating water (from precipitation and wetting for dust control) and those constituents may move through the subsurface and could then be present in shallow groundwater. Constituents could move with groundwater as it flows, usually in a downgradient/downhill direction. The general direction of groundwater flow at the site is south/southwest toward Las Mareas Harbor.

AES-PR is located in what is defined by the US Geological Survey (USGS) as the south coast alluvial aquifer (**Figure 2**) (USGS). The USGS has delineated the hydrologic units in the area of the south coast alluvial aquifer according to the surface topography and hydrologic data. Each hydrologic unit is associated with a code; AES-PR is located in the hydrologic unit: 210100040416 (**Figure 3**). Within these hydrologic units, surface water flows from areas of high elevation to areas of low elevations; surface water in this hydrologic unit is expected to generally move southward and discharge to the sea.

Groundwater moves slowly through the rock and soils beneath the ground. Like surface water, it also moves from areas of high elevation to areas of low elevation and can move into adjacent surface water. The general groundwater direction within the hydrologic unit is from north to south towards the sea – on the eastern edge of the watershed, groundwater can flow in a southeast direction – and on the western edge of the watershed, groundwater can flow in a southwest direction. Therefore, any potential release of constituents to groundwater from either the Chevron site, the TAPI site, or AES-PR will be limited in extent by the direction of groundwater flow and will not impact areas further inland.

At AES-PR, groundwater flows generally towards Las Mareas Harbor. This means that if there is a release of constituents to groundwater from the AES-PR facility, it will be confined to the area of

HALEY

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² https://www.epa.gov/hwcorrectiveactionsites/hazardous-waste-cleanup-chevron-phillips-chemical-puerto-rico-core-guayama

³ https://www.epa.gov/hwcorrectiveactionsites/hazardous-waste-cleanup-tapi-puerto-rico-incorporated-guayama-puerto-rico

⁴ https://cumulis.epa.gov/supercpad/cursites/csitinfo.cfm?id=0202559

groundwater at the plant and downgradient. Any impacted groundwater beneath the site is not expected to migrate inland. As the plant is very close to the ocean (1870 feet), the area of groundwater that could be affected by facility operations is also very small and limited. Along the coastlines there is saltwater intrusion into groundwater; the extent of this intrusion varies along coastlines, see **Figure 4**.

HYDROLOGIC CYCLE

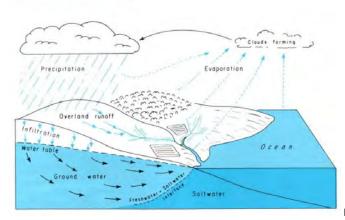


Figure 4: Illustration of Hydrologic Cycle

CCR-derived constituents present in groundwater may move to adjacent surface water; here, that could be the Caribbean Sea at Las Mareas Harbor. Thus, the environmental media of interest for this evaluation are:

- Groundwater at the facility; and
- Las Mareas Harbor surface water.

Las Mareas Harbor is used for ship loading and unloading, but there are public access areas and small beaches present and, therefore, it could also be used for recreation. The area surrounding Las Mareas Harbor can be used for human recreation – wading, swimming, boating, fishing, and as habitat for marine aquatic species and avian receptors.

The neighboring inactive Chevron Phillips Chemical Puerto Rico Core, LLC (CPCPRC) facility to the east of the AES-PR site is another potential source of constituents in groundwater. CPCPRC processed naphtha into refined hydrocarbon products from 1966 to 2008. Sulfolane and benzene, toluene, ethylbenzene, and xylene (BTEX) plumes in the upper and lower aquifers at CPCPRC have migrated to the southeastern portion of the AES-PR property. In 2017, USEPA issued a request for public comments on the proposed remedy decision for CPCPRC, which includes groundwater remediation for BTEX and sulfolane impacts (USEPA, 2017).

There are no on-site users of shallow groundwater adjacent to AES-PR. CPCPRC conducted a private well investigation as part of a sitewide risk characterization (CPCPRC, 2007). As documented in the 2007 CPCPRC Risk Characterization Report, there are some census-designated communities and smaller villages near the CPCPRC and AES-PR facilities (Guayama, Quebrada, Corazon, Jobos and Puerto Jobos, and Barrancas), however none of these communities is considered downgradient (i.e., south of AES-PR and CPCPRC) and, therefore, would not be impacted by groundwater from either facility. Las Mareas is the only community downgradient of CPCPRC and AES-PR, and according to the 2007 CPCPRC Risk Characterization Report, houses in Las Mareas obtain water from a PRASA potable water pipeline and no



existing private wells were found in the area. The 2007 CPCPRC Report also did not find any domestic wells constructed near the CPCPRC facility.

Thus, with respect to shallow groundwater, there are no users of the groundwater near the AES-PR facility. Depth to groundwater in this area is approximately 10 feet, thus contact with groundwater during a short-term construction/excavation event is unlikely.

A depiction of the conceptual site model is shown in **Figure 5**. The potentially complete exposure pathways identified in the figure are those evaluated here.

Figure 6 shows the locations of groundwater sample locations, and the location in Las Mareas harbor where a seawater sample was collected. Based on this conceptual site model and the facility setting, samples collected from groundwater monitoring wells and Las Mareas Harbor have been included in the evaluation. The samples have been analyzed for constituents that are commonly associated with CCR, as discussed below. However, it is recognized by the USEPA that all of these constituents can also be naturally occurring and can be found in rocks, soils, water and sediments; thus, the it is necessary to understand what the naturally occurring background levels are for these constituents. The CCR Rule requires sampling and analysis of upgradient and/or background groundwater just for this reason. The sampling is detailed in the next section. Groundwater samples have also been analyzed for volatile and semi-volatile organic compounds to evaluate groundwater impacts at AES-PR from the adjoining property to the east, as discussed above.

To answer the question, "Are the constituent concentrations high enough to potentially exert a toxic effect?" health risk-based screening levels from Federal and Puerto Rico sources are used for comparison to the data. Groundwater is evaluated using a tiered approach. As a first conservative step, all groundwater data are compared to risk-based drinking water screening levels, even though there are no on-site users of groundwater adjacent to AES-PR. Groundwater results are also compared to human recreational screening levels and ecological screening levels as a conservative evaluation, even though there is no direct exposure to groundwater by human or ecological receptors. The Las Mareas Harbor sample is compared to risk-based human recreational screening levels, and to ecological screening levels.

For the second step, a surface water dilution and attenuation factor (SW-DAF) has been derived for groundwater that may flow to the Caribbean Sea at Las Mareas Harbor. If the concentrations in groundwater are below the SW-DAF-applied risk-based screening levels for ecological receptors and human health recreational receptors, no further evaluation is necessary. If a groundwater concentration is above a SW-DAF-applied risk-based screening level, that does not necessarily mean that surface water will be adversely impacted by the groundwater, only that further evaluation may be warranted, as discussed further below.

5. Samples Used for Evaluation

5.1 GROUNDWATER

Five (5) groundwater monitoring wells and four (4) temporary wells were installed to evaluate groundwater in the uppermost aquifer at AES-PR under the CCR Rule. The monitoring wells are summarized below and shown in **Figure 6**.



- MW-1 and MW-2 Upgradient. These wells were installed to represent background
 groundwater in the uppermost aquifer. MW-2 was installed outside of site operation areas to
 evaluate groundwater potentially impacted by the CPCPRC facility to the east.
- MW-3 through MW-5 Downgradient. These wells were installed downgradient of the temporary AGREMAX™ Storage Area to evaluate the potential impacts to groundwater in the uppermost aquifer.
- TW-A, TW-B, TW-C, and TW-D. These four temporary monitoring wells were installed within property boundaries along the north-south axis of AES-PR and the AES Ilumina, LLC solar energy farm properties to evaluate potential effects of saltwater intrusion on the water quality of downgradient monitoring wells.

5.2 LAS MAREAS HARBOR

One seawater sample (not required by the CCR Rule for compliance) from Las Mareas Harbor was taken in July 2018. The location of the Las Mareas Harbor sample is shown on **Figure 6**.

5.3 SAMPLE ANALYSIS

The CCR Rule identifies the constituents that are included for groundwater testing; these are:

Boron	Antimony	Lead
Calcium	Arsenic	Lithium
Chloride	Barium	Mercury
рН	Beryllium	Molybdenum
Sulfate	Cadmium	Selenium
TDS	Chromium	Thallium
Fluoride	Cobalt	Radium 226/228

Seven rounds of monitoring groundwater samples collected from August 2017 through June 2018 and two rounds of temporary well samples collected from December 2017 and July 2018 were analyzed for the above constituents. The monitoring wells were resampled in October 2018 and analyzed for a subset of constituents, per the CCR Rule.

So as to create an appropriate dataset for comparison, the Las Mareas Harbor sample collected in July 2018 was analyzed for all the above parameters except for radium 226/228, which was not detected in groundwater above the drinking water standard. Two sets of analyses were conducted on the Las Mareas Harbor sample. The sample was analyzed for the list above (referred to as the "total [unfiltered]" results), and then an aliquot of each sample was filtered to remove sediments/particulates and then analyzed (referred to as the "dissolved [filtered]" results). This is an important step for the analysis of surface water samples for two reasons:

- Surface water can carry a large sediment load the total (unfiltered results) include constituent concentrations that are associated with sediment and not the water; and
- Some of the ecological screening levels used to evaluate the results apply only to dissolved (filtered) data.



5.4 SAMPLE RESULTS

Table 1 provides the results of the groundwater and seawater sampling.

6. Risk-Based Screening Levels

A comprehensive set of risk-based screening levels have been compiled for this evaluation for the types of potential exposures identified in the conceptual site model discussion above:

- Human health drinking water consumption;
- Human health recreational use of marine surface water; and
- Aquatic ecological receptors for marine surface water.

Table 2 provides the human health drinking water levels available from the Puerto Rico sources and from Federal sources. **Table 3** provides the marine human health recreational and ecological screening levels available from the Puerto Rico sources and from Federal sources.

6.1 DRINKING WATER SCREENING LEVELS

The human health screening levels for drinking water are obtained from USEPA and Puerto Rico sources and address the drinking water exposure pathway. These sources are:

- Puerto Rico Water Quality Standards Regulation. Environmental Quality Board. Rule 1303.1
 Water Quality Standards. Class SG Groundwater (PR EQB, 2016).
- USEPA 2018 Edition of the Drinking Water Standards and Health Advisories (USEPA, 2018b).
- USEPA Regional Screening Levels (RSLs), November 2018, Values for Tap Water (USEPA, 2018a).

It is important to note that the CCR Rule limits the evaluation of groundwater monitoring data of CCR management areas to Federal USEPA Maximum Contaminant Levels (MCLs), to risk-based screening levels for cobalt, lead, lithium, and molybdenum (USEPA, 2018c), or to a comparison with site-specific background. In addition to the MCLs that are enforceable for municipal drinking water supplies, there are Federal secondary MCLs, or SMCLs, that are generally based on aesthetics (taste, color) and are not risk-based. The USEPA also provides RSLs for tapwater (drinking water) that are used to supplement this evaluation. The tapwater RSLs are based on a target risk level of one in one million (10-6) and a target noncancer hazard index of 1.

Table 2 shows the hierarchy of drinking water-based screening levels used in this evaluation. For the selected Federal screening levels, the hierarchy is: USEPA MCL; where an MCL is not available the USEPA tap water RSL is selected, where an RSL is not available the USEPA SMCL is selected. For the selected Puerto Rico screening levels the hierarchy is: Puerto Rico Groundwater Quality Standards, USEPA MCL; USEPA tap water RSL, USEPA SMCL. The selected Puerto Rico screening levels are used in this evaluation – the Federal levels are provided for comparison.

The use of a more comprehensive set of screening levels in this evaluation versus the MCLs as supplemented by USEPA RSLs and SMCLs (2018a,b) provides a broader risk-based evaluation of the groundwater data than would be provided by the CCR Rule requirements.



6.2 RECREATIONAL SCREENING LEVELS

The human health recreational screening levels for marine surface water are obtained from USEPA and Puerto Rico sources and address the fish/shellfish consumption pathway (where such values are available). These sources are:

- Puerto Rico Water Quality Standards Regulation. Environmental Quality Board. Rule 1303.1
 Water Quality Standards. Class SB and SC Coastal and Estuarine Waters. Values based on protection of the water body or aquatic life for reasons of human health. (PR EQB, 2016).
- USEPA Ambient Water Quality Criteria (AWQC) Human Health Consumption of Organism Only (USEPA, 2019a). Human Health Consumption Organism Only values apply to freshwater and estuarine water and use a fish ingestion rate based on consumption of freshwater and estuarine finfish and shellfish.

Table 3 presents the human health screening levels for recreational exposures and identifies the selected Federal and Puerto Rico human health risk-based screening levels for further evaluation. The selected Puerto Rico based screening levels are used in this evaluation; the selected Federal based screening levels are provided for comparison. Note that this evaluation of human uses of surface water are above and beyond the requirements of the CCR Rule.

6.3 ECOLOGICAL SCREENING LEVELS

The ecological risk-based screening levels for marine surface water are also provided in **Table 3**. Some screening levels apply only to total surface water concentrations, and some screening levels apply to only dissolved surface water concentrations. Values for both scenarios are provided. The table also identifies the selected ecological risk-based screening levels for further evaluation. Note that this ecological evaluation of surface water is above and beyond the requirements of the CCR Rule.

Ecological screening levels were obtained from both Puerto Rico and USEPA sources:

- Puerto Rico Water Quality Standards Regulation. Environmental Quality Board. Rule 1303.1
 Water Quality Standards. Class SB and SC Coastal and Estuarine Waters. Values based on
 protection of the water body for the propagation and preservation of aquatic species or species
 dependent on the water body. (PR EQB, 2016).
- USEPA chronic saltwater AWQC (USEPA, 2019b). The continuous concentration criterion (CCC) (Chronic AWQC) is the USEPA national water quality criteria recommendation for the highest concentration of a toxicant or an effluent to which organisms can be exposed indefinitely without causing unacceptable effect.

7. Risk-Based Evaluation

This section describes the risk-based approach for evaluation of the groundwater and surface water data from AES-PR. The level of analysis and comparison to risk-based screening levels presented below is above and beyond the requirements of the CCR Rule. This report serves to supplement those requirements by providing the risk-based analysis of groundwater and surface water, so that the groundwater results can be understood in their broader environmental context.



7.1 RISK-BASED EVALUATION OF GROUNDWATER

Groundwater data from eight rounds of groundwater monitoring, and two rounds of temporary well groundwater monitoring were compared to the Puerto Rico based human health risk-based drinking water screening levels. **Figure 6** shows the location of the monitoring wells and temporary wells that are all located at the edge of the AES-PR facility and AES Ilumina, LLC solar energy farm.

Tables 4 and 5 compare the results of all sampling rounds to Puerto Rico based human health drinking water screening levels, for total and dissolved groundwater concentrations, respectively. The majority of the results indicate concentration levels below the human health risk-based drinking water screening levels.

A limited number of parameters are above screening values for some, but not all, sampling events. Of all of the laboratory analyses conducted for these wells, lithium and molybdenum are above drinking water screening levels in MW-4, and molybdenum and selenium are above drinking water screening levels in MW-3. For the constituents with the most results above the screening levels (chloride, sulfate, and TDS (total dissolved solids)), results are also above screening levels in the background wells MW-1 and MW-2, although at lower concentrations.

The groundwater data are also compared to Puerto Rico based human health recreational and ecological screening levels and are presented in **Tables 6 through 9**. Note that groundwater is not used for "recreation" and ecological receptors are not directly exposed to groundwater, so this comparison serves as a conservative approach.

- **Tables 6 and 7** Comparison to human health recreational screening levels Only total and dissolved concentrations of arsenic are above their screening levels.
- Tables 8 and 9 Comparison to ecological screening levels Only total and dissolved concentrations of selenium in MW-3 are above their screening levels. Two sample results for pH in MW-5 and TW-D are below the pH screening level range.

As described further within this report, concentrations above screening levels alone does not indicate a human health risk basis or an ecological risk basis. Rather, as discussed below, this report concludes that these concentrations of constituents in groundwater at AES-PR do <u>not</u> pose a risk to human health or the environment.

7.2 RISK-BASED EVALUATION OF HARBOR SAMPLE

As noted in Section 4, groundwater in the south coast alluvial aquifer is limited in extent in the vicinity of the AES-PR site (see **Figures 3 and 4**). Groundwater moves from areas of high elevation to areas of low elevation and can move into adjacent surface water. In the vicinity of the AES-PR site, the predominant direction of groundwater flow is to the south towards Las Mareas Harbor. Thus, a sample of sea water collected at Las Mareas Harbor was used for this evaluation. The comparison to risk-based screening levels of the analytical results for the Las Mareas Harbor Sea sample are presented in **Table 10**.

• **Table 10** – Only total and dissolved concentrations of arsenic are above the human health based recreational screening level. However, these concentrations are comparable to seawater concentrations worldwide. All results are below risk-based ecological screening levels.



There are no analytical results for the Las Mareas Harbor sample that are above marine ecological screening levels, and with the exception of arsenic no analytical results above human health recreational screening levels. Thus, the Las Mareas Harbor sample results do not show evidence of impact of constituents derived from AES-PR. This is important in that the absence of concentrations above risk-based screening levels means that there is not a significant pathway of exposure.

Table 11 provides literature data for seawater from two sources (USGS, 1985; Antoni, 2006), and the data from the Las Mareas Harbor sample. The results from the Las Mareas Harbor sample are consistent with natural levels of these constituents in seawater. This indicates that there is no measurable effect of groundwater at the AES-PR facility on surface water in the harbor. Note that the background concentration of arsenic in the world's seawater (0.0026-0.003 mg/L) is also above the human health recreational screening level of 0.00014 mg/L.

7.3 DEVELOPMENT AND APPLICATION OF A GROUNDWATER TO SURFACE WATER DILUTION ATTENUATION FACTOR

If a groundwater concentration is above a surface water screening level, that does not mean that surface water will be adversely impacted by the groundwater. Dilution and attenuation mechanisms can occur as groundwater moves to surface water. This section describes the approach to evaluating the magnitude of dilution effects resulting from the mixing of groundwater that may flow from beneath the temporary AGREMAX™ Storage Area to the nearby surface water body − the Las Mareas Harbor (Figure 1), through the development of a Surface Water Dilution Attenuation Factor (SW-DAF). This factor is then applied to the target risk-based marine water concentrations to identify target groundwater concentrations that are protective of surface water. These risk-based target groundwater concentrations (protective of the Las Mareas Harbor) are used to evaluate the current groundwater data, and can be used to evaluate future groundwater data.

The primary driving force responsible for migration of constituents from the temporary AGREMAX™ Storage Area is infiltration of precipitation from ground surface to groundwater. The direction of groundwater flow is generally toward the Las Mareas Harbor.

To make a conservative estimate of the potential impacts of groundwater to the Las Mareas Harbor, a SW-DAF has been calculated. The SW-DAF describes the effect of mixing on constituent concentrations expected for the surface water body potentially receiving the groundwater. Currently available on-site groundwater information, groundwater elevation data and other hydrogeological data, and Las Mareas Harbor data were used for this evaluation.

The details of the SW-DAF development and results are provided in **Appendix A**. The evaluation took into account the potential for infiltration in the temporary AGREMAX™ Storage Area and the subsurface, groundwater flow to Las Mareas Harbor, and the flow rate of the seawater flushing in the Las Mareas Harbor. Tidal data for the National Oceanic & Atmospheric Administration station in Las Mareas, Puerto Rico (Station ID: 9755679) were used to calculate a conservative estimate of the seawater flushing volume each day for Las Mareas Harbor.



7.4 SURFACE WATER DILUTION ATTENUATION FACTOR

The SW-DAF was calculated to quantify the dilution of groundwater that may flow from beneath the temporary AGREMAX™ Storage Area towards the Las Mareas Harbor. The most conservative assumptions were used wherever possible. For groundwater that may flow to the Las Mareas Harbor, the conservatively calculated SW-DAF is **1,300** (a unitless value).

7.5 APPLICATION OF THE SW-DAF

Table 12 presents the selected Federal and Puerto Rico human health and ecological screening levels (from **Table 2**) and identifies the lowest screening level for surface water for the potential exposure scenarios. **Table 12** also shows the application of the SW-DAF to calculate risk-based screening levels for each of the Appendix III and Appendix IV groundwater constituents. For each constituent, the human health recreational screening levels and the ecological screening levels are presented. The lowest of the screening levels is then identified for surface water. The SW-DAF is then applied to this lowest screening level for surface water to result in the target groundwater concentrations developed based on the SW-DAF for the Las Mareas Harbor of 1,300.

Table 12 identifies the maximum groundwater concentration of each constituent detected in the AES-PR monitoring wells. The comparison between the target levels and the maximum concentrations indicates that there is a wide margin of safety between the two values. This margin is shown in the last column of the tables. To illustrate, concentration levels of arsenic and lead would need to be more than 20 and 400 times higher, respectively, than currently measured levels before an adverse impact in the Las Mareas Harbor could occur. As noted above, even the naturally occurring concentration of arsenic in seawater is above the human health recreational screening level.

This means that not only do the present concentrations of constituents in groundwater at AES-PR not pose a risk to human health or the environment, but even much higher concentrations would not be harmful. This comprehensive evaluation demonstrates that there are no adverse impacts on human health from either Las Mareas Harbor or groundwater uses resulting from AGREMAX™ management practices at AES-PR.

8. Conclusion

Table 13 provides a summary of groundwater and Las Mareas results that are above Puerto Rico selected human health drinking water, human health recreational, and ecological screening levels. The screening and the Las Mareas seawater sample results indicate that there is no impact of the AGREMAX™ management practices at AES-PR on surface water. The striking aspect of the analysis shown in **Table 13** is how few results are above a conservative risk-based drinking water screening level for human health, given that the wells are located at the base of the AGREMAX™ storage area.

This investigation demonstrates that the impacts of the temporary AGREMAX™ Storage Area are limited. There is no impact on drinking water and there is no evidence of impact to human health or the environment. There are no downgradient users of groundwater as drinking water – thus, there is no impact on drinking water. Las Mareas Harbor does not show impacts. There is no exposure to CCR-derived constituents detected in groundwater at the AES-PR facility – either via groundwater use or surface water. Even for the very few results that may be above screening values for some of the



sampling events, there is no complete drinking water exposure pathway to groundwater. Where there is no exposure, there is no risk.

AES-PR is continuing with further evaluation and actions at the facility, consistent with the requirements of the CCR Rule.

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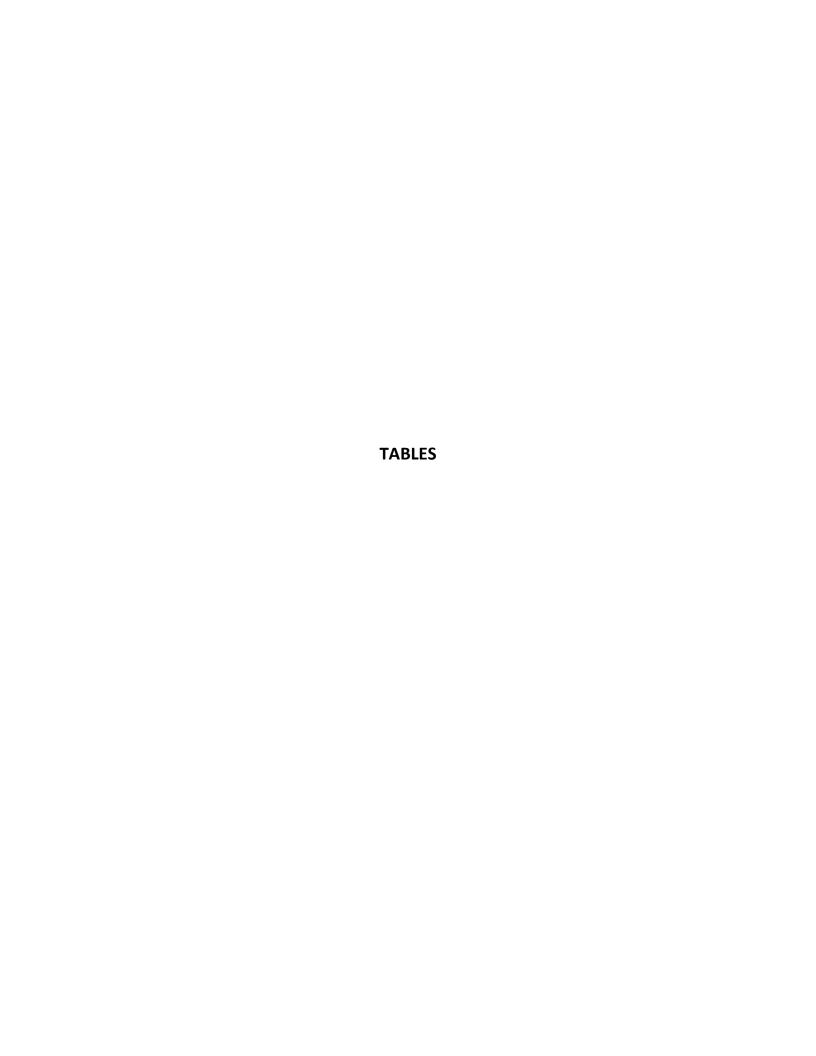


TABLE 1 CCR RULE GROUNDWATER MONITORING, TEMPORARY WELL, AND HARBOR SAMPLE ANALYTICAL RESULTS AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

					Appendix	(III (a)			Appendix III							Ant	pendix IV (b)	1								/ \	
						(-)			and IV (a, b)														Radium		Sulfolane and V	OCs (c) Methyl tert-	
		Constituent	Boron	Calcium	Chloride	На	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury	Molybdenum	Selenium	Thallium	226/228	Chlorobenzene	Isopropylbenzene		Sulfolane
Location ID	Sampling Event Date	Fraction	mg/L	mg/L	mg/L	Ś.U.	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	pCi/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 -	8/8/2017	Total	0.26	140	240	6.87	340	1100	0.47	< 0.001	< 0.00046		< 0.00034		< 0.0011		< 0.00035			0.0022 J	0.0073	< 0.000085	< 0.0899	NA	NA	NA	NA
Background Well	8/15/2017	Total	0.26	150	260	7.07	410	1400	0.53	< 0.001							< 0.00035			< 0.00085	0.0062	< 0.000085	0.205	NA	NA NA	NA	NA
vveii	8/22/2017 8/29/2017	Total	0.25 0.25 B	150 160	220 240	6.74 6.92	400 390	1400 1400	0.55 0.58 B	< 0.001	< 0.00046		< 0.00034 < 0.00034				< 0.00035			0.0023 J < 0.00085	0.0065 0.0057	< 0.000085 < 0.000085	0.270 0.576	NA NA	NA NA	NA NA	NA NA
	9/12/2017	Total Total	0.25 B	160	220	6.9	410	1400	0.38 B	< 0.001							< 0.00035		< 0.00007	0.00083	0.0057	< 0.000085	NA	NA NA	NA NA	NA NA	NA NA
	6/25/2018	Total	0.25	130	260 F1	7.13	510 F1	1500	0.61	< 0.0010	< 0.00046								< 0.000070	< 0.00085	0.025	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	< 0.00058
	6/25/2018	Dissolved	0.28	130	260 F1	NA	490 F1	1600	0.61		< 0.00046		< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.025	< 0.000085	NA	NA	NA	NA	NA
.=0.181/.0	10/1/2018	Total	0.24	120	200	7.33	400	1300	0.69		< 0.00046			< 0.00034	NA	0.00050 J		< 0.0011		< 0.00085	0.015	NA	0.495	NA	NA	NA	NA
AES MW-2 - Background	8/8/2017 8/15/2017	Total Total	0.16 0.17	88 88	37 37	6.53 6.83	7.7 7.1	460 470	0.36 0.4	< 0.001 < 0.001	< 0.00046 0.00047 J		< 0.00034		< 0.0011 < 0.0011				< 0.00007 < 0.00007	< 0.00085 < 0.00085		< 0.000085 < 0.000085	< 0.129 0.545	NA NA	NA NA	NA NA	NA NA
Well	8/22/2017	Total	0.17	89	37	6.54	10	450	0.4	< 0.001	< 0.00047 3		< 0.00034						< 0.00007	0.00005		< 0.000085	< 0.0379	NA NA	NA NA	NA NA	NA NA
	8/29/2017	Total	0.17 B	100	37	6.68	16	470	0.42 B	< 0.001	< 0.00046		< 0.00034						< 0.00007	< 0.00085		< 0.000085	0.113	NA	NA.	NA.	NA
	9/12/2017	Total	0.17	94	36	6.65	9.8	480	0.35	< 0.001	< 0.00046		< 0.00034	< 0.00034	< 0.0011	< 0.0004	< 0.00035	< 0.0032	< 0.00007	0.00094 J	0.00046 J	< 0.000085	NA	NA	NA	NA	NA
	6/25/2018	Total	0.16	110	140	6.84	43	740	0.52		< 0.00046								< 0.000070			< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0069 J
	6/25/2018	Dissolved	0.17	110 110	130	NA	44 15	730 690	0.5		< 0.00046	0.15	< 0.00034		< 0.0011 NA				< 0.000070			< 0.000085 NA	NA 0.004	NA	NA NA	NA	NA
AES MW-3	10/1/2018 8/8/2017	Total Total	0.16	290	85 2900	7.04 6.74	630	6000	0.67	< 0.0010	< 0.00046			< 0.00034		0.00058 J	NA < 0.00035	0.0014 J		< 0.00085	< 0.00024	< 0.000085	< 0.321	NA NA	NA NA	NA NA	NA NA
7.20 0	8/15/2017	Total	0.85	320	3400	7.1	1300	7600	2.1	< 0.001	0.0034		< 0.00034				< 0.00035		< 0.00007	0.16	0.098	< 0.000085	0.142	NA.	NA.	NA.	NA.
	8/22/2017	Total	0.83	340	3600	6.78	1500	8600	2.2	< 0.001	0.0021	0.37	< 0.00034	< 0.00034	< 0.0011	0.0023 J	< 0.00035	0.0075	< 0.00007	0.2	0.13	< 0.000085	0.212	NA	NA	NA	NA
	8/29/2017	Total	0.90 B	390	3700	7.01	1700	8300	2.3 B	< 0.001	0.0024		< 0.00034				< 0.00035		< 0.00007	0.22	0.14	< 0.000085	0.0888	NA	NA	NA	NA
	9/12/2017 6/25/2018	Total Total	0.9 1.2	370 330	3900 4400	7.03 7.23	2300 2800	9900 11000	1.9 1.6	0.0012 J < 0.0010	0.0029 0.0018		< 0.00034 < 0.00034				< 0.00035 < 0.00035		< 0.00007	0.28	0.18	< 0.000085 < 0.000085	NA NA	NA 0.0027	NA 0.00053 J	NA . 0.0074	NA 0.004 J
	6/25/2018	Dissolved	1.2	330	4300	7.23 NA	2500	10000	1.6	< 0.0010	0.0018		< 0.00034				< 0.00035		< 0.000070	0.22	0.21	< 0.000085	NA NA	0.0027 NA	0.00053 J NA	< 0.00074 NA	0.004 J NA
	10/1/2018	Total	1.0	330	4700	7.43	3300	13000	1.6	< 0.0010	0.0024	0.19		< 0.00034	NA	0.0034	NA	0.021	NA	0.22	0.23	NA	0.511	NA NA	NA.	NA	NA
AES MW-4	8/8/2017	Total	3.4	590	9800	6.91	15000	41000	0.63	< 0.001	0.0036	0.057			< 0.0011		< 0.00035	1	< 0.00007	0.44	0.011	< 0.000085	0.527	NA	NA	NA	NA
	8/8/2017 Dup	Total	3.4	620	9900	6.91	15000	41000	0.61	0.0014 J	0.0031	0.057	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	1	< 0.00007	0.45	0.011	< 0.000085	0.137	NA	NA	NA	NA
	8/16/2017	Total	3.7	620	11000	7.08	16000	43000	0.63	< 0.001	0.0037		< 0.00034				< 0.00035		< 0.00007	0.4	0.0048	< 0.000085	0.112	NA	NA	NA	NA
	8/16/2017 Dup 8/23/2017	Total Total	4.1 3.8	630 620	10000 9800	7.08 7.09	16000 15000	43000 42000	0.61 0.65	< 0.001	0.0033		< 0.00034 < 0.00034				< 0.00035 < 0.00035	1.1 0.88	< 0.00007 < 0.00007	0.38 0.44	0.0061 0.006	< 0.000085 < 0.000085	0.507 < 0.0545	NA NA	NA NA	NA NA	NA NA
	8/23/2017 8/23/2017 Dup	Total	3.8	590	9800	7.09	15000	42000	0.65	< 0.001	0.0026					0.0017 J		1.1	< 0.00007	0.44	0.0065	< 0.000085	< 0.0545 0.0942	NA NA	NA NA	NA NA	NA NA
	8/30/2017 Dup	Total	3.6 B	670	11000	7.14	16000	42000	0.68	< 0.001	0.0023		< 0.00034			0.0017 J		0.9	< 0.00007	0.4	0.0058	< 0.000085	0.403	NA NA	NA.	NA.	NA.
	8/30/2017 Dup	Total	3.6 B	670	11000	7.14	16000	41000	0.68	< 0.001	0.0024		< 0.00034			0.0016 J	< 0.00035	0.98	< 0.00007	0.42	0.0054	< 0.000085	< 0.146	NA	NA	NA	NA
	9/12/2017	Total	3.2	600	10000	7.12	17000	42000	0.53	< 0.001	0.0035		< 0.00034				< 0.00035	0.75	< 0.00007	0.41	0.013	< 0.000085	NA	NA	NA	NA	NA
	9/12/2017 Dup	Total	3.4	610	10000	7.12	17000	43000	0.63	< 0.001	0.0038		< 0.00034				< 0.00035	0.86	< 0.00007	0.42	0.014	< 0.000085	NA	NA	NA	NA	NA
	6/26/2018 6/26/2018 Dup	Total Total	3.2 3.2	460 440	9100 8900	7.27 7.27	12000 12000	16000 17000	0.76 0.76	0.0023 J 0.0019 J	0.0024 0.0021		< 0.00034 < 0.00034		< 0.0011 < 0.0011	0.0016 J 0.0016 J	< 0.00035	0.54 0.57	< 0.000070 < 0.000070	0.55 0.58	0.0064 0.0055	< 0.000085 < 0.000085	NA NA	< 0.00050 < 0.00050	< 0.00053 < 0.00053	< 0.00074 < 0.00074	0.0053 J 0.0046 J
	6/26/2018	Dissolved	3.4	450	9100	NA	11000	13000	0.76	< 0.0019 3	0.0021		< 0.00034		< 0.0011	0.0010 J		0.56	< 0.000070	0.58	0.0055	< 0.000085	NA	NA	NA	NA	0.0046 J
	6/26/2018 Dup	Dissolved	3.5	450	8700	NA	11000	14000	0.74	< 0.0010	0.0022	0.046	< 0.00034	0.00035	< 0.0011	0.0016 J	< 0.00035	0.59	< 0.000070	0.6	0.0054	< 0.000085	NA	NA	NA	NA	NA
	10/2/2018	Total	2.6	280	5600	7.41	6000	21000	1.0	< 0.0010	0.0031	0.035		0.00057 J	NA	0.0016 J	NA	0.38	NA	0.74	0.0043	NA	< 0.0708	NA	NA	NA	NA
	10/2/2018 Dup	Total	2.6	250	5300	7.41	6200	22000	1.0	< 0.0010	0.0027	0.036		0.00051 J	NA	0.0016 J	NA	0.34	NA	0.76	0.0048	NA	< 0.168	NA	NA	NA	NA
AES MW-5	8/9/2017 8/16/2017	Total Total	0.37 0.46	850 890	3800 3800	6.52 6.61	2500 2700	8200 7900	0.42 0.45	< 0.001 < 0.001	0.0032 0.0024		< 0.00034 < 0.00034		< 0.0011	0.0034	< 0.00035 < 0.00035		< 0.00007 < 0.00007	0.0022 J 0.0086 J	0.01 0.013	< 0.000085 < 0.000085	0.473 0.576	NA NA	NA NA	NA NA	NA NA
	8/22/2017	Total	0.39	800	3700	6.49	2500	11000	0.45	< 0.001	0.0024				< 0.0011		< 0.00035		< 0.00007	0.0080 J	0.013	< 0.000085	0.102	NA NA	NA NA	NA NA	NA NA
	8/29/2017	Total	0.39 B	930	3700	6.79	2600	9800	0.48	< 0.001	0.0021	0.036	< 0.00034		< 0.0011		< 0.00035		< 0.00007	0.0057 J	0.0099	< 0.000085	0.601	NA	NA	NA	NA
	9/12/2017	Total	0.37	830	3400	6.76	2600	9700	0.29	< 0.001	0.0041	0.038			< 0.0011		< 0.00035			0.0048 J	0.0053	< 0.000085	NA	NA	NA	NA	NA
	6/26/2018	Total	0.47	690	3700	6.72	2100	8700	0.49	< 0.0010	0.0071	0.036			< 0.0011	0.003			< 0.000070	0.0042 J	< 0.00024		NA	< 0.00050	< 0.00053	0.046	0.75
	6/26/2018 10/2/2018	Dissolved Total	0.44	670 710	3400 3700	NA 6.73	2100 2200	8800 10000	0.48 0.5	< 0.0010	0.0059	0.036		< 0.00034	< 0.0011 NA	0.003 0.0030 J	< 0.00035 NA	0.0047 J 0.0038	< 0.000070 NA	0.0034 J 0.0053	< 0.00024	< 0.000085 NA	NA < -0.0397	NA NA	NA NA	NA NA	NA NA
TW-A	12/12/2017	Total	0.39	170	49	6.92	280	930	0.5	< 0.0010	0.0008 J	0.032			<0.0011			< 0.0038		0.0053 0.0014 J	0.00046	<0.000085	< -0.0397 NA	NA NA	NA NA	NA NA	NA NA
	7/10/2018	Total	0.14	110	54	6.96	79	620	0.20	< 0.001	< 0.00046	0.19	< 0.00034							< 0.00143	0.021	< 0.000085	NA	NA NA	NA NA	NA.	< 0.00061
	7/10/2018	Dissolved	0.13	110	55	NA	78	610	0.3	< 0.0010	< 0.00046		< 0.00034		< 0.0011	0.00044 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.0014	< 0.000085	NA	NA	NA	NA	NA
TW-B	12/12/2017	Total	0.59	170	300	7.07	670 F1	2300	1.2	< 0.001		0.035			<0.0011				<0.00007	0.0044 J		<0.000085	NA	NA	NA	NA	NA
	7/10/2018	Total	0.54	140	240	6.96	660	2000	1.3	< 0.001	<0.00046	0.033			< 0.0011				<0.00007	0.0028 J		<0.000085	NA	NA NA	NA NA	NA	<0.00062
TW-C	7/10/2018 12/12/2017	Dissolved	0.51 3.6	140 310	240 13000	7.54	670 1700	2000 25000	1.3	< 0.0010 0.0014 J	0.00071	0.03	< 0.00034			<0.0008 J	< 0.00035	0.0031 J	< 0.000070	0.0041 J 0.0018 J		< 0.000085	NA NA	NA NA	NA NA	NA NA	NA NA
1.44-0	7/10/2018	Total	2.3	310	6900	7.54	3100	17000	1.7	< 0.0014 3	0.0038	0.15	< 0.00034		< 0.0015 3	< 0.0004	<0.00035	0.073	<0.00007	0.0018 J		<0.000085	NA NA	NA NA	NA NA	NA NA	<0.00066
	7/10/2018	Dissolved	2.3	310	6600	NA	3000	18000	1.7	< 0.0010	0.0029		< 0.00034		< 0.0011		< 0.00035		< 0.000070	0.0076 J		< 0.000085	NA	NA	NA NA	NA	NA NA
TW-D	12/12/2017	Total	0.27	170	300	6.45	250	1400	0.35	< 0.001	0.0023	0.11	< 0.00034		< 0.0011	0.0021 J	<0.00035			0.0029 J	0.0024	<0.000085	NA	NA	NA	NA	NA
	7/11/2018	Total	0.17	74	96	6.99	110	620	0.44	< 0.001	<0.00046	0.055			< 0.0011		<0.00035			<0.00085		<0.000085	NA	NA	NA	NA	0.0022 J
	7/11/18 DUP 7/11/2018	Total Dissolved	0.2 0.22	85 82	99 100	NA NA	110 110	620 590	0.5 0.45	< 0.001 < 0.0010	<0.00046 0.00084	0.064			<0.0011 < 0.0011				<0.00007 < 0.000070	<0.00085 < 0.00085		<0.000085 < 0.000085	NA NA	NA NA	NA NA	NA NA	0.0022 J
	7/11/2016 7/11/18 DUP	Dissolved	0.22	79	99	NA	110	610	0.45	< 0.0010	0.00086				< 0.0011				< 0.000070	< 0.00085		< 0.000085	NA NA	NA NA	NA NA	NA NA	NA NA
AES-SEA	7/10/2018	Dissolved	4.2	370	20000	NA	2400	39000	0.88	<0.001	0.0032	0.008	<0.00034		<0.0011	<0.0004	<0.00035	0.18	<0.00007	0.0096 J		<0.000085	NA	NA	NA NA	NA	NA
	7/10/2018	Total	4.4	390	20000	8.4	2400	40000	0.88	<0.001	0.0024	0.008	< 0.00034	< 0.00034	<0.0011	< 0.0004	<0.00035	0.19	<0.00007	0.009 J	0.00079 J	<0.000085	NA	NA	NA	NA	NA
	Frequency of D	etection (d)	51:51	51:51	51:51	50:50	51:51	51:51	51:51	5:51	36:51	51:51	0:45	5:51	1:45	43:51	1:45	31:51	0:45	39:51	48:51	0:45	21:30	1:6	1:6	1:6	7:11

CCR - Coal Combustion Residuals.

NA - Not available/Constituent not analyzed.

mg/L - milligram per liter. MS/MSD - Matrix spike/Matrix spike duplicate.

pCi/L - picoCurie per liter. S.U. - Standard Units. TDS - Total Dissolved Solids. Qualifiers:

< - Not Detected, value is the reporting limit.

B - Analyte found in sample and associated blank.

J - Value is estimated. F1 - MS/MSD Recovery was outside acceptance limits.

(a) - The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

(a) - In e CLR Rule lists these constituents as Constituents for Detection Monitoring (Appendix IV).
 (b) - The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).
 (c) - Volatile organic compounds (VOCs) detected in one or more samples are shown.
 VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility
 (d) - Frequency of detection for groundwater (total concentrations) = Number of detected concentrations: total number of samples.

TABLE 2 **HUMAN HEALTH DRINKING WATER SCREENING LEVELS** AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

Constituent (n)	CASRN	Units	USEPA M	lCLs	USEPA SMCLs (a)	November 2 USEPA Tapwater RSLs (b)		Puerto Rico Groundwater Quality Standards (c)	Selected Federal Drinking Water Screening Level (d)	Selected Puerto Rico Drinking Water Screening Level (e, m)
Inorganics	07101111	•	(-)		(-,	- ()		0141144140 (0)	(.)	(., ,
Antimony	7440-36-0	mg/L	0.006		NA	0.0078	(j)	0.0056	0.006	0.0056
Arsenic	7440-38-2	mg/L	0.01		NA NA	0.000052	U)	0.01	0.01	0.01
Barium	7440-39-3	mg/L	2		NA NA	3.8		NA NA	2	2
Beryllium	7440-41-7	mg/L	0.004		NA NA	0.025		NA	0.004	0.004
Boron	7440-42-8	mg/L	NA		NA	4		NA	4	4
Cadmium	7440-43-9	mg/L	0.005		NA	0.0092		0.005	0.005	0.005
Calcium	7440-70-2	mg/L	NA		NA	NA		NA	NA	NA
Chloride	7647-14-5	mg/L	NA		250	NA		NA	250	250
Chromium	7440-47-3	mg/L	0.1	(f)	NA	22	(I)	0.1 (f)	0.1	0.1
Cobalt	7440-48-4	mg/L	NA	()	NA	0.006	()	NA	0.006	0.006
Fluoride	16984-48-8	mg/L	4		2	0.8		4	4	4
Lead	7439-92-1	mg/L	0.015	(g)	NA	0.015	(g)	0.015	0.015	0.015
Lithium	7439-93-2	mg/L	NA	(3)	NA	0.04	(3)	NA	0.04	0.04
Mercury	7439-97-6	mg/L	0.002	(h)	NA	0.0057	(i)	0.00005	0.002	0.00005
Molybdenum	7439-98-7	mg/L	NA	. ,	NA	0.1	.,	NA	0.1	0.1
Radium 226/228	RADIUM226228	pCi/L	5		NA	NA		NA	5	5
Selenium	7782-49-2	mg/L	0.05		NA	0.1		0.05	0.05	0.05
Sulfate	7757-82-6	mg/L	NA		250	NA		NA	250	250
Thallium	7440-28-0	mg/L	0.002	(k)	NA	0.0002	(k)	0.00024	0.002	0.00024
Total Dissolved Solids	TDS	mg/L	NA	` ,	500	NA	` '	NA	500	500
pH	PHFLD	S.U.	NA		6.5 - 8.5	NA		NA	6.5 - 8.5	6.5 - 8.5
VOCs and Sulfolane (o)										
Chlorobenzene	108-90-7	mg/L	0.1		NA	0.078		0.1	0.1	0.1
Isopropylbenzene	98-82-8	mg/L	NA		NA	0.45		NA	0.45	0.45
Methyl tert-butyl ether	1634-04-4	mg/L	NA		NA	0.014		NA	0.014	0.014
Sulfolane	126-33-0	mg/L	NA		NA	0.02		NA	0.02	0.02

Notes:

CASRN - Chemical Abstracts Service Registry Number.

MCL - Maximum Contaminant Level.

mg/L - milligram per liter.

NA - Not Available. pCi/L - picoCurie per liter. RSL - Regional Screening Levels (USEPA).

SMCL - Secondary Maximum Contaminant Level.

S.U. - Standard Units.

USEPA - United States Environmental Protection Agency.

VOC - Volatile Organic Compound.

- (a) USEPA 2018 Edition of the Drinking Water Standards and Health Advisories. Spring 2018.
- http://water.epa.gov/drink/contaminants/index.cfm
- (b) USEPA Regional Screening Levels (November 2018). Values for tapwater.

http://www.epa.gov/reg3hwmd/risk/human/rb-concentration_table/Generic_Tables/index.htm

(c) - Puerto Rico Water Quality Standards Regulation as amended on April 2016. Commonwealth of Puerto Rico Office of the Governor Environmental Quality Board. Rule 1303.1 Water Quality Standards. Class SG Groundwater. Numbers represent a total recoverable value.

Ground waters intended for use as source of drinking water supply and agricultural uses including irrigation.

Also included under this class are those ground waters that flow into coastal, surface, and estuarine waters and wetlands.

Available at: https://www.epa.gov/sites/production/files/2014-12/documents/prwqs.pdf

- (d) The hierarchy for selecting the Federal Human Health Screening Level for Drinking Water is: USEPA MCL for Drinking Water; USEPA Tapwater RSL; USEPA SMCL for Drinking Water.
- (e) The hierarchy for selecting the Puerto Rico Human Health Screening Level for Drinking Water is: Puerto Rico Groundwater Quality Standards; USEPA MCL for Drinking Water (a); USEPA Tapwater RSL; USEPA SMCL for Drinking Water.
- (f) Value for Total Chromium.
- (g) Lead Treatment Technology Action Level is 0.015 mg/L.
- (h) Value for Inorganic Mercury.
- (i) RSL for Mercuric Chloride used for Mercury.
- (j) RSL for Antimony (metallic) used for Antimony
- (k) RSL for Thallium (Soluble Salts) used for Thallium.
- (I) RSL for Chromium (III), Insoluble Salts used for Chromium.
- (m) The only differences between the Puerto Rico and Federal screening levels are the values for mercury and thallium.
- (n) The CCR Rule does not include values for boron, chloride, sulfate, pH or TDS, but these have been included here for this evaluation.

(o) - VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility

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TABLE 3 HUMAN HEALTH AND ECOLOGICAL MARINE WATER QUALITY CRITERIA AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

			Human Hea	alth Recreational			Ecological			Human Hea	Ith Recreational		Ecological	
Constituent	CASRN	Units	USEPA AWQC Consumption of Organism Only (a)	Puerto Rico Coastal and Estuarine Water Quality Standards - Human Health (b)	USEPA Ambien Water Quality Criteria for Saltwater (chronic) (c) Total		USEPA Ambient Water Quality Criteria for Saltwater (chronic) (c) Dissolved	Puerto Rico Coastal and Estuarine War Quality Standa - Aquatic (d	l ter irds	Screening	Selected Federal and Puerto Rico Human Health Recreational Screening Level (f)	Selected Federal Ecological Screening Level (g)	Selected Puerto Rico Ecological Screening Level (h)	Selected Federal and Puerto Rico Ecological Screening Level (g, i) Dissolved
Inorganics				, ,										
Antimony	7440-36-0	mg/L	0.64	0.64	NA		NA	NA		0.64	0.64	NA	NA	NA
Arsenic	7440-38-2	mg/L	0.00014	NA	0.036 (j	j)	0.036 (j)	0.036		0.00014	0.00014	0.036	0.036	0.036
Barium	7440-39-3	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Beryllium	7440-41-7	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Boron	7440-42-8	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Cadmium	7440-43-9	mg/L	NA	NA	0.0079		0.0079	0.00885		NA	NA	0.0079	0.00885	0.0079
Calcium	7440-70-2	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Chloride	7647-14-5	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Chromium	7440-47-3	mg/L	NA	NA	0.050 (k	k)	0.050 (k)	0.050	(k)	NA	NA	0.05	0.05	0.050
Cobalt	7440-48-4	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Fluoride	16984-48-8	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Lead	7439-92-1	mg/L	NA	NA	0.0081		0.0077	0.00852		NA	NA	0.0081	0.00852	0.0077
Lithium	7439-93-2	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Mercury	7439-97-6	mg/L	NA	0.000051	0.00094		0.00080	NA		NA	0.000051	0.00094	0.00094	0.00080
Molybdenum	7439-98-7	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Radium 226/228	RADIUM226228	pCi/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Selenium	7782-49-2	mg/L	4.2	NA	0.071		0.071	0.07114		4.2	4.2	0.071	0.07114	0.071
Sulfate	7757-82-6	mg/L	NA	2800 (I)	NA		NA	2800	(I)	NA	2800	NA	2800	NA
Thallium	7440-28-0	mg/L	0.00047	0.00047	NA		NA	NA		0.00047	0.00047	NA	NA	NA
Total Dissolved Solids	TDS	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
pH	PHFLD	S.U.	NA	7.3-8.5 (I)	6.5 - 8.5		NA	7.3-8.5	(l)	NA	7.3-8.5	6.5 - 8.5	7.3-8.5	NA
VOCs and Sulfolane (m)				,,,								ĺ		
Chlorobenzene	108-90-7	mg/L	0.8	1.6	NA		NA	NA		0.8	1.6	NA	NA	NA
Isopropylbenzene	98-82-8	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Methyl tert-butyl ether	1634-04-4	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA
Sulfolane	126-33-0	mg/L	NA	NA	NA		NA	NA		NA	NA	NA	NA	NA

HUMAN HEALTH AND ECOLOGICAL MARINE WATER QUALITY CRITERIA AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

Notes

AWQC - Ambient Water Quality Criteria.

CASRN - Chemical Abstracts Service Registry Number.

mg/L - milligram per liter.

NA - Not Available.

pCi/L - picoCurie per liter.

S.U. - Standard Units.

USEPA - United States Environmental Protection Agency.

VOC - Volatile Organic Compound.

(a) - USEPA National Recommended Water Quality Criteria. USEPA Office of Water and Office of Science and Technology.

http://www.epa.gov/wqc/national-recommended-water-quality-criteria-human-health-criteria-table

USEPA AWQC Human Health for the Consumption of Organism Only apply to total concentrations.

(b) - Puerto Rico Water Quality Standards Regulation as amended on April 2016.

Commonwealth of Puerto Rico Office of the Governor Environmental Quality Board.

Rule 1303.1 Water Quality Standards. Class SB and SC Coastal and Estuarine Waters. Numbers represent a total recoverable value.

Values based on protection of the water body or aquatic life for reasons of human health.

Available at: https://www.epa.gov/sites/production/files/2014-12/documents/prwqs.pdf

(c) - USEPA Ambient Water Quality Criteria for Saltwater (chronic).

https://www.epa.gov/wgc/national-recommended-water-guality-criteria-aguatic-life-criteria-table

(d) - Puerto Rico Water Quality Standards Regulation as amended on April 2016.

Commonwealth of Puerto Rico Office of the Governor Environmental Quality Board.

Rule 1303.1 Water Quality Standards. Class SB and SC Coastal and Estuarine Waters. Numbers represent a total recoverable value.

Values based on protection of the water body for the propagation and preservation of aquatic species or species dependent on the water body.

Available at: https://www.epa.gov/sites/production/files/2014-12/documents/prwqs.pdf

- (e) The Federal Human Health Recreational Screening Level for Drinking Water is: USEPA AWQC Human Health for the Consumption of Organism Only.
- (f) The hierarchy for selecting the Puerto Rico Human Health Recreational Screening Level is: Puerto Rico Coastal and Estuarine Water Quality Standards Human Health; USEPA AWQC Human Health for the Consumption of Organism Only.
- (g) The Federal Ecological Screening Level is: USEPA Ambient Water Quality Criteria for Saltwater (chronic).
- (h) The hierarchy for selecting the Puerto Rico Ecological Screening Level is: Puerto Rico Coastal and Estuarine Water Quality Standards Aquatic; USEPA Ambient Water Quality Criteria for Saltwater (chronic).
- (i) Puerto Rico Coastal and Estuarine Water Quality Standards Aquatic apply to total concentrations, therefore the USEPA Ambient Water Quality Criteria for Saltwater (chronic) dissolved screening levels are used.
- (i) Value for total arsenic.
- (k) Value for chromium (VI).
- (I) Standards for Class SB Coastal and Estuarine Waters.
- (m) VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility

COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO SELECTED HUMAN HEALTH DRINKING WATER SCREENING LEVELS - TOTAL (UNFILTERED)
AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

				Appendix	III (b)			Appendix III and IV (b, c)							Appen	dix IV (c)								Sulfolane and V	OCs (d)	
								(2, 5)														Radium			Methyl tert-	
	Constituent	Boron	Calcium	Chloride	Hq	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Bervllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury (e)	Molvbdenum	Selenium	Thallium (e)	226/228	Chlorobenzene	Isopropylbenzene	butyl ether	Sulfolane
	Puerto Rico								- 1																	
	HH DW SL (a)	4	NA	250	6.5-8.5	250	500	4	0.0056	0.01	2	0.004	0.005	0.1	0.006	0.015	0.04	0.00005	0.1	0.05	0.00024	5	0.1	0.45	0.014	0.02
Well ID	Sampling Event Date	mg/L	mg/L	mg/L	S.U.	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	pCi/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 -	8/8/2017	0.26	140	240	6.87	340	1100	0.47	< 0.001	< 0.00046			< 0.00034	< 0.0011		< 0.00035			0.0022 J	0.0073	< 0.000085	< 0.0899	NA NA	NA.	NA	NA.
Background	8/15/2017	0.26	150	260	7.07	410	1400	0.53	< 0.001	0.00055 J			< 0.00034	< 0.0011		< 0.00035		< 0.00007	< 0.0022 3	0.0073	< 0.000085	0.205	NA NA	NA NA	NA.	NA NA
Well	8/22/2017	0.25	150	220	6.74	400	1400	0.55	< 0.001	< 0.000333			< 0.00034	< 0.0011		< 0.00035			0.00033 0.0023 J	0.0065	< 0.000085	0.203	NA NA	NA NA	NA NA	NA NA
wen	8/29/2017	0.25 B	160	240	6.92	390	1400	0.55 0.58 B	< 0.001	< 0.00046			< 0.00034	< 0.0011				< 0.00007	< 0.0023 3	0.0057	< 0.000085	0.270	NA NA	NA NA	NA NA	NA NA
	9/12/2017	0.25 B	160	220	6.9	410	1400	0.56 B 0.47	< 0.001	0.00046 0.00046 J			< 0.00034			< 0.00035			0.00065 0.0018 J	0.0057	< 0.000085	NA	NA NA	NA NA	NA NA	NA NA
	6/25/2018	0.25	130	260 F1	7.13 7.33	510 F1 400	1500	0.61	< 0.0010	< 0.00046 < 0.00046			< 0.00034	< 0.0011		0.00077 J		< 0.000070	< 0.00085	0.025	< 0.000085	NA 0.405	< 0.00050	< 0.00053	< 0.00074	< 0.00058
AES MW-2 -	10/1/2018	0.24	120	200			1300	0.69	< 0.0010		0.032	NA 0.00004	< 0.00034	NA 0.0044	0.00050 J		< 0.0011	NA 0.00007	< 0.00085	0.015	NA	0.495	NA NA	NA NA	NA	NA
	8/8/2017	0.16	88	37	6.53	7.7	460 470	0.36	< 0.001	< 0.00046			< 0.00034	< 0.0011		< 0.00035			< 0.00085		< 0.000085	< 0.129	NA NA	NA NA	NA	NA
Background	8/15/2017	0.17	88	37	6.83	7.1		0.4	< 0.001	0.00047 J			< 0.00034	< 0.0011		< 0.00035			< 0.00085		< 0.000085	0.545			NA	NA
Well	8/22/2017	0.16	89	37	6.54	10	450	0.4	< 0.001	< 0.00046			< 0.00034	< 0.0011		< 0.00035			0.0010 J		< 0.000085	< 0.0379	NA NA	NA NA	NA	NA
	8/29/2017	0.17 B	100	37	6.68	16	470	0.42 B	< 0.001	< 0.00046			< 0.00034					< 0.00007	< 0.00085		< 0.000085	0.113	NA	NA	NA	NA
	9/12/2017	0.17	94	36	6.65	9.8	480	0.35	< 0.001	< 0.00046			< 0.00034	< 0.0011		< 0.00035			0.00094 J		< 0.000085	NA	NA	NA	NA	NA
	6/25/2018	0.16	110	140	6.84	43	740	0.52	< 0.0010	< 0.00046			< 0.00034					< 0.000070	< 0.00085		< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0069 J
	10/1/2018	0.16	110	85	7.04	15	690	0.67	< 0.0010	< 0.00046	0.13	NA	< 0.00034	NA	0.00058 J	NA	0.0014 J	NA	< 0.00085	< 0.00024		< 0.321	NA	NA	NA	NA
AES MW-3	8/8/2017	0.78	290	2900	6.74	630	6000	2	< 0.001	0.0038			< 0.00034	< 0.0011		< 0.00035		< 0.00007	0.096	0.052	< 0.000085	0.099	NA	NA	NA	NA
	8/15/2017	0.85	320	3400	7.1	1300	7600	2.1	< 0.001	0.0034			< 0.00034	< 0.0011		< 0.00035		< 0.00007	0.16	0.098	< 0.000085	0.142	NA	NA	NA	NA
	8/22/2017	0.83	340	3600	6.78	1500	8600	2.2	< 0.001	0.0021			< 0.00034			< 0.00035		< 0.00007	0.2	0.13	< 0.000085	0.212	NA	NA	NA	NA
	8/29/2017	0.90 B	390	3700	7.01	1700	8300	2.3 B	< 0.001	0.0024			< 0.00034			< 0.00035		< 0.00007	0.22	0.14	< 0.000085	0.0888	NA	NA	NA	NA
	9/12/2017	0.9	370	3900	7.03	2300	9900	1.9	0.0012 J	0.0029			< 0.00034		0.0025	< 0.00035		< 0.00007	0.28	0.18	< 0.000085	NA	NA	NA	NA	NA
	6/25/2018	1.2	330	4400	7.23	2800	11000	1.6	< 0.0010	0.0018	0.24	< 0.00034	0.00042 J	< 0.0011	0.0031	< 0.00035	0.0073	< 0.000070	0.22	0.21	< 0.000085	NA	0.0027	0.00053 J	< 0.00074	0.004 J
	10/1/2018	1.0	330	4700	7.43	3300	13000	1.6	< 0.0010	0.0024	0.19	NA	< 0.00034	NA	0.0031	NA	0.021	NA	0.22	0.23	NA	0.511	NA	NA	NA	NA
AES MW-4	8/8/2017	3.4	590	9800	6.91	15000	41000	0.63	< 0.001	0.0036	0.057	< 0.00034	0.00036 J	< 0.0011	0.0018 J	< 0.00035	1	< 0.00007	0.44	0.011	< 0.000085	0.527	NA	NA	NA	NA
	8/8/2017 Dup	3.4	620	9900	6.91	15000	41000	0.61	0.0014 J	0.0031	0.057	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	1	< 0.00007	0.45	0.011	< 0.000085	0.137	NA	NA	NA	NA
	8/16/2017	3.7	620	11000	7.08	16000	43000	0.63	< 0.001	0.0037	0.06	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	1.1	< 0.00007	0.4	0.0048	< 0.000085	0.112	NA	NA	NA	NA
	8/16/2017 Dup	4.1	630	10000	7.08	16000	43000	0.61	< 0.001	0.0033	0.06	< 0.00034	< 0.00034	< 0.0011	0.0016 J	< 0.00035	1.1	< 0.00007	0.38	0.0061	< 0.000085	0.507	NA	NA	NA	NA
	8/23/2017	3.8	620	9800	7.09	15000	42000	0.65	< 0.001	0.0026	0.057	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.88	< 0.00007	0.44	0.006	< 0.000085	< 0.0545	NA	NA	NA	NA
	8/23/2017 Dup	3.7	590	9900	7.09	15000	42000	0.65	< 0.001	0.0025	0.058	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	1.1	< 0.00007	0.38	0.0065	< 0.000085	0.0942	NA	NA	NA	NA
	8/30/2017	3.6 B	670	11000	7.14	16000	42000	0.68	< 0.001	0.0027	0.055	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.9	< 0.00007	0.4	0.0058	< 0.000085	0.403	NA	NA	NA	NA
	8/30/2017 Dup	3.6 B	670	11000	7.14	16000	41000	0.68	< 0.001	0.0024	0.054	< 0.00034	< 0.00034	< 0.0011	0.0016 J	< 0.00035	0.98	< 0.00007	0.42	0.0054	< 0.000085	< 0.146	NA	NA	NA	NA
	9/12/2017	3.2	600	10000	7.12	17000	42000	0.53	< 0.001	0.0035	0.056	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.75	< 0.00007	0.41	0.013	< 0.000085	NA	NA	NA	NA	NA
	9/12/2017 Dup	3.4	610	10000	7.12	17000	43000	0.63	< 0.001	0.0038	0.056	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.86	< 0.00007	0.42	0.014	< 0.000085	NA	NA	NA	NA	NA
	6/26/2018	3.2	460	9100	7.27	12000	16000	0.76	0.0023 J	0.0024	0.044	< 0.00034	0.00034 J	< 0.0011	0.0016 J	< 0.00035	0.54	< 0.000070	0.55	0.0064	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0053 J
	6/26/2018 Dup	3.2	440	8900	7.27	12000	17000	0.76	0.0019 J	0.0021	0.046	< 0.00034	< 0.00034	< 0.0011	0.0016 J	< 0.00035	0.57	< 0.000070	0.58	0.0055	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0046 J
	10/2/2018	2.6	280	5600	7.41	6000	21000	1.0	< 0.0010	0.0031	0.035	NA	0.00057 J	NA	0.0016 J	NA	0.38	NA	0.74	0.0043	NA	< 0.0708	NA	NA	NA	NA
	10/2/2018 Dup	2.6	250	5300	7.41	6200	22000	1.0	< 0.0010	0.0027	0.036	NA	0.00051 J	NA	0.0016 J	NA	0.34	NA	0.76	0.0048	NA	< 0.168	NA	NA	NA	NA
AES MW-5	8/9/2017	0.37	850	3800	6.52	2500	8200	0.42	< 0.001	0.0032	0.041	< 0.00034	< 0.00034	< 0.0011	0.0034	< 0.00035	< 0.0032	< 0.00007	0.0022 J	0.01	< 0.000085	0.473	NA	NA	NA	NA
	8/16/2017	0.46	890	3800	6.61	2700	7900	0.45	< 0.001	0.0024	0.043	< 0.00034	< 0.00034	< 0.0011	0.0035	< 0.00035	0.0047	< 0.00007	0.0086 J	0.013	< 0.000085	0.576	NA	NA	NA	NA
	8/22/2017	0.39	800	3700	6.49	2500	11000	0.46	< 0.001	0.0018			< 0.00034	< 0.0011	0.0036	< 0.00035		< 0.00007	0.0080 J	0.014	< 0.000085	0.102	NA	NA	NA	NA
	8/29/2017	0.39 B	930	3700	6.79	2600	9800	0.48	< 0.001	0.0021			< 0.00034		0.0033	< 0.00035		< 0.00007	0.0057 J	0.0099	< 0.000085	0.601	NA	NA	NA	NA
	9/12/2017	0.37	830	3400	6.76	2600	9700	0.29	< 0.001	0.0041			< 0.00034	< 0.0011	0.0033		< 0.0032	< 0.00007	0.0048 J	0.0053	< 0.000085	NA	NA	NA	NA	NA
	6/26/2018	0.47	690	3700	6.72	2100	8700	0.49	< 0.0010	0.0071			< 0.00034		0.003			< 0.000070	0.0042 J		< 0.000085	NA	< 0.00050	< 0.00053	0.046	0.75
	10/2/2018	0.39	710	3700	6.73	2200	10000	0.5	< 0.0010	0.0088	0.032	NA	< 0.00034	NA	0.0030 J	NA	0.0038	NA NA	0.0053	0.00046	NA NA	< -0.0397	NA NA	NA	NA	NA
TW-A	12/12/2017	0.14	170	49	6.92	280	930	0.26	< 0.0010	0.0008 J	0.26	<0.00034		<0.0011		<0.00035		<0.00007	0.0014 J	0.00040	<0.000085	NA	NA NA	NA NA	NA	NA
	7/10/2018	0.14	110	54	6.96	79	620	0.3	< 0.001	< 0.00046		< 0.00034		< 0.0011	0.000713			< 0.00007	< 0.00085	0.0015	<0.000085	NA	NA.	NA.	NA.	<0.00061
TW-B	12/12/2017	0.59	170	300	7.07	670 F1	2300	1.2	< 0.001	0.00069 J			< 0.00034	<0.0011		< 0.00035			0.0044 J	0.0004 J		NA	NA NA	NA NA	NA	NA
5	7/10/2018	0.54	140	240	6.96	660	2000	1.3	< 0.001	< 0.00046	0.033	< 0.00034		<0.0011	0.0012 J	< 0.00035		<0.00007	0.0028 J		<0.000085	NA	NA.	NA.	NA.	<0.00062
TW-C	12/12/2017	3.6	310	13000	7.54	1700	25000	1.1	0.0014 J	0.0038	0.033	< 0.00034		0.0015 J		< 0.00035		<0.00007	0.0028 J		<0.000085	NA NA	NA NA	NA NA	NA NA	NA
100-0	7/10/2018	2.3	310	6900	7.18	3100	17000	1.7	< 0.001	0.0038	0.13	< 0.00034		< 0.0013 3	< 0.0004	< 0.00035		<0.00007	0.0018 J		<0.000085	NA.	NA NA	NA NA	NA NA	<0.00066
TW-D	12/12/2017	0.27	170	300	6.45	250	1400	0.35	< 0.001	0.0023		< 0.00034		<0.0011	0.0021 J	< 0.00035		<0.00007	0.0001 J	0.0004	<0.000085	NA NA	NA NA	NA NA	NA NA	NA
144-0	7/11/2018	0.27	74	96	6.99	110	620	0.33	< 0.001	< 0.0023	0.055	< 0.00034	< 0.00034	<0.0011	0.00213 0.0014 J	< 0.00035		<0.00007	< 0.00293		<0.000085	NA.	NA NA	NA NA	NA NA	0.0022 J
	7/11/18 DUP	0.17	85	99	NA	110	620	0.5	< 0.001	<0.00046			< 0.00034		0.0014 J				<0.00085		<0.000085	NA.	NA NA	NA NA	NA NA	0.0022 J
	.,,.0001	0.2	30	- 33	.4/1	.10	320	0.0	3 0.001	-0.00040	0.004	40.0000 1	-0.0000 1	40.0011	0.00170	-0.00000		-0.00007	10.00000	0.00040	10.000000	14/1			1 .4/5	0.00220

DW - Drinking Water. CCR - Coal Combustion Residuals. MCL - Maximum Contaminant Level.

pCi/L - picoCurie per liter. RSL - Regional Screening Level. HH - Human Health. SL - Screening Level. SMCL - Secondary Maximum Contaminant Level.

mg/L - milligram per liter. S.U. - Standard Units. MS/MSD - Matrix spike/Matrix spike duplicate. TDS - Total Dissolved Solids.

(a) - Puerto Rico Human Health Drinking Water Screening Levels selected in Table 2 using the following hierarchy:

Puerto Rico Groundwater Quality Standards. Federal USEPA MCL for Drinking Water.

Federal USEPA Tapwater RSL, November 2018. Federal USEPA SMCL for Drinking Water.

(b) - The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

- (c) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

(d) - Volatile organic compounds (VOCs) detected in one or more samples are shown.

VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility

(e) - The selected Federal Human Health Drinking Water Screening Level for both mercury and thallium is 0.002 mg/L, as shown on Table 2. All results for mercury and thallium are also below the selected Federal Human Health Drinking Water Screening Level.

greater than the Selected Puerto Rico Human Health Drinking Water Screening Level.

Qualifiers:

< - Not Detected, value is the reporting limit. J - Value is estimated.
F1 - MS/MSD Recovery was outside acceptance limits.
B - Analyte found in sample and associated blank.

TABLE 5 COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO HUMAN HEALTH DRINKING WATER SCREENING LEVELS - DISSOLVED (FILTERED) AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

				Appendix III (b))		Appendix III and IV (b, c)							Appendix IV (c)					
	Constituent	Boron	Calcium	Chloride	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury (d)	Molybdenum	Selenium	Thallium (d)
	Puerto Rico																			
	HH DW SL (a)	4	NA	250	250	500	4	0.0056	0.01	2	0.004	0.005	0.1	0.006	0.015	0.04	0.00005	0.1	0.05	0.00024
Well ID	Sampling Event Date	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 -																				
Background Well	6/25/2018	0.28	130	260 F1	490 F1	1600	0.61	< 0.0010	< 0.00046	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.025	< 0.000085
AES MW-2 -																				
Background Well	6/25/2018	0.17	110	130	44	730	0.5	< 0.0010	< 0.00046	0.15	< 0.00034	< 0.00034	< 0.0011	0.00067 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.00030 J	< 0.000085
AES MW-3	6/25/2018	1.1	320	4300	2500	10000	1.7	< 0.0010	0.0016	0.26	< 0.00034	0.00034 J	< 0.0011	0.0034 J	< 0.00035	0.0064	< 0.000070	0.2	0.2	< 0.000085
AES MW-4	6/26/2018	3.4	450	9100	11000	13000	0.76	< 0.0010	0.0024	0.045	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.56	< 0.000070	0.58	0.005	< 0.000085
	6/26/2018 Dup	3.5	450	8700	11000	14000	0.74	< 0.0010	0.0022	0.046	< 0.00034	0.00035 J	< 0.0011	0.0016 J	< 0.00035	0.59	< 0.000070	0.6	0.0054	< 0.000085
AES MW-5	6/26/2018	0.44	670	3400	2100	8800	0.48	< 0.0010	0.0059	0.036	< 0.00034	< 0.00034	< 0.0011	0.003	< 0.00035	0.0047 J	< 0.000070	0.0034 J	< 0.00024	< 0.000085
TW-A	7/10/2018	0.13	110	55	78	610	0.28	< 0.0010	< 0.00046	0.18	< 0.00034	< 0.00034	< 0.0011	0.00044 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.0014	< 0.000085
TW-B	7/10/2018	0.51	140	240	670	2000	1.3	< 0.0010	0.00071 J	0.03	< 0.00034	< 0.00034	< 0.0011	0.00082 J	< 0.00035	0.0031 J	< 0.000070	0.0041 J	0.00033 J	< 0.000085
TW-C	7/10/2018	2.3	310	6600	3000	18000	1.7	< 0.0010	0.0029	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	0.014	< 0.000070	0.0076 J	0.00026 J	< 0.000085
TW-D	7/11/2018	0.22	82	100	110	590	0.45	< 0.0010	0.00084 J	0.063	< 0.00034	< 0.00034	< 0.0011	0.00092 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085
	7/11/18 DUP	0.21	79	99	110	610	0.47	< 0.0010	0.00086 J	0.061	< 0.00034	< 0.00034	< 0.0011	0.00093 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085

DW - Drinking Water. CCR - Coal Combustion Residuals. HH - Human Health. MCL - Maximum Contaminant Level.

mg/L - milligram per liter.

NA - Not Available. RSL - Risk-Based Screening Level. SL - Screening Level.

SMCL - Secondary Maximum Contaminant Level.

TDS - Total Dissolved Solids.

MS/MSD - Matrix spike/Matrix spike duplicate. USEPA - United States Environmental Protection Agency.

(a) - Puerto Rico Human Health Drinking Water Screening Levels selected in Table 2 using the following hierarchy: Puerto Rico Groundwater Quality Standards.

Federal USEPA MCL for Drinking Water. Federal USEPA Tapwater RSL, November 2018. Federal USEPA SMCL for Drinking Water.

- Pederial OSEPA SWCL tol Unlinking Water.

 (b) -The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

 (c) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

 (d) The selected Federal Human Health Drinking Water Screening Level for both mercury and thallium is 0.002 mg/L, as shown on Table 2.

 All results for mercury and thallium are also below the selected Federal Human Health Drinking Water Screening Level.

greater than the Selected Puerto Rico Human Health Drinking Water Screening Level.

- Qualifiers:
 < Not Detected, value is the reporting limit.
 B Analyte found in sample and associated blank.
- F1 MS/MSD Recovery was outside acceptance limits.
- J Value is estimated.

TABLE 6
COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO SELECTED HUMAN HEALTH RECREATIONAL SCREENING LEVELS - TOTAL (UNFILTERED)
AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

Well ID Sampling	Constituent I and Puerto Rico HH Rec St. (a) ng Event Date 88/2017 7/55/2017 7/25/2017 7/25/2018 0/1/2018 88/2017 1/2017 7/25/2018 1/2017 1/202017 1/202017 1/202017 1/202017 1/202017 1/202017 1/202017 1/202017 1/202017	NA mg/L 0.26 0.25 0.25 B 0.26 0.25 0.25 0.24 0.16 0.17 B 0.17 B 0.17 C.16	NA mg/L 140 150 160 160	NA mg/L 240 260 220 240 220 260 F1 200 37 37	pH 7.3 - 8.5 S.U. 6.87 7.07 6.74 6.92 6.9 7.13 7.33		TDS NA mg/L 1100 1400 1400 1400 1400	Appendix III and IV (b, c) Fluoride NA mg/L 0.47 0.53 0.55 0.58 B	0.64 mg/L < 0.001 < 0.001	Arsenic 0.00014 mg/L < 0.00046 0.00055 J	NA mg/L 0.05	NA mg/L < 0.00034	NA mg/L	Chromium NA mg/L	Cobalt	Lead		Mercury	Molybdenum	Selenium	Thallium	Radium 226/228	Chlorobenzene	Sulfolane and V	Methyl tert-	Sulfolane
Well ID Sampling	l and Puerto Rico HH Rec SL (a) ng Event Date 3/8/2017 1/5/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017	NA mg/L 0.26 0.25 0.25 B 0.26 0.25 0.24 0.16 0.17 0.17 B	NA mg/L 140 150 150 160 160 130 120 88 88 89	NA mg/L 240 260 220 240 220 260 F1 200 37	7.3 - 8.5 S.U. 6.87 7.07 6.74 6.92 6.9 7.13 7.33	2800 mg/L 340 410 400 390 410	NA mg/L 1100 1400 1400 1400 1400	NA mg/L 0.47 0.53 0.55	0.64 mg/L < 0.001 < 0.001	0.00014 mg/L < 0.00046	NA mg/L 0.05	NA mg/L	NA mg/L	NA	NA		Lithium	Mercury	Molybdenum	Selenium	Thallium		Chlorobenzene	Isopropylbenzen		Sulfolane
Well ID Sampling	l and Puerto Rico HH Rec SL (a) ng Event Date 3/8/2017 1/5/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017 1/2/2017	NA mg/L 0.26 0.25 0.25 B 0.26 0.25 0.24 0.16 0.17 0.17 B	NA mg/L 140 150 150 160 160 130 120 88 88 89	NA mg/L 240 260 220 240 220 260 F1 200 37	7.3 - 8.5 S.U. 6.87 7.07 6.74 6.92 6.9 7.13 7.33	2800 mg/L 340 410 400 390 410	NA mg/L 1100 1400 1400 1400 1400	NA mg/L 0.47 0.53 0.55	0.64 mg/L < 0.001 < 0.001	0.00014 mg/L < 0.00046	NA mg/L 0.05	NA mg/L	NA mg/L	NA	NA		Lithium	Mercury	Molybdenum	Selenium	Thallium	226/228	Chlorobenzene	Isopropylbenzen	e butyl ether	Sulfolane
Well ID Sampling	HH Rec SL (a) ng Event Date 3/8/2017 7/5/2017 7/29/2017 7/29/2017 7/29/2017 7/29/2017 7/2/2017 7/2/2017 7/2/2017 7/2/2017 7/2/2017 7/2/2017 7/2/2017	mg/L 0.26 0.26 0.25 0.25 B 0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	mg/L 140 150 150 160 160 130 120 88 88 89	mg/L 240 260 220 240 220 260 F1 200 37	S.U. 6.87 7.07 6.74 6.92 6.9 7.13 7.33	mg/L 340 410 400 390 410	mg/L 1100 1400 1400 1400 1400	mg/L 0.47 0.53 0.55	mg/L < 0.001 < 0.001	mg/L < 0.00046	mg/L 0.05	mg/L	mg/L													
AES MW-1 8/8 Background Well 8/22 8/25 9/11/ AES MW-2 8/8 Background Well 8/22 10/0 AES MW-2 8/8 Background Well 8/22 8/25 11/0 AES MW-3 8/8 8/15 8/25 8/25 8/25 8/26 8/11/ AES MW-4 8/8 8/8/27 8/16/2 8/16/2 8/26 8/26 8/26 8/26 8/26 8/26 8/26 8	ng Event Date 3/8/2017 /15/2017 /15/2017 /22/2017 /29/2017 /12/2017 /12/2018 0/1/2018 3/8/2017 /15/2017 /22/2017 /22/2017 /12/2017 /12/2017 /12/2017 /12/2018 0/1/2018	mg/L 0.26 0.26 0.25 0.25 B 0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	mg/L 140 150 150 160 160 130 120 88 88 89	mg/L 240 260 220 240 220 260 F1 200 37	S.U. 6.87 7.07 6.74 6.92 6.9 7.13 7.33	mg/L 340 410 400 390 410	mg/L 1100 1400 1400 1400 1400	mg/L 0.47 0.53 0.55	mg/L < 0.001 < 0.001	mg/L < 0.00046	mg/L 0.05	mg/L	mg/L													
AES MW-1 8/8 Background Well 8/22 8/25 9/11/ AES MW-2 8/8 Background Well 8/22 10/0 AES MW-2 8/8 Background Well 8/22 8/25 11/0 AES MW-3 8/8 8/15 8/25 8/25 8/25 8/26 8/11/ AES MW-4 8/8 8/8/27 8/16/2 8/16/2 8/26 8/26 8/26 8/26 8/26 8/26 8/26 8	3/8/2017 /15/2017 /29/2017 /29/2017 /12/2017 /12/2017 /12/2018 8/6/2017 /15/2017 /22/2017 /12/2017 /12/2017 /12/2018 8/6/2017 /12/2017 /12/2018	0.26 0.26 0.25 0.25 B 0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	140 150 150 160 160 130 120 88 88 89	240 260 220 240 220 260 F1 200 37	6.87 7.07 6.74 6.92 6.9 7.13 7.33	340 410 400 390 410	1100 1400 1400 1400 1400	0.47 0.53 0.55	< 0.001 < 0.001	< 0.00046	0.05					NA	NA	0.000051	NA.	4.2	0.00047	NA - O'/	1.6	NA	NA	NA.
Background Well 8/22 AES MW-2 - 8/8 Background Well 8/22 AES MW-3 8/8 AES MW-3 8/8 AES MW-3 8/8 8/22 8/22 8/22 8/22 8/22 8/22 8/24 AES MW-4 8/8 8/8/22	/15/2017 /22/2017 /29/2017 /29/2017 /12/2017 /25/2018 0/1/2018 3/8/2017 /15/2017 /22/2017 /29/2017 /12/2017 /25/2018	0.26 0.25 B 0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	150 150 160 160 130 120 88 88 88	260 220 240 220 220 260 F1 200 37	7.07 6.74 6.92 6.9 7.13 7.33	410 400 390 410	1400 1400 1400 1400	0.53 0.55	< 0.001			< 0.00034			mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	pCi/L	mg/L	mg/L	mg/L	mg/L
Well 8/22 8/25 9/112 6/25 9/112 AES MW-2 8/8 Background 8/11 6/25 9/112 6/25 10/1 AES MW-3 8/8 8/11 8/12 8/22 8/22 8/22 8/26 9/11 AES MW-4 8/8 8/8/12 8/16/2	/22/2017 /29/2017 /12/2017 /12/2017 /25/2018 0/1/2018 3/8/2017 /15/2017 /22/2017 /12/2017 /12/2017 /25/2018	0.25 B 0.26 0.25 D.24 0.16 0.17 0.16 0.17 B 0.17	150 160 160 130 120 88 88 88	220 240 220 260 F1 200 37	6.74 6.92 6.9 7.13 7.33	400 390 410	1400 1400 1400	0.55		0.00055 J		0.00004		< 0.0011	0.00058 J	< 0.00035		< 0.00007	0.0022 J		< 0.000085	< 0.0899	NA NA	NA	NA	NA
AES MW-2 - 8/8 Background Well 8/22 8/22 8/22 8/22 8/22 8/22 8/22 8/	/29/2017 /12/2017 /25/2018 /0/1/2018 /0/1/2018 /0/1/2017 /15/2017 /22/2017 /12/2017 /12/2017 /25/2018	0.25 B 0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	160 160 130 120 88 88 88 89	240 220 260 F1 200 37	6.92 6.9 7.13 7.33	390 410	1400 1400		< 0.001	< 0.00046					0.00055 J	< 0.00035 < 0.00035		< 0.00007 < 0.00007	< 0.00085 0.0023 J		< 0.000085 < 0.000085	0.205 0.270	NA NA	NA NA	NA	NA
AES MW-2 8/8 Background 8/15 Well 8/22 9/12 AES MW-3 8/8 8/15 AES MW-3 8/8 8/15 8/22 8/25 9/11 AES MW-4 8/8 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26 8/8/26	/12/2017 /25/2018 0/1/2018 3/8/2017 /15/2017 /22/2017 /29/2017 /12/2017 /25/2018 0/1/2018	0.26 0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	160 130 120 88 88 88	220 260 F1 200 37	6.9 7.13 7.33	410	1400	U.30 D	< 0.001										< 0.0023 3		< 0.000085	0.270	NA NA	NA NA	NA NA	NA NA
AES MW-2 - 8/8, 8/25 MW-3 - 8/10/1 AES MW-3 AES MW-4 8/8/22 8/25 8/25 8/25 8/25 8/25 8/25 8/	/25/2018 0/1/2018 3/8/2017 //5/2017 //22/2017 //29/2017 //25/2017 //25/2018 0/1/2018	0.25 0.24 0.16 0.17 0.16 0.17 B 0.17	130 120 88 88 88	260 F1 200 37	7.13 7.33			0.47	< 0.001	< 0.00046		< 0.00034		< 0.0011		< 0.00035		< 0.00007	0.00085 0.0018 J		< 0.000085	NA	NA NA	NA NA	NA NA	NA NA
AES MW-2 - 8/8 Background Well 8/22 8/25 9/12 6/25 8/25 8/25 8/25 8/25 8/25 8/25 8/25 8	0/1/2018 8/8/2017 /15/2017 /22/2017 /29/2017 /12/2017 /25/2018 0/1/2018	0.24 0.16 0.17 0.16 0.17 B 0.17	120 88 88 88	200 37	7.33	31011	1500	0.47		< 0.00046		< 0.00034						< 0.000070	< 0.00085		< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	< 0.00058
AES MW-2 - 8/8 Background Well 8/22 8/25 8/25 9/12 6/22 10/0 AES MW-3 8/8 8/15 8/25 8/25 9/12 6/22 8/25 8/26 8/8/27 8/8/28 8/8/28 8/8/28 8/8/28	3/8/2017 /15/2017 /22/2017 /29/2017 /12/2017 /25/2018 0/1/2018	0.16 0.17 0.16 0.17 B 0.17	88 88 89	37		400	1300	0.69		< 0.00046		NA	< 0.00034	NA	0.00050 J	NA	< 0.0011	× 0.000070	< 0.00085	0.025	NA	0.495	NA	NA	NA	NA
Background Well 8/22 8/22 8/22 8/22 8/22 8/22 10/1 AES MW-3 8/8 8/16 8/22 8/22 8/22 8/22 8/22 8/24 8/8/24 8/8/24 8/8/24 8/8/24 8/8/24 8/8/24 8/8/24 8/8/24 8/8/24	/15/2017 /22/2017 /29/2017 /12/2017 /25/2018 0/1/2018	0.17 0.16 0.17 B 0.17	88 89		6.53	7.7	460	0.36		< 0.00046		< 0.00034		< 0.0011	< 0.0004			< 0.00007	< 0.00085		< 0.000085	< 0.129	NA NA	NA.	NA NA	NA NA
Well 8/22 8/22 9/12 6/25 10/0 AES MW-3 8/8 8/15 8/22 8/22 8/25 10/0 AES MW-4 8/8 8/8/2(2 8/16/2 8/16/2 8/16/2 8/16/2 8/16/2	/22/2017 /29/2017 /12/2017 /25/2018 0/1/2018	0.16 0.17 B 0.17	89		6.83	7.1	470	0.4	< 0.001	0.00047 J		< 0.00034		< 0.0011	< 0.0004						< 0.000085	0.545	NA NA	NA.	NA.	NA NA
AES MW-3 88.8 8/15 8/25 8/25 8/25 8/25 8/25 8/25 8/25 8/2	/29/2017 /12/2017 /25/2018 0/1/2018	0.17 B 0.17		37	6.54	10	450	0.4		< 0.00046		< 0.00034			< 0.0004						< 0.000085	< 0.0379	NA.	NA.	NA	NA.
9/12 6/25 10/12 10	/12/2017 /25/2018 0/1/2018	0.17		37	6.68	16	470	0.42 B		< 0.00046		< 0.00034			< 0.0004						< 0.000085	0.113	NA.	NA.	NA.	NA.
6/25 10/1 AES MW-3 8/8, 8/15 8/22 8/25 9/11/ 6/25 10/1 AES MW-4 8/8 8/8/20 8/16/2 8/16/2	/25/2018 0/1/2018		94	36	6.65	9.8	480	0.35	< 0.001	< 0.00046		< 0.00034			< 0.0004						< 0.000085	NA	NA	NA	NA	NA
AES MW-3 8/8. 8/16/2 8/22 8/25/2 9/12 6/25 10/1 AES MW-4 8/8. 8/8/22/8/16/2 8/16/2 8/25/8/25/8/25/8/25/8/25/8/25/8/25/8/	0/1/2018		110	140	6.84	43	740	0.52		< 0.00046		< 0.00034						< 0.000070			< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0069 J
AES MW-3 8/8 8/15 8/25 8/25 9/12 6/25 10/0 AES MW-4 8/8 8/8/2/ 8/16/2 8/26 8/26 8/27 8/26 8/27 8/26 8/26 8/26 8/26 8/26 8/26		0.16	110	85	7.04	15	690	0.67	< 0.0010	< 0.00046	0.13	NA	< 0.00034	NA	0.00058 J	NA	0.0014 J	NA	< 0.00085	< 0.00024	NA	< 0.321	NA	NA	NA	NA
8/15 8/22 8/25 9/12 6/25 10/1 AES MW-4 8/8 8/8/2(2 8/16/2 8/25 8/25 8/25 8/25 8/25 8/25 8/25 8/	3/8/2017	0.78	290	2900	6.74	630	6000	2	< 0.001	0.0038		< 0.00034			0.0018 J			< 0.00007	0.096	0.052	< 0.000085	0.099	NA	NA	NA	NA
8/25 9/12 6/25 10// AES MW-4 8/8, 8/8/25 8/16 8/16/2 8/25	/15/2017	0.85	320	3400	7.1	1300	7600	2.1	< 0.001	0.0034	0.29	< 0.00034	< 0.00034	< 0.0011	0.0019 J	< 0.00035	0.0077	< 0.00007	0.16	0.098	< 0.000085	0.142	NA	NA	NA	NA
9/12 6/25 10/1 AES MW-4 8/8 8/8/2(8/16/2 8/16/2 8/23	/22/2017	0.83	340	3600	6.78	1500	8600	2.2	< 0.001	0.0021	0.37	< 0.00034	< 0.00034	< 0.0011	0.0023 J	< 0.00035	0.0075	< 0.00007	0.2	0.13	< 0.000085	0.212	NA	NA	NA	NA
6/25 10/1 AES MW-4 8/8 8/8/20 8/16/2 8/16/2 8/23	/29/2017	0.90 B	390	3700	7.01	1700	8300	2.3 B	< 0.001	0.0024	0.25	< 0.00034	< 0.00034	< 0.0011	0.0022 J	< 0.00035	0.0075	< 0.00007	0.22	0.14	< 0.000085	0.0888	NA	NA	NA	NA
AES MW-4 8/8/8 8/8/20 8/16/2 8/16/2 8/23	/12/2017	0.9	370	3900	7.03	2300	9900	1.9	0.0012 J	0.0029	0.23	< 0.00034	< 0.00034	< 0.0011	0.0025	< 0.00035	0.0056	< 0.00007	0.28	0.18	< 0.000085	NA	NA	NA	NA	NA
AES MW-4 8/8 8/8/20 8/16/2 8/23	/25/2018	1.2	330	4400	7.23	2800	11000	1.6	< 0.0010	0.0018	0.24	< 0.00034	0.00042 J	< 0.0011	0.0031	< 0.00035	0.0073	< 0.000070	0.22	0.21	< 0.000085	NA	0.0027	0.00053 J	< 0.00074	0.004 J
8/8/20 8/16 8/16/2 8/23	0/1/2018	1.0	330	4700	7.43	3300	13000	1.6	< 0.0010	0.0024	0.19	NA	< 0.00034	NA	0.0031	NA	0.021	NA	0.22	0.23	NA	0.511	NA	NA	NA	NA
8/16/2 8/16/2 8/23	3/8/2017	3.4	590	9800	6.91	15000	41000	0.63	< 0.001	0.0036	0.057	< 0.00034	0.00036 J	< 0.0011	0.0018 J	< 0.00035	1	< 0.00007	0.44	0.011	< 0.000085	0.527	NA	NA	NA	NA
8/16/2 8/23	/2017 Dup	3.4	620	9900	6.91	15000	41000	0.61	0.0014 J	0.0031		< 0.00034			0.0017 J		1	< 0.00007	0.45		< 0.000085	0.137	NA	NA	NA	NA
8/23	/16/2017	3.7		11000	7.08	16000	43000	0.63	< 0.001	0.0037		< 0.00034			0.0017 J		1.1	< 0.00007	0.4		< 0.000085	0.112	NA	NA	NA	NA
	6/2017 Dup	4.1		10000	7.08	16000	43000	0.61	< 0.001	0.0033		< 0.00034				< 0.00035	1.1	< 0.00007	0.38		< 0.000085	0.507	NA	NA	NA	NA
	/23/2017	3.8	620	9800	7.09	15000	42000	0.65	< 0.001	0.0026		< 0.00034			0.0017 J		0.88	< 0.00007	0.44		< 0.000085	< 0.0545	NA	NA	NA	NA
	3/2017 Dup	3.7	590	9900	7.09	15000	42000	0.65	< 0.001	0.0025		< 0.00034			0.0017 J		1.1	< 0.00007	0.38		< 0.000085	0.0942	NA	NA	NA	NA
	/30/2017	3.6 B		11000	7.14	16000	42000	0.68	< 0.001	0.0027		< 0.00034			0.0017 J		0.9	< 0.00007	0.4	0.0058	< 0.000085	0.403	NA	NA	NA	NA
	0/2017 Dup	3.6 B		11000	7.14	16000	41000	0.68	< 0.001	0.0024		< 0.00034			0.0016 J		0.98	< 0.00007	0.42		< 0.000085	< 0.146	NA NA	NA NA	NA	NA
	/12/2017	3.2	600 610	10000 10000	7.12 7.12	17000	42000	0.53 0.63	< 0.001	0.0035 0.0038		< 0.00034				< 0.00035	0.75	< 0.00007	0.41	0.013	< 0.000085	NA	NA NA	NA NA	NA	NA NA
	2/2017 Dup /26/2018	3.4 3.2	460	9100	7.12	17000 12000	43000 16000	0.63	< 0.001 0.0023 J	0.0038		< 0.00034 < 0.00034			0.0017 J 0.0016 J		0.86 0.54	< 0.00007 < 0.000070	0.42 0.55	0.014 0.0064	< 0.000085 < 0.000085	NA NA	NA < 0.00050	NA < 0.00053	NA < 0.00074	NA 0.0053 J
	6/2018 Dup	3.2	440	8900	7.27	12000	17000	0.76	0.0023 J 0.0019 J	0.0024		< 0.00034			0.0016 J			< 0.000070	0.55	0.0055	< 0.000085	NA NA	< 0.00050	< 0.00053	< 0.00074	0.0053 J 0.0046 J
	0/2/2018 Dup	2.6	280	5600	7.41	6000	21000	1.0	< 0.0019 3	0.0021	0.046		0.00057 J	NA	0.0016 J	NA	0.38	NA	0.74	0.0033	NA	< 0.0708	NA	NA	NA	NA
	2/2018 Dup	2.6	250	5300	7.41	6200	22000	1.0	< 0.0010	0.0031	0.035	NA	0.00057 J	NA.	0.0016 J	NA	0.34	NA	0.74	0.0043	NA NA	< 0.168	NA NA	NA NA	NA NA	NA NA
	3/9/2017	0.37	850	3800	6.52	2500	8200	0.42	< 0.001	0.0027		< 0.00034		< 0.0011	0.0034	< 0.00035		< 0.00007	0.0022 J	0.0040	< 0.000085	0.473	NA NA	NA.	NA NA	NA NA
	/16/2017	0.46	890	3800	6.61	2700	7900	0.45	< 0.001	0.0024		< 0.00034		< 0.0011	0.0035	< 0.00035		< 0.00007	0.002E J		< 0.000085	0.576	NA.	NA.	NA	NA
	/22/2017	0.39	800	3700	6.49	2500	11000	0.46	< 0.001	0.0018		< 0.00034		< 0.0011	0.0036	< 0.00035		< 0.00007	0.0080 J		< 0.000085	0.102	NA	NA	NA	NA
	/29/2017	0.39 B	930	3700	6.79	2600	9800	0.48	< 0.001	0.0021		< 0.00034		< 0.0011	0.0033	< 0.00035		< 0.00007	0.0057 J		< 0.000085	0.601	NA	NA	NA	NA
	/12/2017	0.37	830	3400	6.76	2600	9700	0.29	< 0.001	0.0041		< 0.00034		< 0.0011	0.0033	< 0.00035		< 0.00007	0.0048 J		< 0.000085	NA	NA	NA	NA	NA
	/26/2018	0.47	690	3700	6.72	2100	8700	0.49	< 0.0010	0.0071		< 0.00034			0.003			< 0.000070	0.0042 J		< 0.000085	NA	< 0.00050	< 0.00053	0.046	0.75
	0/2/2018	0.39	710	3700	6.73	2200	10000	0.5	< 0.0010	0.0088	0.032		< 0.00034	NA	0.0030 J	NA	0.0038	NA	0.0053	0.00046	NA	< -0.0397	NA	NA	NA	NA
	2/12/2017	0.14	170	49	6.92	280	930	0.26	< 0.001	0.0008 J	0.26		< 0.00034	< 0.0011	0.00071 J		< 0.0011	<0.00007	0.0014 J	0.021	<0.000085	NA	NA	NA	NA	NA
	/10/2018	0.14	110	54	6.96	79	620	0.3	< 0.001	<0.00046	0.19		< 0.00034	< 0.0011	0.00098 J	< 0.00035		< 0.00007	< 0.00085	0.0015	< 0.000085	NA	NA	NA	NA	< 0.00061
TW-B 12/1:	2/12/2017	0.59	170	300	7.07	670 F1	2300	1.2	< 0.001	0.00069 J	0.035	< 0.00034	< 0.00034	< 0.0011	0.0012 J	< 0.00035	0.0035 J	<0.00007	0.0044 J	0.0004 J	<0.000085	NA	NA	NA	NA	NA
		0.54	140	240	6.96	660	2000	1.3	< 0.001	<0.00046	0.033	< 0.00034	< 0.00034	< 0.0011	0.0012 J	< 0.00035	0.0033 J	<0.00007	0.0028 J	0.00081 J	<0.000085	NA	NA	NA	NA	< 0.00062
	/10/2018	3.6	310	13000	7.54	1700	25000	1.1	0.0014 J	0.0038	0.15		<0.00034	0.0015 J	<0.0004	<0.00035	0.073	<0.00007	0.0018 J		<0.000085	NA	NA	NA	NA	NA
	2/12/2017	2.3	310	6900	7.18	3100	17000	1.7	< 0.001	0.0023		<0.00034		<0.0011	<0.0004	<0.00035	0.014	<0.00007			<0.000085	NA	NA	NA	NA	< 0.00066
	2/12/2017 /10/2018	0.27	170	300	6.45	250	1400	0.35	< 0.001	0.0023	0.11		< 0.00034	< 0.0011	0.0021 J	< 0.00035	< 0.0011	<0.00007	0.0029 J	0.0024	<0.000085	NA	NA	NA	NA	NA
	2/12/2017 /10/2018 2/12/2017		74	96	6.99	110	620	0.44	< 0.001	< 0.00046	0.055	< 0.00034	< 0.00034	< 0.0011	0.0014 J	< 0.00035	< 0.0011	< 0.00007	< 0.00085	0.00027 J	< 0.000085	NA	NA	NA	NA	0.0022 J
7/11/	2/12/2017 /10/2018 2/12/2017 /11/2018	0.17	85	99	NA	110	620	0.5	< 0.001	< 0.00046		< 0.00034		< 0.0011	0.0014 J	< 0.00035		< 0.00007	< 0.00085	0.0004 J	< 0.000085	NA	NA	NA	NA	0.0022 J

CCR - Coal Combustion Residuals.

Rec - Recreational. HH - Human Health. RSL - Regional Screening Level. mg/L - milligram per liter. MS/MSD - Matrix spike/Matrix spike duplicate. SL - Screening Level. S.U. - Standard Units.

NA - Not available/Constituent not analyzed. TDS - Total Dissolved Solids.

pCi/L - picoCurie per liter. USEPA - United States Environmental Protection Agency. Qualifiers:

- < Not Detected, value is the reporting limit.
- J Value is estimated.
 F1 MS/MSD Recovery was outside acceptance limits.
 B Analyte found in sample and associated blank.

(a) - Puerto Rico Human Health Recreational Screening Levels selected in Table 3 as: Puerto Rico Coastal and Estuarine Water Quality Standards - Human Health.

USEPA National Recommended Water Quality Criteria - Human Health for the Consumption of Organism Only. Applies to total concentrations.

- (b) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

 (c) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

 (d) Volatile organic compounds (VOCs) detected in one or more samples are shown.

greater than the Selected Federal and Puerto Rico Human Health Recreational Screening Level.

TABLE 7 COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO HUMAN HEALTH RECREATIONAL SCREENING LEVELS - DISSOLVED (FILTERED) AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

				Appendix III (b)		Appendix III and IV (b, c)							Appendix IV (c)					
	Constituent	Boron	Calcium	Chloride	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury	Molybdenum	Selenium	Thallium
	Federal and Puerto Rico HH																			
	Rec SL (a)	NA	NA	NA	2800	NA	NA	0.64	0.00014	NA	NA	NA	NA	NA	NA	NA	0.000051	NA	4.2	0.00047
Well ID	Sampling Event Date	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 -																				
Background Well	6/25/2018	0.28	130	260 F1	490 F1	1600	0.61	< 0.0010	< 0.00046	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.025	< 0.000085
AES MW-2 -																				
Background Well	6/25/2018	0.17	110	130	44	730	0.5	< 0.0010	< 0.00046	0.15	< 0.00034	< 0.00034	< 0.0011	0.00067 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.00030 J	< 0.000085
AES MW-3	6/25/2018	1.1	320	4300	2500	10000	1.7	< 0.0010	0.0016	0.26	< 0.00034	0.00034 J	< 0.0011	0.0034 J	< 0.00035	0.0064	< 0.000070	0.2	0.2	< 0.000085
AES MW-4	6/26/2018	3.4	450	9100	11000	13000	0.76	< 0.0010	0.0024	0.045	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.56	< 0.000070	0.58	0.005	< 0.000085
	6/26/2018 Dup	3.5	450	8700	11000	14000	0.74	< 0.0010	0.0022	0.046	< 0.00034	0.00035 J	< 0.0011	0.0016 J	< 0.00035	0.59	< 0.000070	0.6	0.0054	< 0.000085
AES MW-5	6/26/2018	0.44	670	3400	2100	8800	0.48	< 0.0010	0.0059	0.036	< 0.00034	< 0.00034	< 0.0011	0.003	< 0.00035	0.0047 J	< 0.000070	0.0034 J	< 0.00024	< 0.000085
TW-A	7/10/2018	0.13	110	55	78	610	0.28	< 0.0010	< 0.00046	0.18	< 0.00034	< 0.00034	< 0.0011	0.00044 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.0014	< 0.000085
TW-B	7/10/2018	0.51	140	240	670	2000	1.3	< 0.0010	0.00071 J	0.03	< 0.00034	< 0.00034	< 0.0011	0.00082 J	< 0.00035	0.0031 J	< 0.000070	0.0041 J	0.00033 J	< 0.000085
TW-C	7/10/2018	2.3	310	6600	3000	18000	1.7	< 0.0010	0.0029	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	0.014	< 0.000070	0.0076 J	0.00026 J	< 0.000085
TW-D	7/11/2018	0.22	82	100	110	590	0.45	< 0.0010	0.00084 J	0.063	< 0.00034	< 0.00034	< 0.0011	0.00092 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085
	7/11/18 DUP	0.21	79	99	110	610	0.47	< 0.0010	0.00086 J	0.061	< 0.00034	< 0.00034	< 0.0011	0.00093 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085

NA - Not Available.

CCR - Coal Combustion Residuals. HH - Human Health. mg/L - milligram per liter. MS/MSD - Matrix spike/Matrix spike duplicate.

Rec - Recreational. RSL - Risk-Based Screening Level. SL - Screening Level.

TDS - Total Dissolved Solids.

USEPA - United States Environmental Protection Agency.

- Qualifiers:
 < Not Detected, value is the reporting limit.
 B Analyte found in sample and associated blank.
- F1 MS/MSD Recovery was outside acceptance limits.
- J Value is estimated.

(a) - Puerto Rico Human Health Recreational Screening Levels selected in Table 3 as:
 Puerto Rico Coastal and Estuarine Water Quality Standards - Human Health.
 USEPA National Recommended Water Quality Criteria - Human Health for the Consumption of Organism Only. Applies to total concentrations.
 (b) - The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).
 (c) - The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

greater than the Selected Federal and Puerto Rico Human Health Recreational Screening Level.

TABLE 8 COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO ECOLOGICAL SCREENING LEVELS - TOTAL (UNFILTERED) AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

				Append	lix III (b)			Appendix III and IV (b, c)							Ap	pendix IV (c)								Sulfolane and V	OCs (d)	
																						Radium			Methyl tert-	
	Constituent	Boron		Chloride		Sulfate	TDS	Fluoride	Antimony						Cobalt	Lead	Lithium		Molybdenum			226/228	Chlorobenzene	Isopropylbenzene		Sulfolane
	Eco SL (a)	NA	NA		7.3 - 8.5		NA	NA	NA	0.036	NA	NA	0.00885	0.05	NA	0.00852	NA	0.00094	NA	0.07114	NA	NA	NA .	NA	NA	NA
Well ID	Sampling Event Date	mg/L	mg/L	mg/L	S.U.	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	pCi/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 - Background	8/8/2017	0.26	140	240	6.87	340	1100	0.47	< 0.001	< 0.00046	0.05		< 0.00034	< 0.0011	0.00058 J	< 0.00035		< 0.00007	0.0022 J	0.0073	< 0.000085	< 0.0899	NA	NA	NA	NA
Well	8/15/2017	0.26	150	260	7.07	410 400	1400 1400	0.53		0.00055 J	0.056		< 0.00034	< 0.0011		< 0.00035		< 0.00007	< 0.00085	0.0062	< 0.000085	0.205	NA	NA	NA	NA
vveii	8/22/2017 8/29/2017	0.25	150	220	6.74			0.55	< 0.001	< 0.00046			< 0.00034	< 0.0011		< 0.00035		< 0.00007	0.0023 J	0.0065	< 0.000085	0.270	NA	NA	NA	NA
	9/12/2017	0.25 B	160 160	240 220	6.92 6.9	390 410	1400 1400	0.58 B 0.47		< 0.00046 0.00046 J			< 0.00034 < 0.00034	< 0.0011		< 0.00035 < 0.00035		< 0.00007 < 0.00007	< 0.00085 0.0018 J	0.0057	< 0.000085 < 0.000085	0.576 NA	NA NA	NA NA	NA NA	NA NA
	6/25/2018	0.26 0.25	130	260 F1	7.13	510 F1	1500	0.47		< 0.00046 3			< 0.00034	< 0.0011				< 0.00007	< 0.00085	0.0057 0.025	< 0.000085	NA NA	< 0.00050	< 0.00053	< 0.00074	< 0.00058
	10/1/2018	0.23	120	200	7.13	400	1300	0.69		< 0.00046		NA	< 0.00034	NA	0.00050 J	0.00077 J	< 0.0011	NA	< 0.00085	0.025	NA	0.495	NA	NA	NA	NA
AES MW-2 -	8/8/2017	0.16	88	37	6.53	7.7	460	0.36	< 0.0010	< 0.00046	0.032		< 0.00034	< 0.0011	< 0.000304	< 0.00035		< 0.00007	< 0.00085	0.00035 J		< 0.129	NA NA	NA NA	NA.	NA.
Background	8/15/2017	0.17	88	37	6.83	7.1	470	0.4		0.00047 J			< 0.00034	< 0.0011	< 0.0004	< 0.00035		< 0.00007	< 0.00085		< 0.000085	0.545	NA.	NA.	NA	NA
Well	8/22/2017	0.16	89	37	6.54	10	450	0.4		< 0.00046			< 0.00034	< 0.0011	< 0.0004	< 0.00035		< 0.00007	0.0010 J		< 0.000085	< 0.0379	NA	NA	NA	NA
	8/29/2017	0.17 B	100	37	6.68	16	470	0.42 B		< 0.00046			< 0.00034	< 0.0011	< 0.0004	< 0.00035		< 0.00007	< 0.00085		< 0.000085	0.113	NA	NA	NA	NA
	9/12/2017	0.17	94	36	6.65	9.8	480	0.35	< 0.001	< 0.00046	0.11	< 0.00034	< 0.00034	< 0.0011	< 0.0004	< 0.00035	< 0.0032	< 0.00007	0.00094 J	0.00046 J	< 0.000085	NA	NA	NA	NA	NA
	6/25/2018	0.16	110	140	6.84	43	740	0.52	< 0.0010	< 0.00046	0.15	< 0.00034	< 0.00034	< 0.0011	0.00067 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.00040 J	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0069 J
	10/1/2018	0.16	110	85	7.04	15	690	0.67	< 0.0010	< 0.00046	0.13	NA	< 0.00034	NA	0.00058 J	NA	0.0014 J	NA	< 0.00085	< 0.00024	NA	< 0.321	NA	NA	NA	NA
AES MW-3	8/8/2017	0.78	290	2900	6.74	630	6000	2	< 0.001	0.0038	0.33	< 0.00034	< 0.00034	< 0.0011	0.0018 J	< 0.00035	0.0068	< 0.00007	0.096	0.052	< 0.000085	0.099	NA	NA	NA	NA
	8/15/2017	0.85	320	3400	7.1	1300	7600	2.1	< 0.001	0.0034	0.29	< 0.00034	< 0.00034	< 0.0011	0.0019 J	< 0.00035	0.0077	< 0.00007	0.16	0.098	< 0.000085	0.142	NA	NA	NA	NA
	8/22/2017	0.83	340	3600	6.78	1500	8600	2.2	< 0.001	0.0021	0.37		< 0.00034	< 0.0011	0.0023 J	< 0.00035		< 0.00007	0.2	0.13	< 0.000085	0.212	NA	NA	NA	NA
	8/29/2017	0.90 B	390	3700	7.01	1700	8300	2.3 B	< 0.001	0.0024	0.25		< 0.00034	< 0.0011	0.0022 J	< 0.00035		< 0.00007	0.22	0.14	< 0.000085	0.0888	NA	NA	NA	NA
	9/12/2017	0.9	370	3900	7.03	2300	9900	1.9	0.0012 J	0.0029	0.23		< 0.00034	< 0.0011	0.0025	< 0.00035		< 0.00007	0.28	0.18	< 0.000085	NA	NA	NA	NA	NA
	6/25/2018	1.2	330	4400	7.23	2800	11000	1.6	< 0.0010	0.0018	0.24		0.00042 J	< 0.0011	0.0031	< 0.00035		< 0.000070	0.22	0.21	< 0.000085	NA	0.0027	0.00053 J	< 0.00074	0.004 J
	10/1/2018	1.0	330	4700	7.43	3300	13000	1.6	< 0.0010	0.0024	0.19	NA	< 0.00034	NA	0.0031	NA	0.021	NA	0.22	0.23	NA	0.511	NA	NA	NA	NA
AES MW-4	8/8/2017 8/8/2017 Dup	3.4 3.4	590 620	9800 9900	6.91 6.91	15000 15000	41000 41000	0.63 0.61	< 0.001 0.0014 J	0.0036 0.0031	0.057		0.00036 J < 0.00034	< 0.0011	0.0018 J 0.0017 J	< 0.00035 < 0.00035	1	< 0.00007 < 0.00007	0.44 0.45	0.011 0.011	< 0.000085 < 0.000085	0.527 0.137	NA NA	NA NA	NA NA	NA NA
	8/16/2017 Dup	3.7	620	11000	7.08	16000	43000	0.63	< 0.0014 3	0.0031	0.057		< 0.00034	< 0.0011		< 0.00035	1.1	< 0.00007	0.45	0.0048	< 0.000085	0.137	NA NA	NA NA	NA NA	NA NA
	8/16/2017 Dup	4.1	630	10000	7.08	16000	43000	0.63	< 0.001	0.0037	0.06		< 0.00034	< 0.0011		< 0.00035	1.1	< 0.00007	0.4	0.0048	< 0.000085	0.112	NA NA	NA NA	NA NA	NA NA
	8/23/2017	3.8	620	9800	7.09	15000	42000	0.65	< 0.001	0.0036	0.057		< 0.00034	< 0.0011		< 0.00035		< 0.00007	0.44	0.006	< 0.000085	< 0.0545	NA NA	NA NA	NA.	NA
	8/23/2017 Dup	3.7	590	9900	7.09	15000	42000	0.65	< 0.001	0.0025	0.058		< 0.00034	< 0.0011		< 0.00035	1.1	< 0.00007	0.38	0.0065	< 0.000085	0.0942	NA.	NA.	NA	NA
	8/30/2017	3.6 B	670	11000	7.14	16000	42000	0.68	< 0.001	0.0027	0.055		< 0.00034	< 0.0011		< 0.00035	0.9	< 0.00007	0.4	0.0058	< 0.000085	0.403	NA.	NA.	NA	NA
	8/30/2017 Dup	3.6 B	670	11000	7.14	16000	41000	0.68	< 0.001	0.0024	0.054		< 0.00034	< 0.0011		< 0.00035	0.98	< 0.00007	0.42	0.0054	< 0.000085	< 0.146	NA	NA	NA	NA
	9/12/2017	3.2	600	10000	7.12	17000	42000	0.53	< 0.001	0.0035	0.056	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.75	< 0.00007	0.41	0.013	< 0.000085	NA	NA	NA	NA	NA
	9/12/2017 Dup	3.4	610	10000	7.12	17000	43000	0.63	< 0.001	0.0038	0.056	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.86	< 0.00007	0.42	0.014	< 0.000085	NA	NA	NA	NA	NA
	6/26/2018	3.2	460	9100	7.27	12000	16000	0.76	0.0023 J	0.0024	0.044	< 0.00034	0.00034 J	< 0.0011	0.0016 J	< 0.00035	0.54	< 0.000070	0.55	0.0064	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0053 J
	6/26/2018 Dup	3.2	440	8900	7.27	12000	17000	0.76	0.0019 J	0.0021	0.046	< 0.00034	< 0.00034	< 0.0011	0.0016 J	< 0.00035		< 0.000070	0.58	0.0055	< 0.000085	NA	< 0.00050	< 0.00053	< 0.00074	0.0046 J
	10/2/2018	2.6	280	5600	7.41	6000	21000	1.0	< 0.0010	0.0031	0.035	NA	0.00057 J	NA	0.0016 J	NA	0.38	NA	0.74	0.0043	NA	< 0.0708	NA	NA	NA	NA
	10/2/2018 Dup	2.6	250	5300	7.41	6200	22000	1.0	< 0.0010	0.0027	0.036	NA	0.00051	NA	0.0016 J	NA	0.34	NA	0.76	0.0048	NA	< 0.168	NA	NA	NA	NA
AES MW-5	8/9/2017	0.37	850	3800	6.52	2500	8200	0.42	< 0.001	0.0032	0.041		< 0.00034	< 0.0011	0.0034	< 0.00035		< 0.00007	0.0022 J	0.01	< 0.000085	0.473	NA	NA	NA	NA
	8/16/2017	0.46	890	3800	6.61	2700	7900	0.45	< 0.001	0.0024	0.043		< 0.00034	< 0.0011	0.0035	< 0.00035		< 0.00007	0.0086 J	0.013	< 0.000085	0.576	NA	NA	NA	NA
	8/22/2017	0.39	800	3700 3700	6.49 6.79	2500	11000 9800	0.46	< 0.001	0.0018	0.039		< 0.00034	< 0.0011	0.0036	< 0.00035		< 0.00007	0.0080 J	0.014	< 0.000085	0.102	NA	NA NA	NA	NA
	8/29/2017 9/12/2017	0.39 B 0.37	930 830	3400	6.79	2600 2600	9800	0.48	< 0.001 < 0.001	0.0021	0.036		< 0.00034 < 0.00034	< 0.0011 < 0.0011	0.0033	< 0.00035 < 0.00035		< 0.00007 < 0.00007	0.0057 J 0.0048 J	0.0099	< 0.000085 < 0.000085	0.601 NA	NA NA	NA NA	NA NA	NA NA
	6/26/2018	0.47	690	3700	6.72	2100	8700	0.49	< 0.0010	0.0041	0.036		< 0.00034	< 0.0011	0.0033	< 0.00035		< 0.000070	0.0048 J	< 0.0003		NA	< 0.00050	< 0.00053	0.046	0.75
	10/2/2018	0.39	710	3700	6.73	2200	10000	0.45	< 0.0010	0.0071	0.030	NA	< 0.00034	NA	0.0030 J	NA	0.0038	NA	0.00423	0.00046	NA	< -0.0397	NA	NA	NA	NA
TW-A	12/12/2017	0.14	170	49	6.92	280	930	0.26	< 0.0010	0.0000 J	0.26	<0.00034	< 0.00034	<0.0011	0.00071 J	<0.00035	<0.0011	<0.00007	0.0014 J	0.00040	<0.000085	NA	NA NA	NA NA	NA.	NA.
,	7/10/2018	0.14	110	54	6.96	79	620	0.3	< 0.001	< 0.00046	0.19	< 0.00034	< 0.00034	<0.0011	0.00098 J	<0.00035	< 0.0011	<0.00007	< 0.00085	0.0015	<0.000085	NA	NA NA	NA.	NA.	<0.00061
TW-B	12/12/2017	0.59	170	300	7.07	670 F1	2300	1.2	< 0.001	0.00069 J	0.035	< 0.00034	< 0.00034	<0.0011	0.0012 J	<0.00035	0.0035 J	<0.00007	0.0044 J	0.0004 J	<0.000085	NA	NA NA	NA NA	NA	NA
	7/10/2018	0.54	140	240	6.96	660	2000	1.3	< 0.001	< 0.00046	0.033	< 0.00034	< 0.00034	< 0.0011	0.0012 J	< 0.00035		<0.00007	0.0028 J	0.00081 J		NA	NA	NA	NA	<0.00062
TW-C	12/12/2017	3.6	310	13000	7.54	1700	25000	1.1	0.0014 J	0.0038	0.15	< 0.00034	< 0.00034	0.0015 J	< 0.0004	< 0.00035	0.073	< 0.00007	0.0018 J	0.00064 J	<0.000085	NA	NA	NA	NA	NA
	7/10/2018	2.3	310	6900	7.18	3100	17000	1.7	< 0.001	0.0023	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.0004	< 0.00035	0.014	< 0.00007	0.0061 J	0.00061 J	<0.000085	NA	NA	NA	NA	< 0.00066
TW-D	12/12/2017	0.27	170	300	6.45	250	1400	0.35	< 0.001	0.0023	0.11	<0.00034	< 0.00034	<0.0011	0.0021 J	<0.00035	<0.0011	<0.00007	0.0029 J	0.0024	<0.000085	NA	NA	NA	NA	NA
	7/11/2018	0.17	74	96	6.99	110	620	0.44	< 0.001	< 0.00046	0.055	< 0.00034	< 0.00034	< 0.0011	0.0014 J	< 0.00035	< 0.0011	<0.00007	<0.00085	0.00027 J		NA	NA	NA	NA	0.0022 J
	7/11/18 DUP	0.2	85	99	NA	110	620	0.5	< 0.001	<0.00046	0.064	<0.00034	<0.00034	<0.0011	0.0014 J	<0.00035	<0.0011	<0.00007	<0.00085	0.0004 J	<0.000085	NA	NA	NA	NA	0.0022 J

CCR - Coal Combustion Residuals.

mg/L - milligram per liter.
MS/MSD - Matrix spike/Matrix spike duplicate.
NA - Not available/Constituent not analyzed. pCi/L - picoCurie per liter.

SL - Screening Level.

S.U. - Standard Units. TDS - Total Dissolved Solids.

USEPA - United States Environmental Protection Agency.

VOC - Volatile Organic Compound.

Qualifiers:

- Not Detected, value is the reporting limit.

B - Analyte found in sample and associated blank.

F1 - MS/MSD Recovery was outside acceptance limits.

J - Value is estimated.

- (a) Puerto Rico Ecological Screening Levels selected in Table 3 as:
 Puerto Rico Coastal and Estuarine Water Quality Standards Aquatic.
 USEPA National Recommended Ambient Water Quality Criteria Aquatic Life Saltwater (chronic).
 (b) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).
 (c) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

- (d) Volatile organic compounds (VOCs) detected in one or more samples are shown.

greater than the Selected Ecological Screening Level.

2/28/2019 Haley & Aldrich, Inc.

TABLE 9
COMPARISON OF CCR RULE GROUNDWATER MONITORING AND TEMPORARY WELL RESULTS TO ECOLOGICAL SCREENING LEVELS - DISSOLVED (FILTERED)
AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

			,	Appendix III (b)		Appendix III and IV (b, c)						,	Appendix IV (c)					
	Constituent	Boron	Calcium	Chloride	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury	Molybdenum	Selenium	Thallium
	Eco SL (a)	NA	NA	NA	NA	NA	NA	NA	0.036	NA	NA	0.0079	0.05	NA	0.0077	NA	0.0008	NA	0.071	NA
Well ID	Sampling Event Date	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
AES MW-1 -																				
Background Well	6/25/2018	0.28	130	260 F1	490 F1	1600	0.61	< 0.0010	< 0.00046	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.025	< 0.000085
AES MW-2 -																				
Background Well	6/25/2018	0.17	110	130	44	730	0.5	< 0.0010	< 0.00046	0.15	< 0.00034	< 0.00034	< 0.0011	0.00067 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.00030 J	< 0.000085
AES MW-3	6/25/2018	1.1	320	4300	2500	10000	1.7	< 0.0010	0.0016	0.26	< 0.00034	0.00034 J	< 0.0011	0.0034 J	< 0.00035	0.0064	< 0.000070	0.2	0.2	< 0.000085
AES MW-4	6/26/2018	3.4	450	9100	11000	13000	0.76	< 0.0010	0.0024	0.045	< 0.00034	< 0.00034	< 0.0011	0.0017 J	< 0.00035	0.56	< 0.000070	0.58	0.005	< 0.000085
	6/26/2018 Dup	3.5	450	8700	11000	14000	0.74	< 0.0010	0.0022	0.046	< 0.00034	0.00035 J	< 0.0011	0.0016 J	< 0.00035	0.59	< 0.000070	0.6	0.0054	< 0.000085
AES MW-5	6/26/2018	0.44	670	3400	2100	8800	0.48	< 0.0010	0.0059	0.036	< 0.00034	< 0.00034	< 0.0011	0.003	< 0.00035	0.0047 J	< 0.000070	0.0034 J	< 0.00024	< 0.000085
TW-A	7/10/2018	0.13	110	55	78	610	0.28	< 0.0010	< 0.00046	0.18	< 0.00034	< 0.00034	< 0.0011	0.00044 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	0.0014	< 0.000085
TW-B	7/10/2018	0.51	140	240	670	2000	1.3	< 0.0010	0.00071 J	0.03	< 0.00034	< 0.00034	< 0.0011	0.00082 J	< 0.00035	0.0031 J	< 0.000070	0.0041 J	0.00033 J	< 0.000085
TW-C	7/10/2018	2.3	310	6600	3000	18000	1.7	< 0.0010	0.0029	0.04	< 0.00034	< 0.00034	< 0.0011	< 0.00040	< 0.00035	0.014	< 0.000070	0.0076 J	0.00026 J	< 0.000085
TW-D	7/11/2018	0.22	82	100	110	590	0.45	< 0.0010	0.00084 J	0.063	< 0.00034	< 0.00034	< 0.0011	0.00092 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085
	7/11/18 DUP	0.21	79	99	110	610	0.47	< 0.0010	0.00086 J	0.061	< 0.00034	< 0.00034	< 0.0011	0.00093 J	< 0.00035	< 0.0011	< 0.000070	< 0.00085	< 0.00024	< 0.000085

CCR - Coal Combustion Residuals.

mg/L - milligram per liter.

MS/MSD - Matrix spike/Matrix spike duplicate.

NA - Not Available.

SL - Screening Level.

TDS - Total Dissolved Solids.

USEPA - United States Environmental Protection Agency.

(a) - Puerto Rico Ecological Screening Levels selected in Table 3 as:

Puerto Rico Coastal and Estuarine Water Quality Standards - Aquatic.

USEPA National Recommended Ambient Water Quality Criteria - Aquatic Life Saltwater (chronic).

(b) - The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

(c) - The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

greater than the Selected Ecological Screening Level.

Qualifiers:

- < Not Detected, value is the reporting limit.
- B Analyte found in sample and associated blank.
- F1 MS/MSD Recovery was outside acceptance limits.
- J Value is estimated.

TABLE 10
COMPARISON OF HARBOR WATER SAMPLE RESULTS TO HUMAN HEALTH RECREATIONAL AND ECOLOGICAL SCREENING LEVEL
AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

					Appendi	ix III (c)			Appendix III and IV (c, d)							Appendix I	IV (d)					
	Fraction	Constituent	Boron	Calcium	Chloride	pН	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury	Molybdenum	Selenium	Thallium
		Federal and Puerto Rico																				
	Total	HH Rec SL (a) Federal and Puerto Rico		NA	NA	7.3 - 8.5	2800	NA	NA	0.64	0.00014	NA	NA	NA	NA	NA	NA	NA	0.000051	NA	4.2	0.00047
	Dissolved	HH Rec SL (a)		NA	NA	NA	2800	NA	NA	0.64	0.00014	NA	NA	NA	NA	NA	NA	NA	0.000051	NA	4.2	0.00047
Harbor	Total	Eco SL (b)	NA	NA	NA	7.3 - 8.5	NA	NA	NA	NA	0.036	NA	NA	0.00885	0.050	NA	0.00852	NA	0.00094	NA	0.07114	NA
Water	Dissolved	Eco SL (b)	NA	NA	NA	NA	NA	NA	NA	NA	0.036	NA	NA	0.0079	0.050	NA	0.0077	NA	0.00080	NA	0.071	NA
Sample ID	Fraction	Sampling Event Date	mg/L	mg/L	mg/L	S.U.	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
AES-SEA	Total	7/10/2018	4.4	390	20000	8.4	2400	40000	0.88	<0.001	0.0024	0.0084	< 0.00034	< 0.00034	<0.0011	<0.0004	< 0.00035	0.19	< 0.00007	0.009 J	0.00079 J	<0.000085
AES-SEA	Dissolved	7/10/2018	4.2	370	20000	NA	2400	39000	0.88	< 0.001	0.0032	0.0081	< 0.00034	< 0.00034	< 0.0011	< 0.0004	< 0.00035	0.18	< 0.00007	0.0096 J	0.00066 J	<0.000085

CCR - Coal Combustion Residuals.

HH - Human Health.

mg/L - milligram per liter.

NA - Not available.

Rec - Recreational.

SL - Screening Level.

S.U. - Standard Units.

TDS - Total Dissolved Solids.

USEPA - United States Environmental Protection Agency.

(a) - Puerto Rico Human Health Recreational Screening Levels selected in Table 3 as:

Puerto Rico Coastal and Estuarine Water Quality Standards - Human Health.

USEPA National Recommended Water Quality Criteria - Human Health for the Consumption of Organism Only. Applies to total concentrations.

(b) - Ecological Screening Levels selected in Table 3 as:

Puerto Rico Coastal and Estuarine Water Quality Standards - Aquatic.

USEPA National Recommended Ambient Water Quality Criteria - Aquatic Life Saltwater (chronic).

(c) - The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).

(d) - The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

greater than the Selected Federal and Puerto Rico Human Health Recreational Screening Level.

Qualifiers:

J - Value is estimated.

< - Not Detected, value is the reporting limit.

TABLE 11
COMPARISON OF HARBOR SAMPLE ANALYTICAL RESULTS TO TYPICAL SEAWATER COMPOSITION AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

					Appendi	ix III (d)			Appendix III and IV (d, e)						Ар	pendix IV	(e)					
		Constituent	Boron	Calcium	Chloride	pН	Sulfate	TDS	Fluoride	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Lead	Lithium	Mercury	Molybdenum	Selenium	Thallium
	Seawater (Composition (a)	4.45	411	19345	7.3 - 9.5. (c)	2701	NA	1	0.00033	0.0026	0.021	0.0000006	0.00011	0.0002	0.00039	0.00003	0.17	0.00015	0.01	0.0009	NA
Harbor Water	Seawater	Composition (b)	4.5	410	19000	NA	2700	NA	1.3	0.0003	0.003	0.02	0.0000006	0.00011	0.00005	0.0004	0.00003	0.17	0.0002	0.01	0.00009	NA
Sample ID	Sampling	Fraction	mg/L	mg/L	mg/L	S.U.	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
AES-SEA	7/10/2018	Dissolved	4.2	370	20000	NA	2400	39000	0.88	<0.001	0.0032	0.0081	<0.00034	<0.00034	<0.0011	< 0.0004	<0.00035	0.18	<0.00007	0.0096 J	0.00066 J	< 0.000085
AES-SEA	7/10/2018	Total	4.4	390	20000	8.4	2400	40000	0.88	<0.001	0.0024	0.0084	<0.00034	< 0.00034	<0.0011	< 0.0004	<0.00035	0.19	<0.00007	0.009 J	0.00079 J	<0.000085

Blank cells indicate constituent not analyzed.

- J Value is estimated.
- mg/L milligram per liter.
- S.U. Standard Units.
- < Not Detected, value is the reporting limit.
- (a) Values from The chemical composition of seawater. 2006. Dr J Floor Anthoni.
 - Detailed composition of seawater. (Source cited as: Karl K Turekian: Oceans. 1968. Prentice-Hall).
 - http://www.seafriends.org.nz/oceano/seawater.htm#gases
- (b) Values from USGS. 1985. Study and Interpretation of the Chemical Characteristics of Natural Water. U.S. Geological Survey.
 - Table 2. Composition of Seawater (Source cited as: Goldberg and others (1971)).
 - https://pubs.usgs.gov/wsp/wsp2254/pdf/intro.pdf
- (c) Ocean pH varies from about 7.90 to 8.20 but along the coast one may find much larger variations from 7.3 inside deep estuaries to 8.6 in productive coastal plankton blooms and 9.5 in tide pools.
- (d) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).
- (e) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).

TABLE 12
DERIVATION OF GROUNDWATER RISK-BASED SCREENING LEVELS PROTECTIVE OF HARBOR WATER
AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

	Est	imated Dilution A	Attenuation Factor -	Las Mareas Harbor (d) =	1,300			
Constituents	Selected Federal and Puerto Rico HH REC SL (b) (mg/L)	Selected Puerto Rico Eco SL - Total (c) (mg/L)	Selected Federal and Puerto Rico Eco SL - Dissolved (c) (mg/L)	Lowest of the Human Health and Ecological Screening Levels (mg/L)	Groundwater Risk- Based Screening Level (c) (mg/L)	Ma Groundwate	eximum er Concentration mg/L)	Ratio Between Groundwater Risk-Based Screening Level and the Maximum RIEC Groundwater Concentration
Inorganics								
Antimony	0.64	NA	NA	0.64	832	0.0023	AES MW-4	>360,000
Arsenic	0.00014	0.036	0.036	0.00014	0.182	0.0088	AES MW-5	>20
Barium	NA	NA	NA	NA	NA	0.37	AES MW-3	NA
Beryllium	NA	NA	NA	NA	NA	ND		ND
Boron	NA	NA	NA	NA	NA	4.1	AES MW-4	NA
Cadmium	NA	0.00885	0.0079	0.0079	10.2	0.00057	AES MW-4	>17,000
Calcium	NA	NA	NA	NA	NA	930	AES MW-5	NA
Chloride	NA	NA	NA	NA	NA	13000	TW-C	NA
Chromium	NA	0.05	0.050	0.050	64.5	0.0015	TW-C	>43,000
Cobalt	NA	NA	NA	NA	NA	0.0036	AES MW-5	NA
Fluoride	NA	NA	NA	NA	NA	2.3	AES MW-3	NA
Lead	NA	0.00852	0.0077	0.0077	10.0	0.00077	AES MW-1 (e)	>13,000
Lithium	NA	NA	NA	NA	NA	1.1	AES MW-4	NA
Mercury	0.000051	0.00094	0.00080	0.00005	0.0663	ND		ND
Molybdenum	NA	NA	NA	NA	NA	0.76	AES MW-4	NA
Radium 226/228	NA	NA	NA	NA	NA	0.601	AES MW-5	NA
Selenium	4.2	0.07114	0.071	0.071	92.1	0.23	AES MW-3	>400
Sulfate	2800	2800	NA	2800	3640000	17000	AES MW-4	>200
Thallium	0.00047	NA	NA	0.00047	0.611	ND		ND
Total Dissolved Solids	NA	NA	NA	NA	NA	43000	AES MW-4	NA
pH	7.3-8.5	7.3-8.5	NA	NA	NA	7.54	TW-C	NA
VOCs and Sulfolane								
Chlorobenzene	1.6	NA	NA	1.6	2080	0.0027	AES MW-3	>770,370
Isopropylbenzene	NA	NA	NA	NA	NA	0.00053	AES MW-3	NA
Methyl tert-butyl ether	NA	NA	NA	NA	NA	0.046	AES MW-5	NA
Sulfolane	NA	NA	NA	NA	NA	0.75	AES MW-5	NA

ECO SL - Ecological Screening Level.

HH REC SL - Human Health Recreational Use Screening Level.

mg/L - milligram per liter.

NA - Not Available.

⁽a) - The hierarchy for selecting the Puerto Rico Human Health Recreational Screening Level is: Puerto Rico Coastal and Estuarine Water Quality Standards - Human Health; USEPA AWQC Human Health for the Consumption of Organism Only.

⁽b) - The hierarchy for selecting the Puerto Rico Ecological Screening Level is: Puerto Rico Coastal and Estuarine Water Quality Standards - Aquatic; USEPA Ambient Water Quality Criteria for Saltwater (chronic).

⁽c) - Where the Groundwater Risk-Based Screening Level = Screening Level x Dilution Factor.

⁽d) - Estimated value, see text for derivation.

⁽d) - MW-1 is a background well.

TABLE 13a SUMMARY OF GROUNDWATER AND HARBOR SAMPLE SCREENING RESULTS AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

Constituent		Screening Level Results									
		Groundwater - Human Health Drinking Water Screening Levels		Groundwater - Human Health Recreational Screening Levels		Groundwater - Ecological Screening Levels		Harbor - Human Health Recreational Screening Levels		Harbor - Ecological Screening Levels	
		Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved	Total
	Boron		1 : 51 2%								
	Calcium										
Appendix III (a)	Chloride	6 : 11 55%	34 : 51 67%								
дрених III (а)	pН		2 : 50 4%		45 : 50 90%		45 : 50 90%				
	Sulfate	7 : 11 64%	40 : 51 78%	3 : 11 27%	16 : 51 31%						
	TDS	11 : 11 100%	46 : 51 90%								
Appendix III and IV (a, b)	Fluoride										
	Antimony										
	Arsenic			8 : 11 73%	36 : 51 71%			1 : 1 100%	1 : 1 100%		
	Barium										
	Beryllium										
	Cadmium										
	Chromium										
Annondiy IV (b)	Cobalt										
Appendix IV (b)	Lead										
	Lithium	2 : 11 18%	15 : 51 29%								
	Mercury										
	Molybdenum	3 : 11 27%	20 : 51 39%								
	Selenium	1 : 11 9%	7 : 51 14%			1 : 11 9%	6 : 51 12%				
	Thallium										
	Radium 226/228							NA	NA	NA	NA
Sulfolane and VOCs (c)	Chlorobenzene							NA	NA	NA	NA
	Isopropylbenzene							NA	NA	NA	NA
	ether		1 : 6 17%					NA	NA	NA	NA
	Sulfolane		1 : 11 9%					NA	NA	NA	NA

Notes:

Number of exceedances: total number of samples.

Blank cells - no results above screening levels for the specified constituent / media.

CCR - Coal Combustion Residuals.

NA - Constituent/media not analyzed.

TDS - Total Dissolved Solids.

VOC - Volatile Organic Compound.

- (a) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).
- (b) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).
- (c) VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility.

TABLE 13b SUMMARY OF GROUNDWATER AND HARBOR SAMPLE SCREENING RESULTS AES PUERTO RICO LP, GUAYAMA, PUERTO RICO

		Screening Level Results									
Constitue	Groundwater - Human Health Drinking Water Screening Levels		Groundwater - Human Health Recreational Screening Levels		Groundwater - Ecological Screening Levels		Harbor - Human Health Recreational Screening Levels		Harbor - Ecological Screening Levels		
	Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved	Total	
	Boron		1 : 51								
Appendix III (a)	Calcium										
	Chloride	6 : 11	34 : 51								
	pН		2 : 50		45 : 50		45 : 50				
	Sulfate	7 : 11	40 : 51	3 : 11	16 : 51						
	TDS	11 : 11	46 : 51								
Appendix III and IV (a, b)	Fluoride										
	Antimony										
	Arsenic			8 : 11	36 : 51			1 : 1	1 : 1		
	Barium										
	Beryllium										
	Cadmium										
	Chromium										
Appendix IV (b)	Cobalt										
	Lead										
	Lithium	2 : 11	15 : 51								
	Mercury										
	Molybdenum	3 : 11	20 : 51								
	Selenium	1 : 11	7 : 51			1 : 11	6 : 51				
	Thallium										
	Radium 226/228							NA	NA	NA	NA
Sulfolane and VOCs (c)	Chlorobenzene							NA	NA	NA	NA
	Isopropylbenzene							NA	NA	NA	NA
	ether		1 : 6					NA	NA	NA	NA
	Sulfolane		1 : 11					NA	NA	NA	NA

Number of exceedances: total number of samples.

Blank cells - no results above screening levels for the specified constituent / media.

CCR - Coal Combustion Residuals.

NA - Constituent/media not analyzed.

TDS - Total Dissolved Solids.

VOC - Volatile Organic Compound.

- (a) The CCR Rule lists these constituents as Constituents for Detection Monitoring (Appendix III).
- (b) The CCR Rule lists these constituents as Constituents for Assessment Monitoring (Appendix IV).
- (c) VOCs are not associated with CCR, but are known to be present in groundwater due to the activities at the neighboring facility.

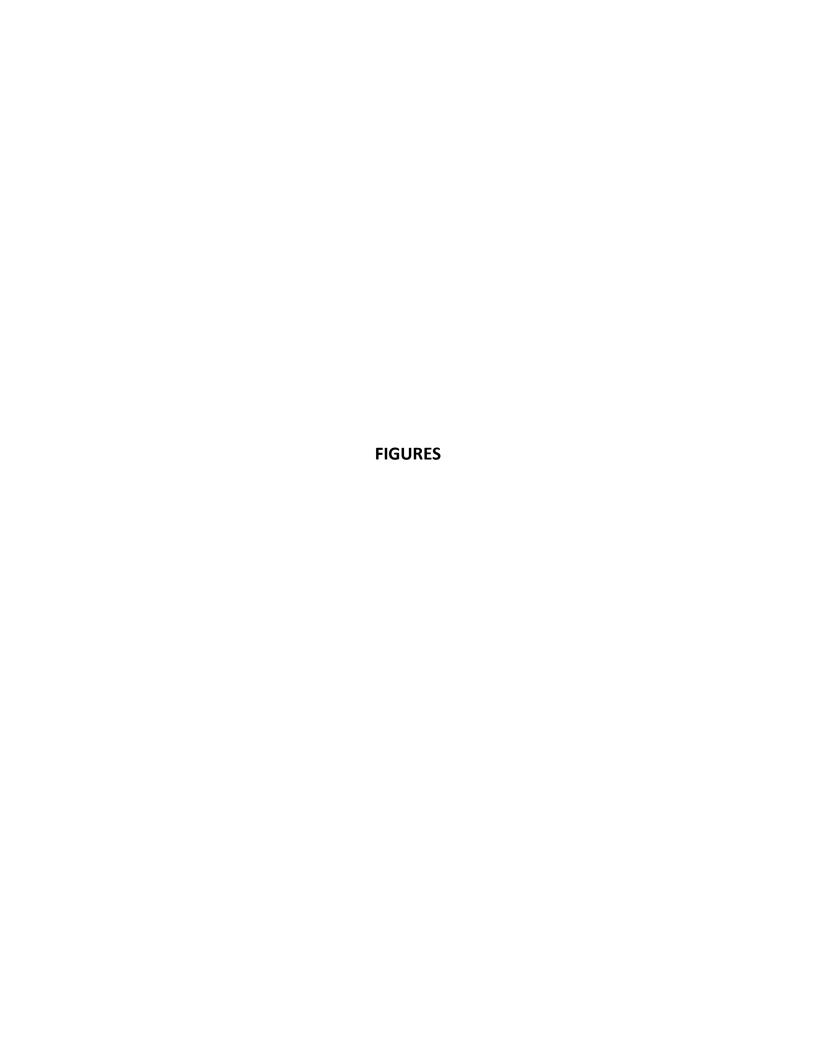
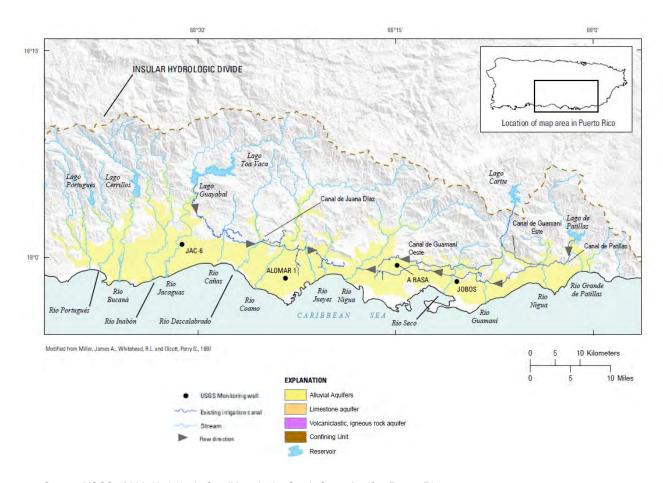




FIGURE 2 SOUTH COAST ALLUVIAL AQUIFER AES PUERTO RICO LP, GUAYAMA, PUERTO RICO



Source: USGS. 2016. Hydrologic Conditions in the South Coast Aquifer, Puerto Rico, 2010–15. U.S. Department of the Interior. U.S. Geological Survey. Available at: https://pubs.er.usgs.gov/publication/ofr20151215

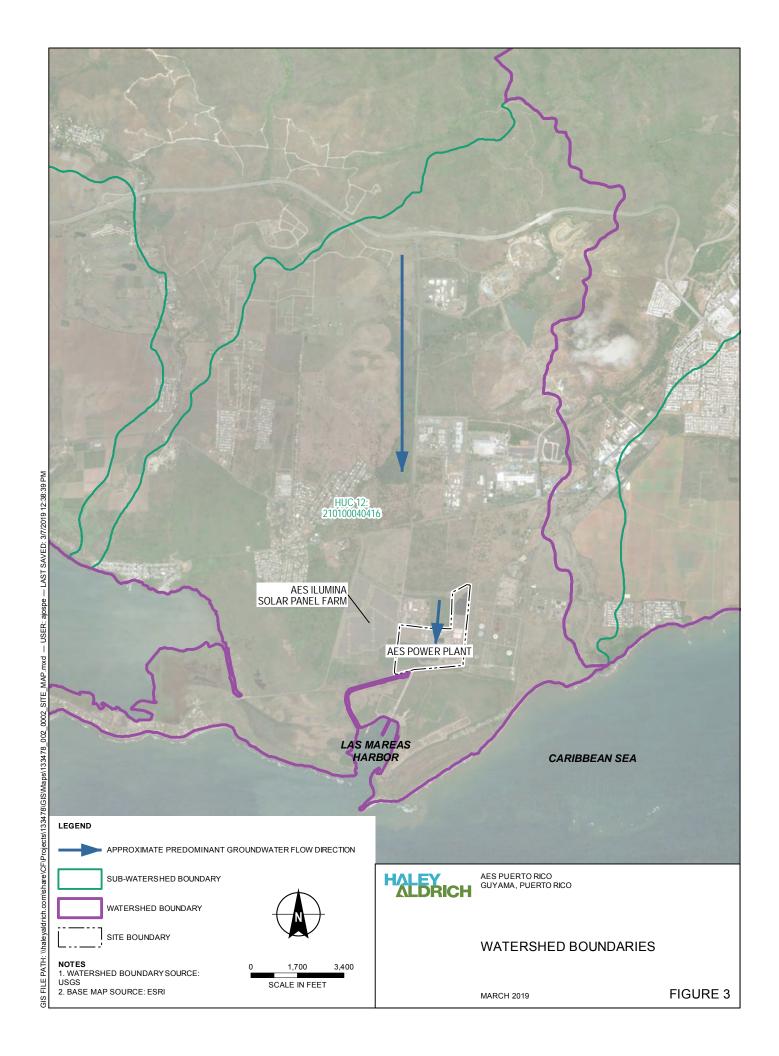
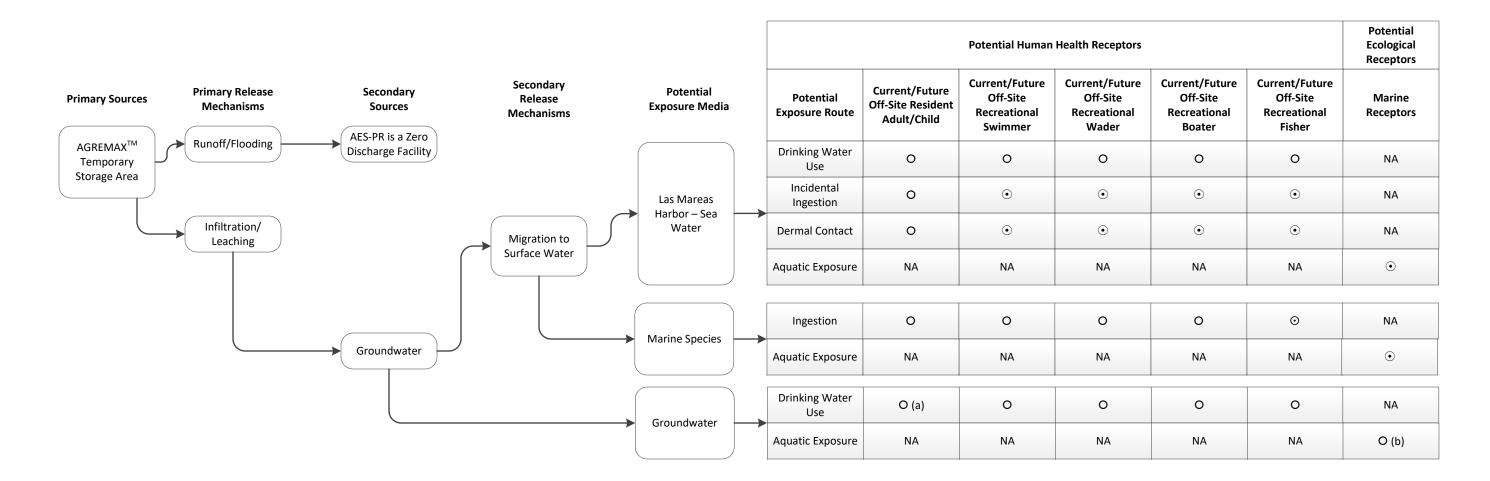


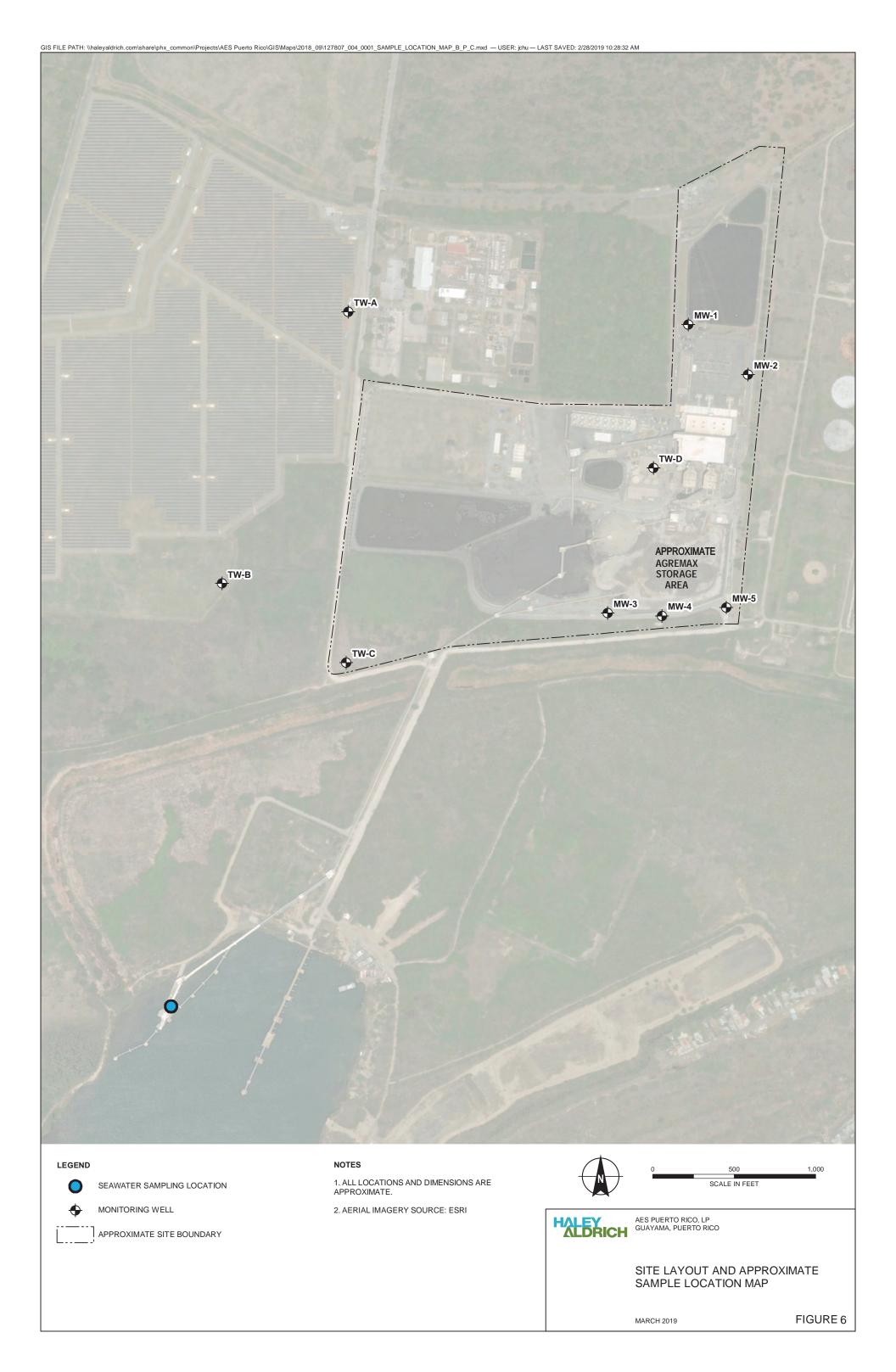
FIGURE 5 CONCEPTUAL SITE MODEL AES PUERTO RICO LP, GUAYAMA, PUERTO RICO



Notes:

- Pathway potentially complete pathway evaluated in this risk assessment; results indicate no risk to human health or the environment.
- O Pathway evaluated and found incomplete; results indicate no risk to human health or the environment.
- (a) The groundwater in the vicinity of AES-PR is not used for drinking water purposes.
- (b) Ecological Receptors are not exposed to groundwater.
- NA Not Applicable.





APPENDIX A

Surface Water Dilution Attenuation Factor

APPENDIX A

SURFACE WATER DILUTION ATTENUATION FACTOR

This appendix describes the evaluation of the magnitude of dilution effects resulting from the mixing of groundwater that may flow from beneath the AGREMAX™ temporary storage area to the nearby surface water body – the Las Mareas Harbor (**Figure A-1**) and documents the development of a surface water dilution attenuation factor (SW – DAF) between groundwater and surface water. The groundwater flow direction shown in Figure A-1 is based on the configuration of the concentration contour lines for sulfolane, which is a groundwater contaminant originated from an adjacent industrial site (PEI, 2016).

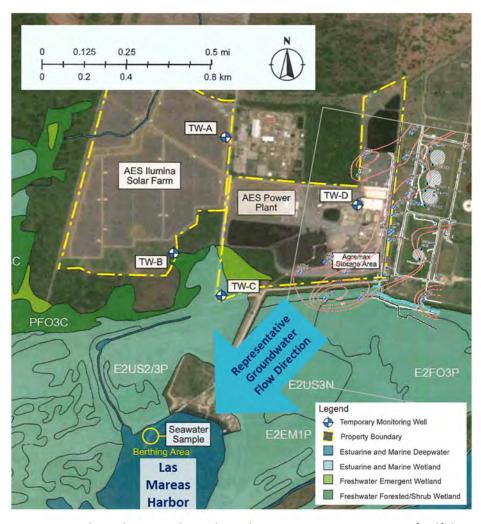


Figure A-1: Site settings. The red contour lines show the concentration contours of sulfolane originating from the neighboring site. The approximate location of the AGREMAX $^{\text{\tiny M}}$ temporary storage area is shown.



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The magnitude of the dilution effect is estimated using the approach below:

- Estimate the flow rate of shallow groundwater beneath the AGREMAX™ temporary storage area across the property boundary (Qgw);
- Estimate the flow rate of the sea water flushing in the Las Mareas Harbor (Qsea); and
- Calculate the SW DAF using the equation: SW DAF = Qsea ÷ Qgw.

Evaluation of Shallow Groundwater Flow Rate Beneath the AGREMAX™ Temporary Storage Area

The rate of shallow groundwater flow beneath the AGREMAX™ temporary storage area was estimated based on the following assumptions and approach:

- Groundwater flow follows Darcy's law: Qgw = K · i · Ac, where Qgw is the groundwater flow rate, K is horizontal hydraulic conductivity, i is horizontal hydraulic gradient, and Ac is the vertical cross-section area that groundwater potentially impacted by leachate from the AGREMAX™ temporary storage area may flow through;
- A conservative K value of 1 feet per day was assumed for the Qgw calculation. This K value is higher than the range of the K values (0.035 – 0.67 feet per day) found through site-specific slug tests (DNA-Environment, 2017);
- A conservative i value of 0.02 feet was assumed for the Qgw calculation. This gradient is higher than the estimated gradient of 0.0105 (DNA-Environment, 2017);
- The cross-section area, Ac, was estimated using a width of 1,400 feet and the saturated thickness of 20 feet (Figure A-2). Both are conservative assumptions based on the groundwater characterization results (DNA-Environment, 2017); the resulting Ac is 280,000 square feet; and
- Based on the assumed values above, Qgw was estimated to be 560 cubic feet per day.

Evaluation of Sea Water Flushing Rate in the Las Mareas Harbor

The direction of groundwater flow is toward the Las Mareas Harbor (Figure A-1). The mechanism of and physical processes involved in submarine groundwater discharge are shown in Figure A-3 (Urish, and McKenna, 2004, Robinson et al., 2007). Based on the flow dynamics near the shore, shallow groundwater typically discharges to the sea near the base of the low tide area in the intertidal zone (Figure A-3); therefore, mixing between the discharged shallow groundwater and seawater flushing in the harbor due to tidal fluctuation can readily occur. Based on the tidal data obtained from the National Oceanic & Atmospheric Administration website for the station in Las Mareas, Puerto Rico (Station ID: 9755679), the mean tidal fluctuation range is 0.64 feet. To conservatively estimate the daily seawater flushing rate, the tidal fluctuation range was assumed to be 0.3 feet, which represents the neap tide conditions. The area of the harbor was estimated to be 0.09 square miles (Figure A-4). Based on this information, a conservative estimate of the seawater flushing volume for the harbor (Qsea) is 753,000 cubic feet per day (= 0.09 square miles x 0.3 feet per day).



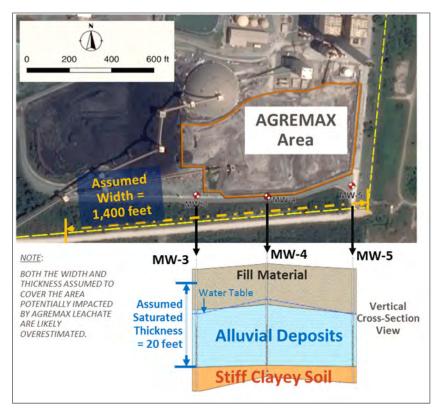


Figure A-2: Conservative assumptions for the cross-section area that AGREMAX $^{\text{\tiny{IM}}}$ -impacted groundwater may flow through. The approximate location of the AGREMAX $^{\text{\tiny{IM}}}$ temporary storage area is shown.

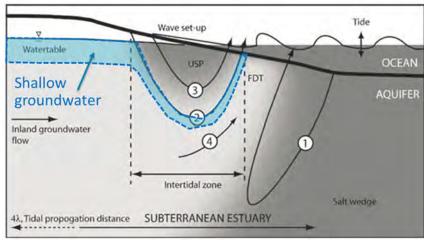


Figure A-3: Conceptual diagram of subterranean estuary including major nearshore flow processes: (1) density-driven circulation (2) tide-induced circulation (3) wave set-up driven circulation and (4) fresh groundwater discharge through the freshwater discharge "tube" (FDT). The blue shaded area shows that the shallow groundwater typically discharges near the base of the low tide area in the intertidal zone.



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Figure A-4: Surface area of the Las Mareas Harbor.

Dilution and Attenuation Effects

Based on the conservative Qgw and Qsea values estimated above, the Surface Water Dilution Attenuation Factor (SW – DAF) is calculated:

$$SW - DAF = \frac{Q_{sea}}{Q_{GW}} = \frac{753,000 \ cubic \ feet \ per \ day}{560 \ cubic \ feet \ per \ day} = 1300$$

This value represents a conservative estimate of the magnitude of dilution for potentially impacted groundwater discharging directly to the Las Mareas Harbor.



AES Puerto Rico, PR 28 February 2019 Appendix A Page 5

REERENCES

- 1. DNA-Environment. 2017. Groundwater Monitoring System & Sampling and Analysis Program, AES Puerto Rico LP, Guayama, Puerto Rico. August.
- 2. PEI. 2016. Corrective Measures Study Report, Chevron Phillips Chemical Puerto Rico Core, LLC, Guayama, Puerto Rico. April.
- 3. Robinson, C., Li, L. and Prommer, H. 2007. Tide-induced recirculation across the aquifer-ocean interface. Water Resources Research, 43(7).
- 4. Urish, D.W. and McKenna, T.E. 2004. Tidal effects on ground water discharge through a sandy marine beach. Ground Water, 42(7), pp.971-982.



APPENDIX B

Response to Comments



Appendix B

Response to Comments AES Puerto Rico - AGREMAX™ Staging Area Corrective Measures Assessment

This document provides responses to comments received on the Corrective Measures Assessment (CMA) AES Puerto Rico (AES-PR) − AGREMAXTM Staging Area. AES-PR received public input and comments during the public meeting on December 12, 2019 at 2:00 pm and accepted comments through a portal on its coal combustion residuals (CCR) public website from December 12, 2019 through January 28, 2020. AES-PR notified the public of the public meeting on November 13, 2019 by way of its CCR public website and through publication in the regional newspaper, the Regional de Guayama¹. AES held the public meeting at Centro de Usos Múltiples Comunidad Olimpo (Olimpio Community Multipurpose Center) in Guayama, Puerto Rico. The public meeting consisted of a presentation by AES representatives describing and explaining the CMA followed by a public comment period. The meeting duration was approximately three and a half hours with approximately 100 public attendees. The CMA presentation materials, and discussions were provided in Spanish².

AES-PR received verbal comments from the public during the public meeting and written comments through its CCR public website portal. In addition, AES-PR received written comments from the Puerto Rico Department of Natural and Environmental Resources (DNER) and U.S EPA Region 2 by electronic mail. AES-PR also received questions and comments on topics outside the scope of the CMA which are not addressed herein. Questions which are addressed by information provided in the Selection of Remedy report are not repeated herein. AES-PR has summarized and consolidated comments and questions where possible.

Public Comments received at Public Meeting and through the CCR Website Portal

I. Corrective Measures Assessment

a. **General.** AES-PR received general comments and questions related to the CMA and the presented remedies as follows:

i. The liner on alternative one is delicate and thin and will break.

RESPONSE: The geosynthetic 60-mil high-density polyethylene (HDPE) flexible membrane liner (FML) which is part of the AGREMAXTM liner system defined in CMA remedial Alternative 1,is compliant with industry standards for geosynthetic liner components. In addition, there are rigorous quality assurance/quality control (QA/QC) requirements which include both material manufacturing and field placement specification to ensure that the liner meets the project specifications and industry standards. Further, the waste management industry has decades of

¹ The Regional de Guayama has a weekly circulation of approximately 55,000 copies in the municipality of Guayama and the adjacent municipalities of Arroyo, Cayey, Coamo, Maunabo, Patillas, Salinas, Santa Isabel, and others.

² AES also provided the presentation materials in English for viewing and offered to provide the presentation discussion in English. However, there were no requests to provide the discussion in English.

performance testing and field performance documentation which confirms the longevity and predictable long-term future performance of the FML prescribed for the AGREMAXTM liner system.

ii. What are the evaluations and the post actions referenced on page 11 of the CMA?

RESPONSE: Page 11 text is part of Section 3 of the CMA – Risk Assessment and Exposure Evaluation and provides a summary of the discussion on that section, which is a summary of the "Groundwater Risk Evaluation" report provided as Appendix B of the CMA. AES-PR will continue to comply with the requirements of the CCR Rule, including continued groundwater monitoring, evaluation of the groundwater data, and selection and implementation of a remedy.

iii. There are more options that could be considered than those that were presented.

RESPONSE: The remedial alternatives presented in the CMA were developed by combining remedial technologies that are appropriate for the Site. While additional remedial alternatives are possible for the facility, the assembled list includes those that are considered most viable to address groundwater impacts.

iv. In the CMA options that include water treatment, what is the treatment?

RESPONSE: The water treatment method contemplated for Alternatives 2 and 4 is reverse osmosis (RO).

v. Complete removal of the AGREMAXTM Staging Area should be considered.

RESPONSE: By moving the AGREMAXTM and placing a liner, then moving the AGREMAXTM back, the remedy is essentially equivalent to removal because it eliminates AGREMAXTM contact with the ground.

vi. The CMA states that vertical infiltration would be virtually eliminated following installation of the Staging Area liner system. What is meant by "virtually" eliminated? Is it eliminated or not?

<u>RESPONSE:</u> The synthetic liner system included with Alternative 1 would reduce the infiltration in some areas from as high as 80+ inches per year to 0.002 inches per year based on standard engineering calculations.

vii. The CMA does not address fugitive dust associated with the presented remedies. Particularly, Option 1 which involve material movement may result in generation of fugitive dust.



RESPONSE: As required by the CCR Rule, all material handling activities are conducted in accordance with the existing AES-PR AGREMAX™ Dust Control Plan that identifies methods to prevent, reduce, and mitigate fugitive dust.

viii. The CMA does not address how contaminated stormwater runoff will be treated.

RESPONSE: Site stormwater that comes into contact with the AGREMAXTM Staging Area in Alternative 1 is collected in stormwater collection drains which will be constructed above the AGREMAXTM liner system that will direct stormwater from the AGREMAXTM Staging Area to the existing on-site lined coal pile runoff pond or lined cooling tower makeup water pond. For CMA remedial Alternatives 2 through 5, any contact water (contaminated stormwater runoff) will be directed to the on-site lined coal pile runoff pond and/or lined cooling tower make-up pond in accordance with the AES-PR on-site water management plans which are currently in effect.

ix. The CMA does not address a situation in which level of constituents increase or new constituents are found above groundwater protection standards in the future.

RESPONSE: Each alternative includes provisions for post-implementation remedy performance monitoring consistent with 40 CFR § 257.98(a), which would include addressing the detection of new constituents. Should a selected remedy not achieve performance goals, remedy enhancements or modifications will be implemented consistent with 40 CFR § 257.98(b).

- x. AES-PR received some comments related to the effectiveness of the presented remedies which did not provide technical justification or explanation. As such, those are not addressed in this document as the CMA documents and explains the effectiveness of the remedies.
- b. **Implementation.** AES-PR received comments and questions related to implementation of the remedies as follows:
 - i. What is the plan with the stormwater that comes in contact with the AGREMAX[™] and coal piles?

RESPONSE: Site stormwater that comes into contact with the AGREMAXTM Staging Area in Alternative 1 is collected in stormwater collection drains which will be constructed above the AGREMAXTM liner system that will direct stormwater from the AGREMAXTM Staging Area to the existing on-site lined runoff ponds. For CMA remedial Alternatives 2 through 5, stormwater infiltration within the AGREMAXTM Staging Area would be collected in the on-site groundwater remedial system. For Alternatives 2 and 4, water will then be directed to the existing on-site treatment system located at the AES-PR facility. For Alternatives 3 and 5, water will then be recirculated to the on-site lined coal pile runoff pond and/or lined cooling water



make-up pond or used for dust suppression and hydration of AGREMAX™ within the Staging Area.

AES-PR's water management practice includes runoff being directed to and collected in either the lined 2-million-gallon stormwater retention pond or the lined coal pile runoff pond which stores water for use in the cooling tower, where much of the water is evaporated. A water treatment system, centrally located on-site adjacent to the plant, treats water from the 2-million-gallon stormwater retention pond intended for use for non-process water needs at the Site.

ii. Is the pile to be completely removed?

RESPONSE: The alternatives identified in the CMA do not require complete removal of the AGREMAXTM in the AGREMAXTM Staging Area. Rather, for Alternative 1, liner installation would be completed in two phases. Phase 1 would involve lining one half of the Staging Area and would necessitate removal of all AGREMAXTM from that half of the area while AGREMAXTM would remain on the Phase 2 area. During Phase 2 liner installation, the remaining AGREMAXTM would be moved to the completed/lined Phase 1 area. The liner would be installed within the current footprint of the Staging Area. Following liner installation, AGREMAXTM could be managed anywhere within the lined Staging Area.

iii. The contaminated soil must be removed.

RESPONSE: During installation of the liner system, soils will be evaluated to determine if they would require removal.

iv. How specifically would the pile be moved in Option 1?

RESPONSE: For Alternative 1, liner installation would be completed in two phases. Phase 1 would involve lining one half of the Staging Area and would necessitate removal of all AGREMAXTM from that half of the area while AGREMAXTM would remain on the Phase 2 area. During Phase 2 liner installation, the remaining AGREMAXTM would be moved to the completed/lined Phase 1 area. The liner would be installed within the current footprint of the Staging Area. Following liner installation, AGREMAXTM could be managed anywhere within the lined Staging Area.

v. Would the liner in Option 1 be below only newly generated AGREMAXTM or also under existing AGREMAXTM

RESPONSE: In CMA remedial Alternative 1, the AGREMAXTM liner system installation is planned to be constructed such that the liner system will be in direct contact with the natural ground below the Staging Area. There would be no AGREMAXTM in direct contact with the natural ground after the installation of the Staging Area liner system.



- c. **Groundwater.** AES-PR received comments and questions related to groundwater and subsurface behavior and characteristics as follows:
 - i. The constituents were detected on wells 3, 4 and 5 but were not detected in the perimeter wells 200 feet downgradient? Where did the constituents go between those two groups of wells?

RESPONSE: The change in concentration between wells 3, 4, and 5 and the downgradient perimeter wells is likely through processes of natural attenuation. The natural attenuation processes include dispersion, dilution, precipitation, and/or sorption. Dispersion and dilution are solute transport processes that result in mixing between impacted and unimpacted groundwater. The extent of dispersion and dilution depends on the degrees of aquifer heterogeneity of hydraulic properties and transport time scale. Precipitation is a reaction process that transforms dissolved constituents into a solid form, which can be subsequently removed from the aqueous phase. The rate and extent of precipitation depends on both chemical concentrations and local biogeochemical conditions. Sorption can be defined as the partitioning of a constituent from the aqueous phase to the surface of an aquifer solid phase. The rate of sorption of aquifer solids for a constituent depends on its relative affinity to the aqueous phase versus to the aquifer solid surface. If the surface of aquifer solids has a high capacity for partitioning of a constituent, a significant portion of the constituent mass in the aguifer is expected to be primarily stored in the aguifer solid phase, thereby reducing the concentration of the constituent in the aqueous phase.

ii. Page 5 of the CMA states that there is an impermeable clay layer. Is this a natural layer or is it man made? Does the layer continue outside the facility? Have there been wells installed to reach below the impermeable clay layer to see if the constituents have passed through?

RESPONSE: The clay layer encountered at approximately 25 feet below ground surface is a natural feature and has been observed to be laterally extensive. The clay layer creates a natural boundary for the downward movement of groundwater and was not penetrated to install wells thereby avoiding cross-contamination.

iii. What is MNA and how does it work? What does it mean that passive treatment of groundwater will happen naturally through geochemical processes? Will contaminant disappear or be transported to other areas?

RESPONSE: As stated in Section 4.3.1 of the CMA report, the United States Environmental Protection Agency (USEPA) defines monitored natural attenuation (MNA) as "the reliance on natural attenuation processes to achieve site-specific remediation objectives within a time frame that is reasonable compared to that offered by other more active methods." The "natural attenuation processes" that are at work in such a remediation approach include a variety of physical, chemical, or biological processes that, under favorable conditions, act without human intervention



to reduce the mass, toxicity, mobility, volume, or concentration of contaminants in soil or groundwater. These in-situ processes may include biodegradation; dispersion; dilution; sorption; volatilization; radioactive decay; and chemical or biological stabilization, transformation, or destruction of contaminants depending on the constituent (USEPA, 2015). Through the natural attenuation methods appropriate for inorganics (dispersion, dilution, and/or sorption), the concentration of Appendix IV constituents would decrease over time. The extent of contamination and the natural attenuation that is occurring has been determined as documented in the report "Use of Monitored Natural Attenuation for Inorganic Contaminants in Groundwater at Superfund Sites" (USEPA, 2015). Transportation of contaminants in groundwater to other areas has been shown not to be occurring and is not expected in the future since the predominant groundwater flow direction in the upper water bearing unit is to the south, towards Las Mareas Harbor. Future releases of constituents to groundwater from the AES-PR facility will be confined to the area of the groundwater at the plant and downgradient.

iv. What effect can geological and natural events have in the movement of the constituents through the aquifer?

RESPONSE: Dramatic changes in geologic conditions (such as a landslide, river channel avulsion, or seismic activity events) can alter the movement of groundwater. However, given the generation facility's location on a coastal plain with low topographic relief, dramatic changes in geologic conditions that would alter groundwater flow through the unconsolidated overburden are unlikely. Natural weather events, such as a period of heavy rainfall, can also alter the movement of constituents through the aquifer, although these events are temporary and do not typically create long-term change.

II. Risk Assessment

a. General.

i. The CMA indicates that there is no exposure to CCR derived constituents detected in groundwater at the Site. This seems contradictory to the identified SSLs above GWPS for lithium, molybdenum, and selenium in groundwater.

RESPONSE: The statistically significant levels (SSL) represent groundwater concentrations of these constituents that are above the Groundwater Protection Standards (GWPS).

Exposure refers to whether anyone is directly contacting groundwater via drinking water at the facility. Groundwater is not used as drinking water at the facility or downgradient of the facility. Results of the Nature and Extent evaluation indicate that SSLs do not extend beyond the AES-PR property.



Although there are SSLs, and some groundwater concentrations are above GWPS, no one is using the groundwater, no one is drinking the groundwater, there is no exposure to the groundwater; therefore, there is no risk posed by the SSLs in groundwater.

ii. The CMA indicates that there is no impact on drinking water and no evidence of impact to human health or the environment. How can this be the case when constituents are above relevant standards?

RESPONSE: The CMA indicates that there is no impact on groundwater used as drinking water. While there are SSL conditions in groundwater, there are no on-site or downgradient of users of groundwater as drinking water. Results of the Nature and Extent evaluation indicate that SSLs do not extend beyond the AES-PR property.

Las Mareas Harbor is the nearest surface water body where groundwater could discharge. It is located approximately 1/3 mile from the AES-PR property line. Results of the Nature and Extent evaluation indicate that SSLs do not extend beyond the AES-PR property. However, Las Mareas Harbor water was sampled, and the results are consistent with seawater across the globe. Thus, there is no evidence of impact on the harbor and, thus no impact on recreational users of the harbor or on the ecology of the harbor.

Where there is no exposure, there is no risk.

- b. Wildlife. AES-PR received comments related to wildlife concerns as follows:
 - i. Crabs and other wild and marine life are exposed to the toxic components in the groundwater which will affect those who consume them and the economy of those who sell them. This could have adverse impacts in public health and the local economy and has not been considered in the CMA or elsewhere.

RESPONSE: Wildlife are not directly exposed to groundwater; their exposure to constituents in groundwater can occur via discharge of groundwater to surface water. Las Mareas Harbor is the nearest surface water body where groundwater could discharge and is located approximately 1/3 mile from the AES-PR property line. Results of the Nature and Extent evaluation indicate that SSLs do not extend beyond the AES-PR property. However, Las Mareas Harbor water was sampled, and the results are consistent with seawater across the globe. Thus, there is no evidence of impact on the harbor and, thus no impact on recreational users of the harbor or on the ecology of the harbor.

ii. MNA dilutes and/or disperses the contaminants into the bay downgradient of the pile which could affect wildlife.



RESPONSE: Las Mareas Harbor is the nearest surface water body where groundwater could discharge and is located approximately 1/3 mile from the AES-PR property line. Results of the Nature and Extent evaluation indicate that SSLs do not extend beyond the AES-PR property. However, Las Mareas Harbor water was sampled, and the results are consistent with seawater across the globe. Thus, there is no evidence of impact on the harbor and, thus no impact on recreational users of the harbor or on the ecology of the harbor.

iii. Aquatic life, birds and the crustaceans in the wetland south of the facility may be impacted. This could have adverse impacts in public health and the local economy and has not been considered in the CMA or elsewhere.

RESPONSE: Although wildlife are not exposed to groundwater directly, AES-PR took the conservative approach of identifying ecological screening levels for a marine environment (see Table 3 of Appendix B of the CMA), and comparing the groundwater data to these screening levels (see Tables 8 and 9 of Appendix B of the CMA). Only selenium concentrations in one well (MW-3) are above the marine screening level. The results for the Las Mareas Harbor surface water sample are below screening levels for selenium (see Table 10 of Appendix B of the CMA), and the selenium concentration in the harbor are consistent with global seawater (see Table 11 of Appendix B of the CMA).

- c. **Studies.** AES-PR received comments related to studies and information as follows:
 - i. The sample of the Las Mareas Harbor was taken in deep waters instead of shallow waters close to land.

RESPONSE: The sample was collected to be representative of the dynamic conditions of a tidal inlet.

ii. Drinking water well data was taken from a 2002 survey, and there may be new drinking water wells south of the AES-PR property. A new survey should be conducted.

RESPONSE: The Nature and Extent investigation has demonstrated that there is no impact to off-site groundwater. As such, there is no requirement under the CCR Rule to perform any additional studies. In addition, off-site shallow groundwater beyond the southern property line is saline water, not suitable for drinking water use.

- **III. Nature and Extent Evaluation.** AES-PR received comments and questions related to the Nature and Extent Evaluation as follows:
 - a. Sampling and monitoring on the wetlands south of the facility should be conducted and added to the nature and extent evaluation, including sediment, surface water, and groundwater.



RESPONSE: Groundwater sampling results from monitoring wells installed at the facility property boundary (TW-104 through TW-109) confirm that concentrations of lithium, molybdenum, or selenium do not exceed GWPS at the property boundary. Given the limited extent of groundwater contamination, monitoring wetlands south of the facility is not required or necessary.

b. Sampling of nearby communities should take place and be added to the Nature and Extent evaluation.

RESPONSE: As stated in Section 3 of the CMA report, no groundwater receptors were identified in the vicinity of the facility and the extent of Appendix IV CCR constituent contamination has been determined.

c. Sampling in the shallow area of Las Mareas Harbor is needed. The CMA indicates that contaminated groundwater discharges into the Harbor in the low tide area.

RESPONSE: The sample was collected to be representative of the dynamic conditions of a tidal inlet. The results are provided on Tables 10 and 11 of Appendix B of the CMA. All results are consistent with global data for seawater.

d. On Page 100-110, the report indicates that TW-C well variations in lithium levels were detected above the drinking water levels in the southwest border of the facility. There is no explanation given for this data.

RESPONSE: A single lithium result from TW-C was detected above the drinking water screening level. Subsequent sampling did not confirm this concentration.

e. AES-PR states that the impact of the staging area is limit. What is meant by limited and how has this been confirmed?

RESPONSE: The impact of the Staging Area on groundwater quality is limited as evidenced by the fact that groundwater concentrations above GWPS are not observed at the property boundary (i.e., the results of the Nature and Extent evaluation). See the discussion in Section 2.5 of the CMA.

f. AES-PR received some comments related to the nature and extent evaluation which did not provide technical justification or explanation. As such, those are not addressed in this document.



DNER Comments and Recommendations

A. Comments

PR-DNER Comment III-A-1: ("Groundwater Characterization Report USEPA Coal Combustion Residuals Rule AES Puerto Rico LP, Guayama, Puerto Rico (September 2019))

a. Even though, a groundwater characterization report was included in the CMA-AESPR, no sampling was performed of the background and up-gradient wells (MW-1 and MW-2) to compare the concentration detected in the monitoring wells (TW-101, TW-104, TW-105, TW-106, TW-107, TW-108, and TW-109) in the property boundary and within 200 from the three (3) monitoring wells located hydraulically down gradient of the CCR Staging Area. This will allow to verify whether or not the concentrations of **Li, Mo, and Se** detected in wells TW-101, TW-104, TW-105, TW-106, TW-107, TW-108, and TW-109, above the MDL but below the GWPS, were equal or below to the background level.

RESPONSE: Table 1 in the CMA report documents MW-1 and MW-2 groundwater results obtained from 10 monitoring events between August 2017 and October 2018. The site-specific background levels for lithium, molybdenum, and selenium are 0.005 mg/L, 0.015 mg/L, and 0.02271 mg/L, respectively, as documented in the report titled "2019 CCR Annual Groundwater Monitoring and Corrective Action Report, AES Puerto Rico LP, Guayama, Puerto Rico." The established background levels were used to establish the site-specific GWPS. As described in Page 7 of the CMA report – "Because the GWPS is the higher of the drinking water concentration and background concentration, and background concentrations are specific to each ash management area, the GWPS are considered to be site-specific." Lithium, molybdenum, and selenium concentrations observed at the monitoring wells, TW-101 and TW-104 through TW-109, are all below the established background levels except that the lithium concentration at TW-106 is between the GWPS and the background level.

It should be noted that, per USEPA's requirements for the Natural and Extent (N&E) Investigation, there is no provision requiring background wells to be sampled during the N&E investigation nor do concentrations observed at TW wells need to be compared with the background levels.

b. The groundwater characterization report contains limited information on the geological and hydrogeological conditions of the site to and the vertical and horizontal extension of the contamination beneath the CCR staging area. In addition, does not contain any technical information or discussion on the monitored natural attenuation (MNA) mechanism being proposed to be implemented in all of the alternatives for the groundwater below the CCR staging area, based upon the hydrogeological conditions beneath the site, including information to be used to determine MNA rate or the viability of this mechanism based upon the aquifer characteristics.



RESPONSE: The general groundwater flow direction beneath the AGREMAXTM Staging Area is shown in Figure 1-2 of the CMA report. The horizontal extent of the CCR constituents that exceed the site-specific GWPS has been determined, as shown in Figure 2-1 of the CMA report. Although the Site is close to the coast, the site water levels have not been found to be affected by tidal fluctuation. It is expected that the shallow groundwater flow will remain shallow before it reaches the intertidal zone, as shown in Figure A-3 in Appendix B of the CMA report. In addition, as described in Section 4.1 of the CMA report, the impacted shallow aquifer has been bounded by a layer of stiff clay of high plasticity. Therefore, the impacts of the Staging Area will remain in the shallow aquifer.

A geochemical evaluation was also conducted to assess site-specific natural attenuation mechanisms that contribute to limited transport of lithium, molybdenum, and selenium observed near the southern property boundary. The results indicate that precipitation is likely the key mechanism responsible for limiting the transport of molybdenum and selenium. The primary natural attenuation mechanism for lithium is likely adsorption by clayey solids in the shallow impacted aquifer. Vegetation between the AGREMAXTM Staging Area and the southern property boundary may also intercept and remove soluble metals in shallow groundwater. More details of this MNA evaluation are documented in **Attachment 1**.

<u>PR-DNER Comment III-A-2:</u> The CMA-AESPR does not establishes clear clean-up objectives, such as reducing the migration of contaminants into the groundwater and restoring groundwater concentration of **Li, Mo and Se** to background levels.

RESPONSE: In accordance with 40 CFR § 257.97(b)(2), the cleanup objective addressed by the CMA is the reduction of lithium, molybdenum, and/or selenium in groundwater to concentrations less than the GWPSs at the AGREMAXTM Staging Area boundary. Groundwater monitoring results indicate that that the GWPS has already been achieved through processes of natural attenuation at the facility property boundary, located less than 200 feet downgradient from the Staging Area.

<u>PR-DNER Comment III-A-3:</u> The CMA-AESPR does not contain a Sampling and Analysis Plan (SAP) and a Quality Assurance Project Plan (QAPP) with the type and frequency sampling required to be performed during and after the implementation of the selected remedy to verify its effectiveness; nor does each alternative contain information on whether or not confirmatory sampling is being contemplated to evaluated effectiveness.

RESPONSE: Sampling and Analysis Plans (SAPs) and Quality Assurance Project Plans (QAPPs) to accompany the CMA document are not required by the CCR Rule (40 CFR § 257.96). These documents would be prepared following remedy selection. Each corrective measure alternative includes a period of post-implementation performance monitoring to confirm the selected remedy is effective per 40 CFR § 257.98(b).

<u>PR-DNER Comment III-A-4:</u> The CMA-AESPR does not contain information in any of the alternatives on what course of action will be implemented in the event of failure of the alternative



to achieve a clean-up objectives, which must ensure the reduction in mobility and impact of the contaminants to the groundwater. In addition, does not included a reporting schedule, including the Federal and State/Local Agency that will be receiving any report generated from the implementation, nor does it includes the public participation procedures that will be implemented during the remediation process.

RESPONSE: Each corrective measure alternative includes provisions for performance monitoring to confirm the selected remedy is effective and cleanup objectives will be achieved long-term. In the event that post-implementation performance monitoring indicates the remedy is not effective, modifications to the remedial approach will be implemented per 40 CFR § 257.98(b).

PR-DNER Comment III-A-5: (Alternative 1 – Synthetic Liner and MNA)

a. In addition to containing limited information or discussion on the MNA mechanism being proposed as part of this mechanism, this alternative does not contain information on the mechanism that will be used to determine the effectiveness of this alternative, such as sampling for the constituents of interest (**Li, Mo, and Se**) and the MNA parameters (e.g. dissolved oxygen, pH, reduction-oxidation potential, temperature) during and after the implementation of the remedy. For this purpose a SAP and QAPP is required.

RESPONSE: For Alternative 1, post-implementation monitoring would begin following installation of the synthetic liner system. As part of the post-implementation monitoring, groundwater samples would be collected for lithium, molybdenum, and/or selenium laboratory analysis. MNA parameters including temperature, pH, dissolved oxygen, conductivity, and oxidation-reduction potential would be measured and recorded at the time of sampling. A SAP and QAPP would be prepared to address these post-implementation monitoring activities following remedy selection.

b. This alternative also, does not contain any option of groundwater pumping and treatment (as other alternatives) to achieve background levels, but simply establishes MNA to remedy current conditions of the groundwater, which not necessary will prevent the constituents detected (**Li, Mo, and Se**) from migrating outside of the property boundary.

RESPONSE: Alternative 1 includes the installation of a synthetic liner system which would dramatically reduce the infiltration rate of precipitation to groundwater. The liner would prevent the future potential release of Appendix IV constituents to groundwater during continued use of the Staging Area. Over time, processes of MNA would reduce the residual concentrations of lithium, molybdenum, and/or selenium in groundwater at the Staging Area. Groundwater monitoring results indicate that that the GWPS has already been achieved through processes of natural attenuation at the facility property boundary, located less than 200 feet downgradient from the Staging Area. Alternative 1 is fully compliant with the CCR Rule and meets the requirements specified under 40 CFR § 257.97.

c. The alternative does not contain information on the specifications of the composite/synthetic system (geosynthetic clay Liner with geomembrane, a geocomposite



drainage layer, protective layer, and dye liner) being proposed to be installed as the capping system such as hydraulic conductivity. This situation limits the evaluation of the alternative because there is not detail information to show effectiveness, protectiveness, and certainty of success of this alternative to reduce the existing impact to the groundwater (40 CFR § 257.97 (c)).

RESPONSE: The use of a 60-mil HDPE geosynthetic membrane liner in the AGREMAXTM liner system has an industry performance standard for vertical permeability which is less than 1×10^{-7} cm/sec (and based on industry standards is rated for vertical permeabilities below 1×10^{-9} cm/sec). The 60-mil HDPE flexible membrane liner (FML) will be installed in accordance with the project QA/QC and construction quality assurance plans which include industry standard material manufacturing and field placement requirements to ensure that the quality and integrity of the FML is maintained and ensured.

d. There is no information on the long-term maintenance of the composite/synthetic system and on the preventive procedures that will be implemented to prevent any damage to the system due to the operation of heavy machinery over and around the pile of the CCR staging area during regular operations at the site.

RESPONSE: The protective layer and dye layer to be installed above the AGREMAX[™] liner system will provide permanent protection of the liner system. The dye layer will serve as a warning layer to prevent further vertical excavation into the protective layer and the underlying liner system.

AGREMAXTM Staging Area material management and handling plans including operator training will be observed to ensure that operators will be informed regarding protection of the liner system and the lower vertical limits of AGREMAXTM.

e. Even though, this alternative may control the source of releases to reduce further release of the constituents in appendix IV (40 CFR § 257.97 (b) (3)) into the groundwater, it does not remove the constituents present in the groundwater to ensure compliance with 40 CFR § 257.97 (b) (4).

RESPONSE: The synthetic liner would prevent the future release of CCR constituents to groundwater during continued use of the Staging Area. While the liner addresses the source by limiting the infiltration of precipitation into and through the CCR, MNA will reduce concentrations of lithium, molybdenum, and selenium in groundwater. MNA is a viable remedial technology recognized by both state and federal regulators that is applicable to inorganic compounds in groundwater.

f. In this alternative there is no specific information on what AESPR will be doing during the placement of the composite/synthetic system, with the CCR needed to be removed during Phase 1 of installation. Specifically, whether or not the CCR removed will be shipped and disposed of outside of PR, or any other procedure, that ensures protection to human health and the environment as per 40 CFR § 257.97 (b)(1), and compliance with local laws and



regulations. In addition, it does not indicate the measures that will implemented for dust control.

RESPONSE: AES-PR is reducing on-site CCR inventory by disposing of CCR outside of Puerto Rico, in compliance with Puerto Rico law. The diminished volume will permit for the installation of the liner in two phases, such that the liner is installed piecemeal in areas cleared of CCR. All material handling activities are conducted in accordance with the existing AES-PR AGREMAX™ Dust Control Plan that identifies methods to prevent, reduce, and mitigate fugitive dust.

<u>PR-DNER Comment III-A-6:</u> (Alternative 2 – Hydraulic Containment via Groundwater Pumping with Treatment)

a. This alternative does not contemplate a Synthetic Liner to prevent further release of; or the construction of the barrier wall (as a redundant method) to prevent the migration of any of the detected constituent of appendix IV (40 CFR § 257.97 (b) (3)) into the groundwater in order to comply with 40 CFR § 257.97; but relies only in hydraulic containment (continuous pumping) to control further migration of the contaminants outside the property boundaries, which does not reduce further release of the constituents.

RESPONSE: As stated in Section 5.2.2.1 of the CMA, Alternative 2 is considered less favorable relative to Balancing Criteria 2(i), "the extent to which containment practices will reduce further releases," since this alternative relies on groundwater pumping only. Groundwater modeling demonstrates that a hydraulic containment system would be effective at controlling further migration of Appendix IV constituents beyond the Staging Area boundary. Alternative 2 meets the five Threshold Criteria listed under 40 CFR § 257.97(b) even though it is considered less favorable when compared to other alternatives.

b. In addition, in the description of this alternative there is no technical information or calculations to allow the reviewer [to] assess whether or not this alternative complies with the criteria in 40 CFR § 257.97 (c).

RESPONSE: The balancing criteria listed under 40 CFR § 257.97(c) are discussed in Section 5 of the CMA report. Groundwater flow modeling and calculations were completed to support the discussion provided in Section 5.

c. This alternative does not provide more information to show its effectiveness to control the source(s) of releases in order to reduce or eliminate, to the maximum extent possible, further releases of constituents in appendix IV of the 40 CFR § 257 into the groundwater.

<u>RESPONSE</u>: Groundwater flow modeling completed as part of the CMA demonstrated that groundwater pumping described for Alternative 2 would be effective at hydraulically containing Appendix IV constituents within the Staging Area boundaries.



d. In addition to containing limited information or discussion on the MNA mechanism being proposed as part of this mechanism, this alternative does not contain information on the mechanism that will be used to determine the effectiveness of this alternative, such as sampling for the constituents of interest (**Li, Mo, and Se**) and the MNA parameters (e.g. dissolved oxygen, pH, reduction-oxidation potential, temperature) during and after the implementation of the remedy. For this purpose a SAP and QAPP is required.

RESPONSE: For Alternative 2, post-implementation monitoring would begin following installation and start-up of the hydraulic containment system. As part of the post implementation monitoring, groundwater samples would be collected for lithium, molybdenum, and/or selenium laboratory analysis. MNA parameters including temperature, pH, dissolved oxygen, conductivity, and oxidation-reduction potential would be measured and recorded at the time of sampling. A SAP and QAPP would be prepared to address these post-implementation monitoring activities following remedy selection.

e. In the description of the alternative there is no information on the final destination of the pumped and treated water. In particular, if they will be accumulated in the CCR staging and coal storage areas run-off collection ponds, or they will be discharge into the PRASA system or injected underground, which will require a particular permit and water quality. This needs to be explained in the CMA-AESPR. If the treated water will be accumulated in the CCR staging and coal storage areas run-off collection ponds, data showing that the additional water volume in these ponds will not exceed their capacity is required in the document.

RESPONSE: The pumped and treated water will be discharged to the on-site lined coal pile runoff pond or the lined cooling tower makeup water pond. No water from the AES-PR site is transferred to the PRASA System except for sanitary wastewater from the power plant bathroom facilities. The on-site lined coal-pile runoff pond has adequate excess capacity to handle the additional total volume generated from the groundwater pump and treatment system in Alternative 2 which is estimated at a maximum combined flow rate of 5 gpm (approximately 7,200 gallons/day based on CMA level groundwater flow estimates).

The overall capacity of the lined coal pile runoff pond is approximately 15 million gallons. Under maximum design conditions (the 100-year storm event – approximately 18 inches/24-hr period), the lined coal pile runoff pond will accumulate approximately 11 million gallons, which will leave significant additional capacity for the additional treated water from any water generated from the Alternative 2 groundwater remedy ³.

f. There is no information on the long-term maintenance of pump and treat system, including redundancy in an event or equipment failure, nor on the management of the wastes generated from the reverse osmosis (RO) water treatment system (disposal of spent filters) in compliance with Federal and Local Regulations.

³ Stormwater and on-site pond storage capacities based on engineering studies entitled "Hydrologic/Hydraulic Study, AES Facility – Existing Conditions Evaluation, Guayama Puerto Rico – CES Project No. 11-0034", completed by Caribe Environmental Services, dated April 17, 2012.



RESPONSE: Details regarding hydraulic containment system operation and maintenance requirements would be included in remedy design documents. Water treatment would be performed by the existing on-site water treatment system including RO.

PR-DNER Comment III-A-7: (Alternative 3 – Hydraulic Containment via Pumping with Recirculation)

a. This alternative does not contemplate a Synthetic Liner to prevent further release of; or the construction of the barrier wall to prevent the migration of any of the detected constituent of appendix IV (40 CFR § 257.97 (b) (3)) into the groundwater; but relies only in hydraulic containment to control further migration of the contaminants outside the property boundaries, which may not prevent the further release of the constituents. This is not consistent with the requirements of 40 CFR § 257.97 (b) (3).

RESPONSE: As stated in Section 5.2.2.1 of the CMA, Alternative 3 is considered less favorable relative to Balancing Criteria 2(i), "the extent to which containment practices will reduce further releases," since this remedy is limited to groundwater pumping. Groundwater modeling demonstrates that a hydraulic containment system would be effective at controlling further migration of Appendix IV constituents beyond the Staging Area boundary. Alternative 3 meets the five Threshold Criteria listed under 40 CFR § 257.97(b) even though it is considered less favorable when compared to other alternatives.

b. The alternative does not contain comprehensive information on how the hydraulic containment will control the release from the source (i.e., CCR in the staging area) in the short- and long-term, if the groundwater pumped is not being treated and is proposed to be sprayed over the CCR pile, which will not have a no synthetic liner in place to prevent further release. In other words, it does not provide the necessary information to show its effectiveness to control the source(s) of releases in order to reduce or eliminate, to the maximum extent possible, further releases of constituents in appendix IV of the 40 CFR § 257 into the groundwater.

RESPONSE: Groundwater flow modeling completed as part of the CMA demonstrated that groundwater pumping described for Alternative 3 would be effective at hydraulically containing Appendix IV constituents within the Staging Area boundaries. Groundwater that is pumped and sprayed over the AGREMAXTM area would be hydraulically contained within the Staging Area boundaries. Groundwater flowing downgradient from the Staging Area will be captured by pumping wells positioned along the southern boundary of the Staging Area. With the hydraulic containment system operating, groundwater passing beneath the Staging Area will no longer migrate beyond the southern (downgradient) boundary of the Staging Area.

c. In addition, in the description of this alternative there is no technical information or calculations to allow the reviewer [to] assess whether or not this alternative complies with the criteria in 40 CFR § 257.97 (c).



RESPONSE: The balancing criteria listed under 40 CFR § 257.97(c) are discussed in Section 5 of the CMA report. Groundwater flow modeling and calculations were completed to support the discussion provided in Section 5.

d. In addition to containing limited information or discussion on the MNA mechanism being proposed as part of this mechanism, this alternative does not contain information on the mechanism that will be used to determine the effectiveness of this alternative, such as sampling for the constituents of interest (Li, Mo, and Se) and the MNA parameters (e.g. dissolved oxygen, pH, reduction-oxidation potential, temperature) during and after the implementation of the remedy. For this purpose a SAP and QAPP is required.

RESPONSE: For Alternative 3, post-implementation monitoring would begin following installation and start-up of the hydraulic containment system. As part of the post-implementation monitoring, groundwater samples would be collected for lithium, molybdenum, and/or selenium laboratory analysis. MNA parameters including temperature, pH, dissolved oxygen, conductivity, and oxidation-reduction potential would be measured and recorded at the time of sampling. A SAP and QAPP would be prepared to address these post-implementation monitoring activities following remedy selection.

e. Since this alternative relies on accumulating the pumped water in the CCR staging and coal storage areas run-off collection ponds, it does not present data to show that the additional water volume in these ponds will not exceed their capacity.

RESPONSE: The on-site lined coal-pile runoff pond has adequate excess capacity to handle the additional water volume associated with the pumped groundwater from CMA Alternative 3. The total volume generated from the groundwater containment system in Alternative 3 is estimated at a maximum combined flow rate of 5 gpm (approximately 7,200 gallons/day based on CMA level groundwater flow estimates).

f. There is no information on the long-term maintenance of pumping system, or any redundancy in the event of equipment failure.

RESPONSE: Details regarding hydraulic containment system operation and maintenance requirements would be included in remedy design documents.

<u>PR-DNER Comment III-A-8:</u> (Alternative 4 – Hydraulic Containment via Groundwater Pumping with Barrier Wall and Treatment)

a. This alternative does not contemplate a Synthetic Liner to prevent further release of the detected constituent of appendix IV (40 CFR § 257.97 (b) (3)) into the groundwater; and relies on the construction of the partial barrier wall and in hydraulic containment to control further migration of the contaminants outside the property boundaries, which may not prevent the further release of the constituents from the source. This is not consistent with the requirements of 40 CFR § 257.97 (b) (3).



RESPONSE: As stated in Section 5.2.2.1 of the CMA, Alternative 4 is considered less favorable relative to Balancing Criteria 2(i), "the extent to which containment practices will reduce further releases," since this alternative uses groundwater pumping with a barrier wall to limit further release of Appendix IV constituents beyond the Staging Area boundary. Groundwater modeling demonstrates that a hydraulic containment system, combined with a barrier wall, would be effective at controlling further migration of Appendix IV constituents beyond the Staging Area boundary. Alternative 4 meets the five Threshold Criteria listed under 40 CFR § 257.97(b) even though it is considered less favorable when compared to other alternatives.

b. In addition, in the description of this alternative there is no technical information or calculations to allow the reviewer [to] assess whether or not this alternative complies with the criteria in 40 CFR § 257.97 (c).

RESPONSE: The balancing criteria listed under 40 CFR § 257.97(c) are discussed in Section 5 of the CMA report. Groundwater flow modeling and calculations were completed to support the discussion provided in Section 5.

c. This alternative does not provide more information to show its effectiveness to control the source(s) of releases in order to reduce or eliminate, to the maximum extent possible, further releases of constituents in appendix IV of the 40 CFR § 257 into the groundwater.

RESPONSE: Groundwater flow modeling completed as part of the CMA demonstrated that groundwater pumping with a barrier wall described for Alternative 4 would be effective at hydraulically containing Appendix IV constituents within the Staging Area boundaries.

d. In addition to containing limited information or discussion on the MNA mechanism being proposed as part of this mechanism, this alternative does not contain information on the mechanism that will be used to determine the effectiveness of this alternative, such as sampling for the constituents of interest (**Li, Mo, and Se**) and the MNA parameters (e.g. dissolved oxygen, pH, reduction-oxidation potential, temperature) during and after the implementation of the remedy. For this purpose a SAP and QAPP is required.

RESPONSE: For Alternative 4, post-implementation monitoring would begin following installation of the barrier wall and hydraulic containment system, and start-up of the pumping wells. As part of the post-implementation monitoring, groundwater samples would be collected for lithium, molybdenum, and/or selenium laboratory analysis. MNA parameters including temperature, pH, dissolved oxygen, conductivity, and oxidation-reduction potential would be measured and recorded at the time of sampling. A SAP and QAPP would be prepared following remedy selection.

e. In the description of the alternative there is no information on the final destination of the pumped and treated water. In particular, if they will be accumulated in the CCR staging and coal storage areas run-off collection ponds, or they will be discharge into the PRASA system or injected underground, which will require a particular permit and water quality. This needs



to be explained in the CMA-AESPR. If the treated water will be accumulated in the CCR staging and coal storage areas run-off collection ponds, data showing that the additional water volume in these ponds will not exceed their capacity will be required in the document.

RESPONSE: The pumped and treated water will be discharged to the on-site lined coal pile runoff pond or the lined cooling tower make up water pond. No water from the AES-PR site is transferred to the PRASA System except for sanitary wastewater from the power plant bathroom facilities. The on-site lined coal-pile run off pond has adequate excess capacity to handle the additional total volume generated from the groundwater pump and treatment system in Alternative 4 which is estimated at a maximum combined flow rate of 5 gpm (approximately 7,200 gallons/day based on CMA level groundwater flow estimates).

The overall capacity of the lined coal pile runoff pond is approximately 15 million gallons. Under maximum design conditions (the 100-year storm event - approx. 18 inches/24-hr period), the lined coal pile runoff pond will accumulate approximately 11 million gallons, which will leave significant additional capacity for any water generated from the Alternative 4 groundwater remedy⁴.

f. There is no information on the long-term maintenance of pump and treat system, including redundancy in an event or equipment failure, nor on the management of the wastes generated from the reverse osmosis (RO) water treatment system (disposal of spent filters) in compliance with Federal and Local Regulations.

RESPONSE: Details regarding hydraulic containment system operation and maintenance requirements would be included in remedy design documents.

<u>PR-DNER Comment III-A-9:</u> (Alternative 5 – Hydraulic Containment via Groundwater Pumping with Barrier Wall and Recirculation)

a. This alternative does not contemplate a Synthetic Liner to prevent further release of the detected constituent of appendix IV (40 CFR § 257.97 (b) (3)) into the groundwater; and relies on the construction of the partial barrier wall and in hydraulic containment to control further migration of the contaminants outside the property boundaries, which may not prevent the further release of the constituents from the source. This is not consistent with the requirements of 40 CFR § 257.97 (b) (3).

RESPONSE: As stated in Section 5.2.2.1 of the CMA, Alternative 5 is considered favorable relative to Balancing Criteria 2(i), "the extent to which containment practices will reduce further releases," since this alternative uses groundwater pumping with a barrier wall to limit further release of Appendix IV constituents beyond the Staging Area boundary.



⁴ Stormwater and on-site pond storage capacities based on engineering studies entitled "Hydrologic/Hydraulic Study, AES Facility – Existing Conditions Evaluation, Guayama Puerto Rico – CES Project No. 11-0034", completed by Caribe Environmental Services, dated April 17, 2012.

Groundwater modeling demonstrates that a hydraulic containment system, combined with a barrier wall, would be effective at controlling further migration of Appendix IV constituents beyond the Staging Area boundary. Alternative 5 meets the five Threshold Criteria listed under 40 CFR § 257.97(b) even though it is considered less favorable when compared to other alternatives.

b. In addition, in the description of this alternative there is no technical information or calculations to allow the reviewer [to] assess whether or not this alternative complies with the criteria in 40 CFR § 257.97 (c).

RESPONSE: The balancing criteria listed under 40 CFR § 257.97(c) are discussed in Section 5 of the CMA report. Groundwater flow modeling and calculations were completed to support the discussion provided in Section 5.

c. This alternative does not provide more information to show its effectiveness to control the source(s) of releases in order to reduce or eliminate, to the maximum extent possible, further releases of constituents in appendix IV of the 40 CFR § 257 into the groundwater.

RESPONSE: Groundwater flow modeling completed as part of the CMA demonstrated that groundwater pumping with a barrier wall described for Alternative 5 would be effective at hydraulically containing Appendix IV constituents within the Staging Area boundaries.

d. The alternative does not contain comprehensive information on how the hydraulic containment will control the release from the source (CCR in the staging area) in the short-and long-term, if the groundwater pumped is not being treated and is proposed to be sprayed over the CCR pile, which will not have a no synthetic liner in place to prevent further release. In other words, it does not provide the necessary information to show its effectiveness to control the source(s) of releases in order to reduce or eliminate, to the maximum extent possible, further releases of constituents in appendix IV of the 40 CFR § 257 into the groundwater.

RESPONSE: Groundwater flow modeling completed as part of the CMA demonstrated that groundwater pumping described for Alternative 5 would be effective at hydraulically containing Appendix IV constituents within the Staging Area boundaries. Groundwater that is pumped and sprayed over the AGREMAXTM area would be hydraulically contained within the Staging Area boundaries. Groundwater flowing downgradient from the Staging Area, including water that re-infiltrates as a result of dust control, will be captured by pumping wells positioned along the southern boundary of the Staging Area. With the hydraulic containment system operating, groundwater passing beneath the Staging Area will no longer migrate beyond the southern (downgradient) boundary of the Staging Area.

e. In addition to containing limited information or discussion on the MNA mechanism being proposed as part of this mechanism, this alternative does not contain information on the mechanism that will be used to determine the effectiveness of this alternative, such as sampling for the constituents of interest (Li, Mo, and Se) and the MNA parameters (e.g.



dissolved oxygen, pH, reduction-oxidation potential, temperature) during and after the implementation of the remedy. For this purpose a SAP and QAPP is required.

RESPONSE: For Alternative 5, post-implementation monitoring would begin following installation of the barrier wall and hydraulic containment system, and start-up of the pumping wells. As part of the post-implementation monitoring, groundwater samples would be collected for lithium, molybdenum, and/or selenium laboratory analysis. MNA parameters including temperature, pH, dissolved oxygen, conductivity, and oxidation-reduction potential would be measured and recorded at the time of sampling. A SAP and QAPP would be prepared following remedy selection.

f. Since this alternative relies on accumulating the pumped water in the CCR staging and coal storage areas run-off collection ponds, it does not present data to show that the additional water volume in these ponds will not exceed their capacity.

RESPONSE: As stated previously, the on-site lined coal-pile run off pond has adequate excess capacity to handle the additional water volume, in this case the pumped groundwater from CMA Alternative 5. The total volume generated from the groundwater containment system with barrier wall in Alternative 5 is estimated at a maximum combined flow rate of 5 gpm (approx. 7,200 gallons/day based on CMA level groundwater flow estimates).

g. There is no information on the long-term maintenance of pumping system, or any redundancy in the event of equipment failure.

RESPONSE: Details regarding hydraulic containment system operation and maintenance requirements would be included in remedy design documents.

B. Recommendations

<u>PR-DNER Recommendation III-B-1:</u> Recommend that any future additional groundwater characterization study ensure the collection of samples from the up-gradient and background monitoring wells (MW-1 and MW-2) concurrently with the down gradient wells for comparison purposes.

RESPONSE: Groundwater characterization has been completed at the site in accordance with 40 CFR § 257.95(g)(1). Currently, under the assessment monitoring program the collection of samples from the upgradient and background monitoring wells (MW-1 and MW-2) is being conducted concurrently with the downgradient wells MW-3, MW-3, and MW-5.

<u>PR-DNER Recommendation III-B-2:</u> For the ultimate selection of a final activity, more comprehensive hydrogeological and geological data is required, as well as the data of any modeling performed to assess the possible alternatives.



RESPONSE: AES-PR anticipates that pre-design investigations and, if necessary, remedy pilot testing would be completed for Alternatives 2 through 5, to refine the design of the final remedy selected during the CMA process. Pre-design investigation data, pilot testing results, and groundwater modeling results would be included with design documents. Regarding Alternative 1, a detailed geochemical evaluation has been conducted to assess potential mechanisms that contribute to natural attenuation of lithium, molybdenum, and selenium (see the response to PR-DNER Comment III-A-1-b). Groundwater monitoring data to be collected in the future will be used to evaluate the long-term stability of the natural attenuation mechanisms that have been identified so far before the selection of the final remedy.

<u>PR-DNER Recommendation III-B-3:</u> The CMA-AESPR need to be revised to establish clear and specific clean-up objectives, including, but not limited to reducing the release of constituents to the groundwater and containing their migration outside the property boundaries, and restoring the groundwater concentrations to background levels.

RESPONSE: As stated in Section 1.3 of the CMA, the selected remedy will be capable of attaining the criteria listed under 40 CFR § 257.97(b), referred to as threshold criteria in the CMA report. The criteria listed under 40 CFR § 257.97(b) are considered the cleanup objectives. Each of the remedial alternatives considered for the CMA can achieve the GWPS at the Staging Area boundary, to satisfy compliance criteria listed under 40 CFR § 257.98(c)(1) and (2).

<u>PR-DNER Recommendation III-B-4:</u> Incorporate SAP containing a QAPP for the sampling required to monitor the effectiveness of any of the alternative selected, including the requirement of confirmatory sampling during the implementation of the remedial alternative to assess effectiveness and to confirm the achievement of the clean-up objectives.

RESPONSE: The CCR Rule does not require SAPs and QAPPs to accompany the CMA document. These documents would be prepared following remedy selection. Each corrective measure alternative includes a period of performance monitoring to confirm the selected remedy is effective.

<u>PR-DNER Recommendation III-B-5:</u> The CMA-AESPR need to established in all of the sections of the proposed alternative, or a separate sections, the course of action and the decision making process to substitute the selected and implemented remedial alternative for other possible remedial alternative in the event of failure to achieve the clean-up goals.

RESPONSE: The CMA considers the anticipated effectiveness of the remedy under 40 CFR § 257.97(c)(2) and overall reliability and ease of implementation under 40 CFR § 257.97(c)(3). Contingency planning would be completed as part of the selected remedy design, such as additional groundwater pumping capacity for the four alternatives that include hydraulic containment if the pumping rate needs to be increased to maintain hydraulic control. In accordance with 40 CFR § 257.98(b), another remedial method would be implemented that would feasibly achieve compliance with the requirement if the five requirements listed under 40 CFR § 257.97(b) are not achieved with the selected remedy.



<u>PR-DNER Recommendation III-B-6:</u> Revise the information for the different remedial alternative in the CMA-AESPR based upon the comments III-A-5 through III-A-9.

RESPONSE: AES-PR considers the CMA report complete and prepared in accordance with 40 CFR § 257.96 and 40 CFR § 257.97. Comments III-A-5 through III-A-9 are addressed above.

<u>PR-DNER Recommendation III-B-7:</u> Any alternative proposed must incorporate the installation of the composite/synthetic system (geosynthetic clay Liner with geomembrane, a geocomposite drainage layer, protective layer, and dye liner) to prevent further release into the groundwater, the treatment of the groundwater until background levels are achieved, and the collection of samples for analysis for the constituents of interest **(Li, Mo, and Se),** during and after the completion of the implementation of the corrective action.

RESPONSE: The CCR Rule allows consideration of multiple remedial technologies to develop viable remedial alternatives that satisfy 40 CFR § 257.97(b). Each alternative presented in the CMA individually meets the requirements of 40 CFR § 257.97(b). Alternative 1 incorporates the installation of the referenced liner and includes MNA, a groundwater remedial technology recognized by EPA. Alternatives 2 and 3 include hydraulic containment and MNA while Alternatives 4 and 5 incorporate the use of a subsurface barrier wall to further impede downgradient migration of groundwater and MNA. Since Alternatives 2 through 5 do not remove the source, a slightly greater residual risk of further release does exist which is why they were ranked less favorable than Alternative 1 in the CMA Section 5.2.1.2 in terms of the likelihood of further release due to CCR. Combinations of the alternatives 1 through 5 would create unnecessary redundancy and complexity because each alternative presented in the CMA individually meets the requirements of 40 CFR § 257.97(b). Each alternative presented in the CMA report includes provisions for post-implementation performance monitoring to confirm the remedy is effective.



USEPA Region 2 Comments

Alternative 1: Synthetic Liner and Monitored Natural Attenuation (MNA)

a. This alternative should include a discussion of which natural attenuation mechanisms (e.g., geochemical precipitation) are occurring at the unit, that could effectively treat the lithium, molybdenum and selenium exceedances in groundwater." Without one or more identified mechanisms, MNA would not be considered an effective remedial response at this site. The specific mechanism(s) are needed in order to evaluate the remedy against criteria such as effectiveness, magnitude of residual risks due to further releases, long-term management required, etc.

RESPONSE: An evaluation was conducted during the Nature and Extent (N&E) investigation to assess site-specific natural attenuation mechanisms that contribute to limited transport of selenium, molybdenum, and lithium observed near the southern property boundary at the site. This evaluation methodology and results are described in **Attachment 1.**

- b. The discussion of the remedy should include a:
 - 1. determination of whether the plume of impacted groundwater is expanding;
 - 2. determination that the expected rate and extent of attenuation within the aquifer is sufficient to achieve GWPS throughout the plume; and
 - 3. determination that immobilized constituents are stable and will not remobilize.

RESPONSE: Section 2.5 of the CMA, "Nature and Extent of Groundwater Impacts," describes the horizontal and vertical limits of Appendix IV constituents in groundwater. The N&E investigation completed in May 2019 demonstrated that the extent of Appendix IV constituents in groundwater that exceed the GWPS (lithium, molybdenum, and selenium) is limited. The concentrations of lithium, molybdenum, and selenium in groundwater samples collected from wells installed 200 feet downgradient from the AGREMAX™ Staging Area along the facility property boundary are well below the GWPS and in most cases the laboratory reporting limits. The observed reduction in concentration indicates that the rate of attenuation within the aquifer is sufficient to achieve GWPS within 200 feet of the source area boundary under current conditions. Alternative 1 includes a synthetic liner to isolate the AGREMAX™ Staging Area from soil and groundwater. With isolation of the source material, the concentrations of lithium, molybdenum, and selenium are expected to attenuate further since the source will be effectively removed.

Based on a geochemical evaluation completed for the Site (see the response to Comment on Alternative 1, Item a - above), geochemical conditions favor selenium and molybdenum being present in the form of precipitates, thereby immobile. For lithium, the primary attenuation mechanisms are sorption to and sequestration into clayey soils. Although the lithium mass adsorbed to and sequestered in aquifer solids may still migrate slowly downgradient after the isolation of the source material, it is expected that, without additional lithium input into the aquifer from the source, lithium concentrations will decline



and meet the GWPS downgradient. The monitoring portion of Alternative 1 will provide results to verify the extent of natural attenuation.

c. This alternative is also missing any discussion of the type of long-term management needed to maintain the integrity of the liner.

RESPONSE: Long-term management of the liner system would likely consist of a combination of operational and administrative controls. Operational controls would include the protective layer and dye layer that would be installed above liner system to maintain the integrity of the liner system. The dye layer will serve as a warning layer to prevent further vertical excavation into the protective layer and underlying liner system.

Administrative controls will include an AGREMAX™ Staging Area material management and handling plan including heavy equipment operator training to ensure that equipment operators will be informed regarding protection of the liner system and the lower vertical limits of AGREMAX™.

Alternative 2: Hydraulic Containment via pumping with treatment

a. This alternative needs a thorough discussion of how it satisfies the requirements for short-and long-term source control.

RESPONSE: The remedy requirements stated under 40 CFR § 257.97(b) do not include provisions for short- and long-term source control. The short- and long-term effectiveness and protectiveness of Alternative 2, relative to the capabilities of the other alternatives, are discussed in Section 5.2.1 (and following subsections) of the CMA. Section 5.2.1 evaluates the short- and long-term capabilities of each alternative using the eight sub-criteria listed in 40 CFR § 257.97(c)(1).

b. The discussion of this alternative should include information necessary to evaluate it according to criteria at 40 CFR § 257.97(c), such as water balance calculations or rates and volume of groundwater flow.

RESPONSE: As described in Section 4.2 of the CMA, the water balance and groundwater flux were evaluated using groundwater flow and transport modeling. The outcome of the groundwater flow and transport modeling was incorporated into the discussion and comparison of each alternative, presented in Sections 4.3.1 through 4.3.5 and Section 5.2 of the CMA.

Alternative 3: Hydraulic Containment via pumping with recirculation

a. This alternative needs a thorough discussion of how it satisfies the requirements for short-and long-term source control.



RESPONSE: The remedy requirements stated under 40 CFR § 257.97(b) do not include provisions for short- and long-term source control. The short- and long-term effectiveness and protectiveness of Alternative 3, relative to the capabilities of the other alternatives, are discussed in Section 5.2.1 (and following subsections) of the CMA. Section 5.2.1 evaluates the short- and long-term capabilities of each alternative using the eight sub-criteria listed in 40 CFR § 257.97(c)(1).

b. The discussion of this alternative should include information necessary to evaluate it according to criteria at 40 CFR § 257.97(c), such as water balance calculations or rates and volume of groundwater flow.

RESPONSE: As described in Section 4.2 of the CMA, the water balance and groundwater flux were evaluated using groundwater flow and transport modeling. The outcome of the groundwater flow and transport modeling was incorporated into the discussion and comparison of each alternative, presented in Sections 4.3.1 through 4.3.5 and Section 5.2 of the CMA.

c. Discharge of pumped water to the coal pile runoff pond or used for AGREMAX™ dust suppression needs to consider and assure compliance with the requirement at 40 CFR § 257.97(b) "to control releases so as to reduce or eliminate them and further releases of constituents in (40 CFR Part 257) appendix IV into the environment to the maximum extent feasible."

RESPONSE: The limited quantities of pumped groundwater derived from the operation of remedial Alternative 3 would be recirculated to the on-site lined coal pile runoff pond and/or lined cooling water make-up pond, or used for dust suppression and hydration of AGREMAX™ within the Staging Area. Management of water in this regard complies with requirements of 40 CFR § 257.97(b) and will be consistent with the AES-PR site permits and related facility operating requirements.

Alternative 4: Hydraulic Containment via pumping with barrier wall and treatment

a. This alternative needs a thorough discussion of how it satisfies the requirements for short-and long-term source control.

RESPONSE: The remedy requirements stated under 40 CFR § 257.97(b) do not include provisions for short- and long-term source control. The short- and long-term effectiveness and protectiveness of Alternative 4, relative to the capabilities of the other alternatives, are discussed in Section 5.2.1 (and following subsections) of the CMA. Section 5.2.1 evaluates the short- and long-term capabilities of each alternative using the eight sub-criteria listed in 40 CFR § 257.97(c)(1).

b. The discussion of this alternative should include information necessary to evaluate it according to criteria at 40 CFR § 257.97(c), such as water balance calculations or rates and volume of groundwater flow.



RESPONSE: As described in Section 4.2 of the CMA, the water balance and groundwater flux were evaluated using groundwater flow and transport modeling. The outcome of the groundwater flow and transport modeling was incorporated into the discussion and comparison of each alternative, presented in Sections 4.3.1 through 4.3.5 and Section 5.2 of the CMA.

Alternative 5: Hydraulic Containment via pumping with barrier wall and recirculation

a. This alternative needs a thorough discussion of how it satisfies the requirements for short-and long-term source control.

RESPONSE: The remedy requirements stated under 40 CFR § 257.97(b) do not include provisions for short- and long-term source control. The short- and long-term effectiveness and protectiveness of Alternative 5, relative to the capabilities of the other alternatives, are discussed in Section 5.2.1 (and following subsections) of the CMA. Section 5.2.1 evaluates the short- and long-term capabilities of each alternative using the eight sub-criteria listed in 40 CFR § 257.97(c)(1).

b. The discussion of this alternative should include information necessary to evaluate this alternative according to criteria at 40 CFR § 257.97(c), such as water balance calculations or rates and volume of groundwater flow.

RESPONSE: As described in Section 4.2 of the CMA, the water balance and groundwater flux were evaluated using groundwater flow and transport modeling. The outcome of the groundwater flow and transport modeling was incorporated into the discussion and comparison of each alternative, presented in Sections 4.3.1 through 4.3.5 and Section 5.2 of the CMA.

c. Discharge of pumped water to the coal pile runoff pond or used for AGREMAX™ dust suppression needs to consider and assure compliance with the requirement at 40 CFR § 257.97(b) "to control releases so as to reduce or eliminate them and further releases of constituents in (40 CFR Part 257) appendix IV into the environment to the maximum extent feasible. "

RESPONSE: The limited quantities of pumped groundwater derived from the operation of remedial Alternative 5 would be recirculated to the on-site lined coal pile runoff pond and/or lined cooling water make-up pond, or used for dust suppression and hydration of AGREMAX™ in the Staging Area. Management of water in this regard complies with requirements of 40 CFR § 257.97(b) and will be consistent with the AES-PR site permits and related facility operating requirements.



EPA has the following additional technical comments:

a. The discussion in section 5.2.2 of the report does not reflect that the source of contamination is the waste in the unit, which is CCR.

RESPONSE: The CMA, including Section 5.2.2, is based on the source of Appendix IV constituents in groundwater exceeding the GWPS being the AGREMAX™ Staging Area. Section 1.1 acknowledges that AGREMAX™ is produced from CCR generated at the power plant.

b. The evaluation in section 5.2.2.2 seems inverted in that alternatives which utilize treatment technologies that remove contaminated material from the environment, in accordance with 40 CFR § 257.97(b) and (c), should be rated more favorably than those that do not.

RESPONSE: Section 5.2.2.2 compares each alternative to 40 CFR § 257.97(c)(2)(ii) which considers "the extent to which treatment technologies may be used." The CMA is based on the understanding that an alternative that relies on fewer treatment technologies to achieve the GWPS is preferable to an alternative that relies on several treatment technologies. For example, Alternative 1 is considered favorable since it only relies on one treatment technology - natural attenuation - to achieve the GWPS. Alternatives 2, 4, and 5 are considered less favorable since these alternatives rely on two or more remedial technologies, with associated complexity. Those complexities include operational, maintenance, and potentially, aboveground treatment technologies and related operation and maintenance issues of the same, in the pursuit of achieving the GWPS. Since greater complexity would be expected to reduce the overall reliability of the remedial alternative, an alternative that includes several treatment technologies is considered less effective at controlling the source to reduce further releases per 40 CFR § 257.97(c)(2). This evaluation approach under 40 CFR 257.97(c)(2)(ii) is consistent with the approach taken under 40 CFR 257.97(c)(3) where a less difficult remedy (difficulty assessed based on complexity of remedy implementation, operational considerations and long-term maintenance and management) is considered more favorable than a more difficult technology.

c. The report needs to include additional technical information about the site in order to adequately assess the alternatives, such as a discussion of how variable hydraulic conductivity and subsurface hydrogeologic features may affect the direction and rate of flow across the site and thereby the effectiveness of proposed remedies.

RESPONSE: The Site geology and hydrogeology is summarized in Section 2.2 of the CMA with additional information, including subsurface boring logs, provided in Appendix A, "Groundwater Characterization Report." The range of hydraulic conductivity values and inferred rate of flow across the site for the upper water bearing unit is provided in Section 2.2. These factors were considered in assessing the effectiveness of the proposed remedies in CMA sections 4.3 and 5.2. The hydrogeologic evaluation completed within the timeframe required under the CCR Rule was adequate to assess the corrective measures alternatives.



d. For each of the alternatives, the discussion lacks estimates of the magnitude of reductions that can be reasonably expected with the proposed technology. Therefore, it is not clear whether each proposed remedy can reliably achieve the groundwater protection standards.

RESPONSE: In accordance with 40 CFR § 257.97(b)(2), each remedial alternative will reduce the concentration of Appendix IV constituents in groundwater to achieve the GWPS at the AGREMAX™ Staging Area boundary. The groundwater remedial technologies included in the CMA pass the threshold criteria found in 40 CFR § 257.97(b) and are recognized by the industry and USEPA as effective technologies which are appropriate for the treatment of metals in groundwater. Remedial technologies or alternatives that would not achieve the GWPS at the unit boundary were not included in the CMA as they could not satisfy 40 CFR § 257.97(b).

e. Any proposed groundwater remedy should take into consideration all media, including air, land and surface water, and the associated discussions of each potential remedy should include these considerations.

RESPONSE: All groundwater remedies (Alternatives 1 through 5) are understood to comply with all environmental requirements associated with fugitive dust control and surface water management, including application permit requirements. Furthermore, once a remedy is selected, AES will obtain all necessary permits and approvals before implementing the remedy and will continue to comply with all applicable environmental requirements.

Finally, in Appendix B: Groundwater Risk Evaluation of the report, the following is stated in the Introduction:

The temporary AGREMAX[™] Storage Area is not a CCR management unit subject to the United States Environmental Protection Agency (USEPA) CCR Rule (USEPA, 2015). However, AES-PR voluntarily monitors groundwater at the temporary AGREMAX[™] Storage Area following the USEPA CCR Rule requirements.

The EPA considers the AGREMAX™ Storage Area to be a CCR landfill as previously communicated in the Agency's correspondence to AES, dated December 22, 2016.

RESPONSE: AES complies with all CCR Rule requirements applicable to a CCR landfill. Certainly, AES developed the Corrective Measures Assessment following the requirements of the CCR Rule for a CCR landfill.

Attachment 1: Additional Technical Analysis - Evaluation of Natural Attenuation Mechanisms for Selenium, Molybdenum, and Lithium in Shallow Groundwater



ATTACHMENT 1

Evaluation of Natural Attenuation Mechanisms for Selenium, Molybdenum, and Lithium in Shallow Groundwater

ATTACHMENT 1

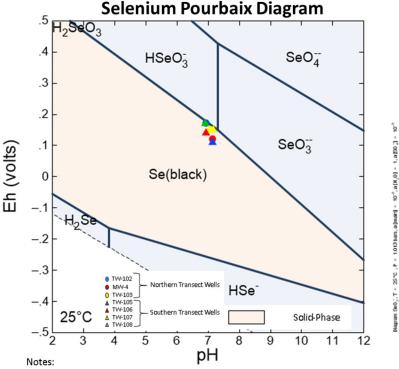
Evaluation of Natural Attenuation Mechanisms for Selenium, Molybdenum, and Lithium in Shallow Groundwater – AES PR Agremax Staging Area

An evaluation was conducted to assess site-specific natural attenuation mechanisms that contribute to limited transport of selenium, molybdenum, and lithium. This evaluation methodology and results are described below.

SELENIUM

A geochemical assessment was performed to determine the preferred state of selenium under site-specific redox and pH conditions. A Pourbaix (or Eh-pH) diagram was developed based on site-specific selenium concentrations and potential selenium speciation across various pH and Eh (electro-potential) conditions. The groundwater pH and redox potential data obtained from TW-102, TW-103, TW-105, TW-106, TW-107, TW-108, and MW-4 were then plotted on the site-specific Pourbaix diagram for selenium.

The results are shown in the figure below. All the pH and Eh data points are within the Se solid phase region, indicating that selenium is preferred to form solid precipitation under the site conditions near the southern property boundary. This assessment demonstrates that selenium precipitation is likely a major attenuation mechanism to remove soluble selenium from groundwater at the Site.

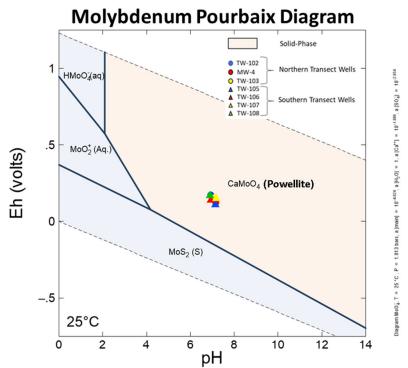


- 1) All field ORP measurements converted to the Standard Hydrogen Electrode (SHE).
- 2) Field pH measurements plotted for accuracy.
- 3) Assumptions: Solute activities = measured concentrations in mols/L
- 4) Modelled system = Se-O-H

MOLYBDENUM

A geochemical assessment was performed to determine the preferred state of molybdenum under site-specific redox and pH conditions. A Pourbaix (or Eh-pH) diagram was developed based on site-specific molybdenum and calcium concentrations and potential molybdenum speciation across various pH and Eh (electro-potential) conditions. The groundwater pH and redox potential data obtained from TW-102, TW-103, TW-105, TW-106, TW-107, TW-108, and MW-4 were then plotted on the site-specific Pourbaix diagram for molybdenum.

The results are shown in the figure below. All the pH and Eh data points are within the CaMoSO₄ (powellite) solid phase region, indicating that molybdenum is preferred to form solid precipitation under the site conditions near the southern property boundary. This assessment demonstrates that molybdenum precipitation is likely a major attenuation mechanism to remove soluble molybdenum from groundwater at the Site.



Notes:

- 1) All field ORP measurements converted to the Standard Hydrogen Electrode (SHE).
- 2) Field pH measurements plotted for accuracy.
- 3) Assumptions: Solute activities = measured concentrations in mols/L
- 4) Analytical concentrations results for TW-103 used to generate stability diagram
- 4) Modelled system = Mo-S-O-H-Ca
- 5) Thermodynamic database used: thermo.com.V8.R6+. Full modified with molybdenum solubility data from Vlek and Lindsay (1977) - Thermodynamic stability and solubility of molybdenum minerals in soils. Soil Science Society of America Journal, 41(1), pp.42-46.

LITHIUM

Lithium Attenuation: No precipitation of lithium is predicted over the range of site specific redox, pH, and chemical conditions. Lithium has been used as a semi-conservative tracer for groundwater flow characterization. It is not likely to be permanently removed from groundwater during its transport at typical groundwater conditions, but it can be subject to sorption to clay minerals or metal oxide minerals to various degrees.^{1,2,3}

Depending on the abundance of clay and oxide minerals, as well as the amount of lithium leached so far relative to the attenuation capacity of aquifer solids, lithium transport may be retarded significantly. Based on the boring logs, clayey sediments are prevailing in the shallow groundwater zone. Based on the monitoring results along the southern property boundary adjacent to the AGREMAX™ temporary staging area, clayey soil in the shallow aquifer has effectively limit lithium migration offsite.

Note that this transport retardation mechanism may also play a minor role to selenium and molybdenum attenuation.

VEGETATION ENHANCED METAL REMOVAL

Phytoextraction has been known to remove metals from shallow groundwater.⁴ Vegetation between the AGREMAX™ temporary staging area and the property boundary (see the figure below) may also intercept and remove soluble metals in shallow groundwater.



¹ Crawley, M.E., 1977. A geochemical model for lithium and boron (Doctoral dissertation, Texas Tech University).

² Garabedian, S.P., 1987. Large-scale dispersive transport in aquifers: Field experiments and reactive transport theory (Doctoral dissertation, Massachusetts Institute of Technology).

³ Akhtar, M.S., Steenhuis, T.S., Richards, B.K. and McBride, M.B., 2003. Chloride and lithium transport in large arrays of undisturbed silt loam and sandy loam soil columns. Vadose Zone Journal, 2(4), pp.715-727.

⁴ Muthusaravanan, S., Sivarajasekar, N., Vivek, J.S., Paramasivan, T., Naushad, M., Prakashmaran, J., Gayathri, V. and Al-Duaij, O.K., 2018. Phytoremediation of heavy metals: mechanisms, methods and enhancements. Environmental chemistry letters, 16(4), pp.1339-1359.